

REGIONE PUGLIA

COMUNE:

COMUNE DI ANDRIA

Piazza Trieste e Trento - 76123 Andria (BT)

PROGETTO:

PROGETTO ESECUTIVO

aggiornato alle disposizioni del D.Lgs. 50/2016

RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO COMUNALE

2° LOTTO FUNZIONALE

RESP. UNICO DEL PROCEDIMENTO: ING. SANTOLA QUACQUARELLI

SOCIETA' INCARICATA



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TITOLO ELABORATO:

RELAZIONE TECNICA SPECIALISTICA E DI CALCOLO DELLE STRUTTURE

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RELAZIONE SPECIALISTICA STRUTTURALE E CALCOLI DELLE STRUTTURE

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1. RELAZIONE GENERALE ILLUSTRATIVA DELL'OPERA

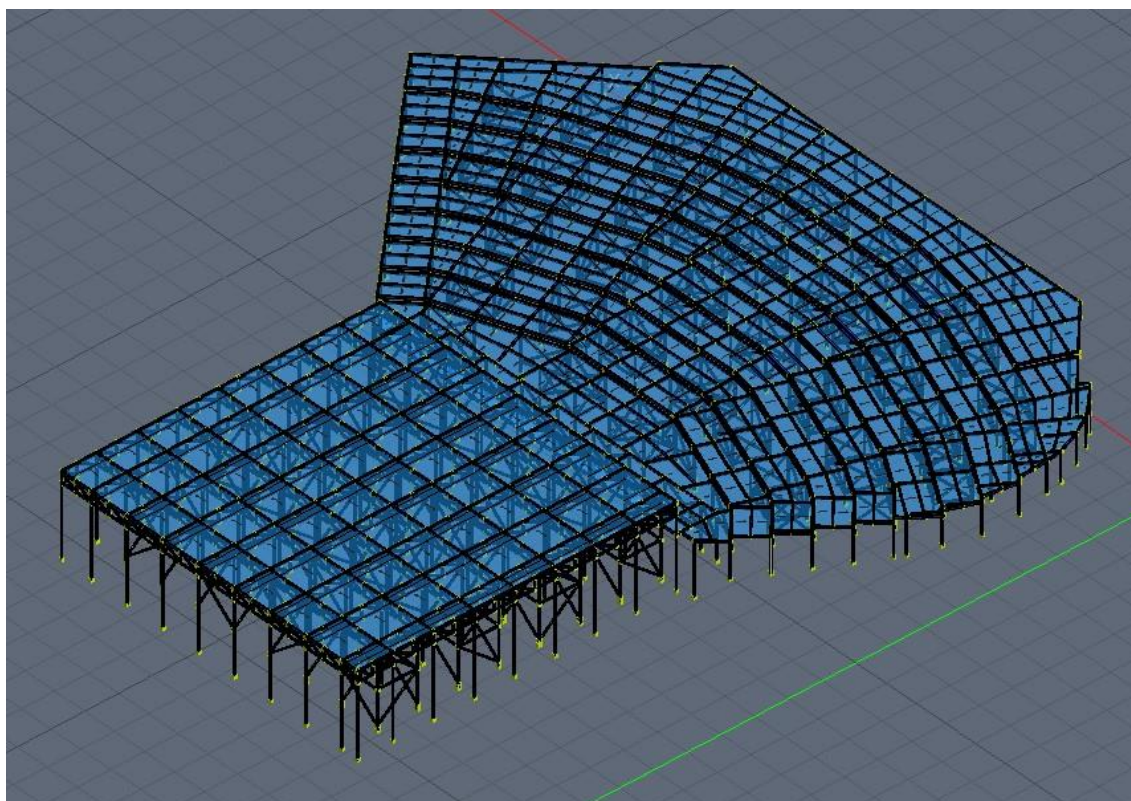
1.1. INQUADRAMENTO ARCHITETTONICO

L'edificio al cui interno saranno realizzati la struttura della platea e del palco e la struttura della graticcia è sito nella periferia dell'abitato di Andria.

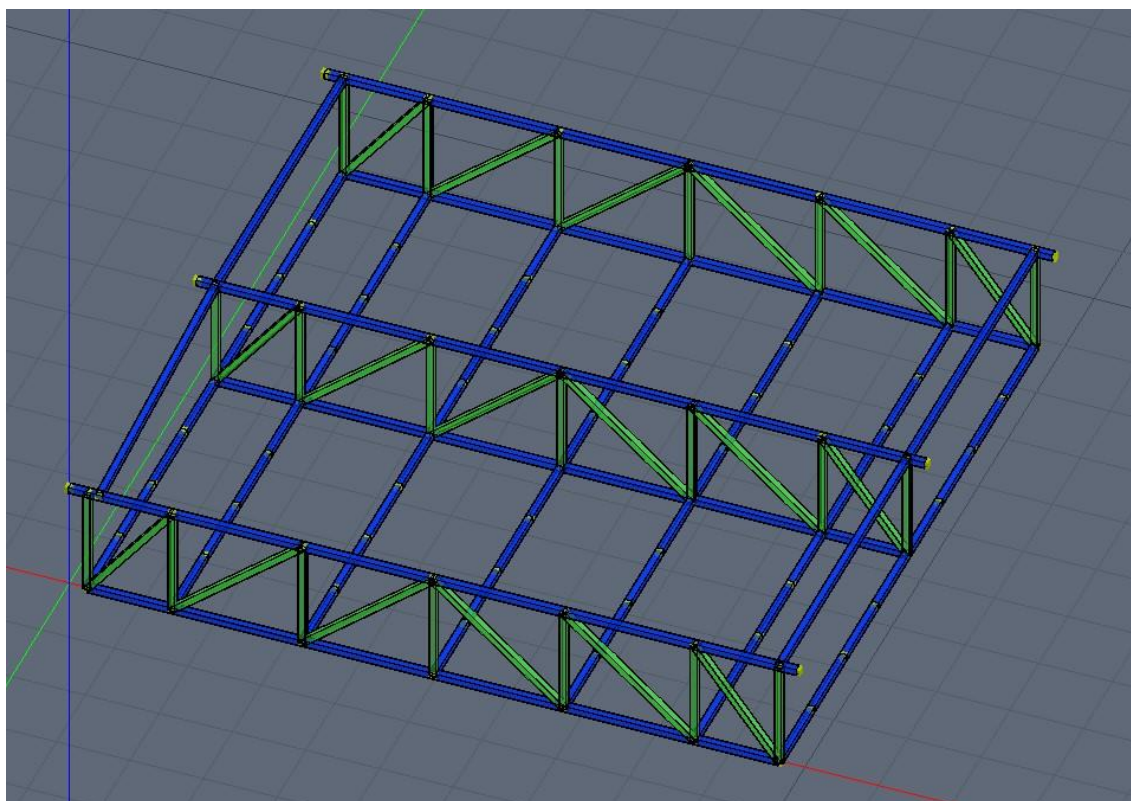
Le coordinate del sito sono: Longitudine 16,2825; Latitudine 41,2216. Il suolo si presenta pianeggiante.

L'intervento consiste nell'installazione di due strutture metalliche, una per la realizzazione della platea e del palco, l'altra per la realizzazione di una graticcia in corrispondenza del soffitto del palco.

Nel seguito è riportata la vista della struttura della platea e del palco.



Nel seguito è riportata la vista della struttura della graticcia.



1.2. ORGANIZZAZIONE STRUTTURALE

La struttura della platea e del palco sarà realizzata in acciaio da carpenteria metallica con profili aventi sezioni tubolari di 40x40x4 e 40x60x4, gli stessi saranno collegati tra loro con bulloni ad alta resistenza classe 8.8 e saldature a T a cordoni d'angolo a completa penetrazione.

La struttura della graticcia sarà realizzata in acciaio da carpenteria metallica con profili aventi sezioni tubolari di 100x100x8, gli stessi saranno collegati tra loro con bulloni ad alta resistenza classe 8.8 e saldature a T a cordoni d'angolo a completa penetrazione.

2. NORMATIVA TECNICA DI RIFERIMENTO

Le fasi di analisi e verifica della struttura sono state condotte in accordo con le seguenti disposizioni normative, per quanto applicabili:

- **Legge 2 febbraio 1974 n. 64**
Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche;
- **O.P.C.M. 20 marzo 2003 n. 3274**
Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica;
- **Deliberazione della Giunta regionale del 02 marzo 2004, n. 153**
Individuazione delle zone sismiche del territorio regionale e delle tipologie di edifici ed opere strategici e rilevanti;
- **Decreto Min. Infrastrutture e Trasporti 14 gennaio 2008**
Norme tecniche per le costruzioni;
- **Circolare del Min. Infrastrutture e Trasporti n. 617 del 02 febbraio 2009**
Istruzioni per l'applicazione delle "Nuove norme tecniche per le costruzioni" di cui al decreto ministeriale 14 gennaio 2008;
- **EUROCODICE 1**
Basi di calcolo ed azioni sulle strutture;
- **EUROCODICE 3**
Progettazione delle strutture di acciaio.

3. VALORI DI CALCOLO DELLE CARATTERISTICHE MECCANICHE DEI MATERIALI

Acciaio per carpenteria metallica **S275 J0**, rispondente alle seguenti caratteristiche:

- $f_{tk} \geq 430 \text{ N/mm}^2$ (Tensione di rottura a trazione);
- $f_{yk} \geq 275 \text{ N/mm}^2$; $f_{y, \max} < 1,2 f_y$ (Tensione di snervamento);
- $A_5 > 20\%$ (Allungamento minimo);
- $(f_t/f_y)_k > 1,20$;
- $E_s = 210000 \text{ N/mm}^2$ (Modulo di elasticità longitudinale).

Unioni bullonate con le seguenti indicazioni:

BULLONI

1. Viti di classe 8.8 secondo UNI EN ISO 898-1:2001
2. Dadi di classe 8 secondo UNI EN 20898-2:1994
3. Rosette in acciaio C50 UNI EN 10083-2:2006

Unioni saldate con le seguenti indicazioni:

La tipologia delle saldature è a T a cordoni d'angolo ed a completa penetrazione, di classe I a filo continuo, con elettrodi di qualità 3 o 4, con materiale di apporto di classe S275.

4. AZIONI SULLE COSTRUZIONI

4.1. PESI PROPRI

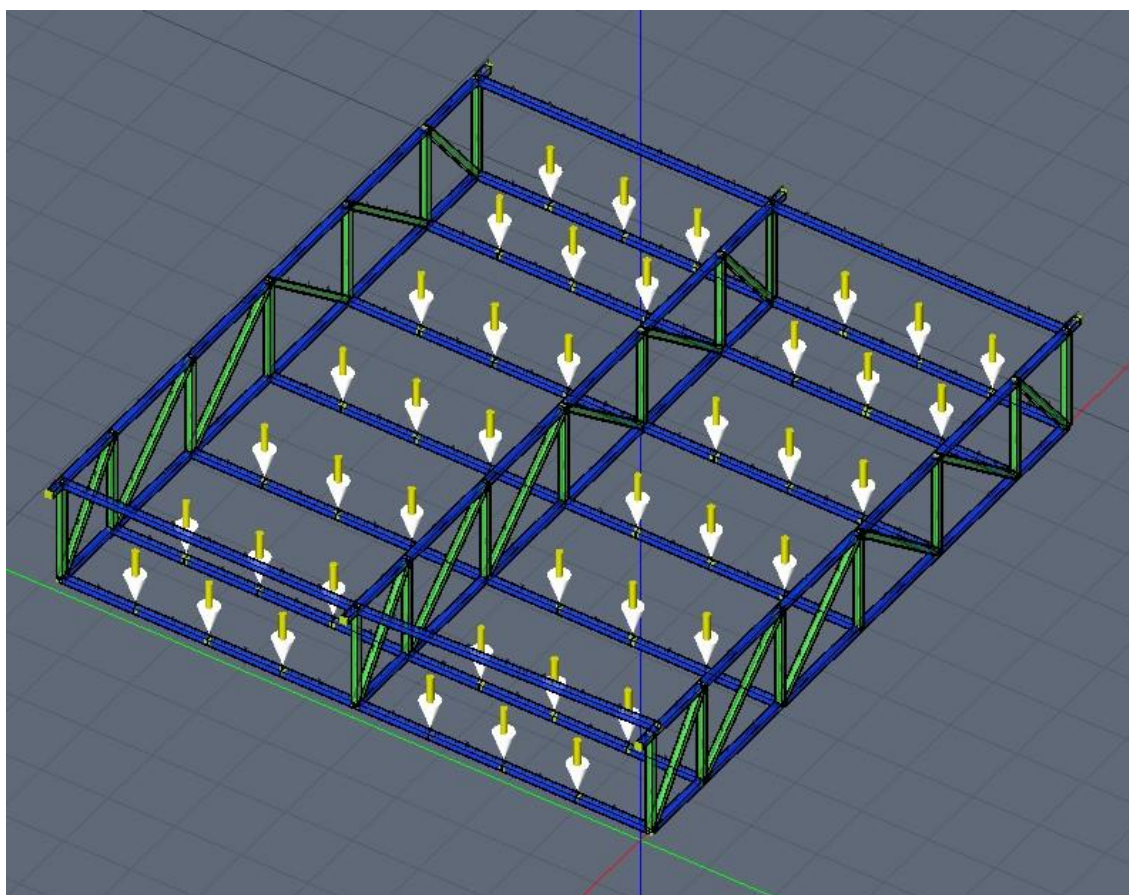
$\gamma_s = 7850 \text{ daN/m}^3$ (Peso specifico dell'acciaio).

4.2. PIANI DI CALPESTIO PLATEA E PALCO

Sol.N°	Descrizione	Spessore	QP	QF	QVar.	ψ_0	ψ_1	ψ_2	Luce netta	Def	%QX	%QY
		cm	kg/mq	kg/mq	kg/mq							
1	Palco	4	40	30	500	0.70	0.70	0.60	No	Si	50	50
2	Tribuna	6	35	155	500	0.70	0.70	0.60	No	Si	90	10

4.3. GRATTICCIA

La struttura della graticcia è stata caricata da quarantadue forze verticali di 500 kg posizionate come riportato nell'immagine seguente.



4.4. AZIONI DEL VENTO

Non considerate perchè la struttura è situata **all'interno di un edificio.**

4.5. AZIONI DELLA NEVE

Non considerate perchè la struttura è situata **all'interno di un edificio.**

4.6. AZIONI SISMICHE

I dati di progetto assunti ai fini dell'analisi sismica sono i seguenti:

- Vita nominale della costruzione V_N : 100;
- Classe d'uso: **IV**;
- Coefficiente di classe d'uso: **2,0**
- Periodo di riferimento per l'azione sismica V_R : 200;
- Latitudine: 40,8891;
- Longitudine: 17,1674;
- Categoria di sottosuolo: B;
- Categoria topografica: T1;
- Coefficiente di amplificazione topografica S_T : 1,00;
- Reticolo di riferimento: Reticolo di cui agli allegati A e B del D.M. 14/01/2008;
- **Stati limite considerati per le verifiche nei confronti dell'azione sismica:**

SLD perché consente di definire il limite entro cui la costruzione nel suo complesso garantisce inagibilità solo temporanee nelle condizioni post-sismiche;

SLV perché consente di verificare la struttura in maniera tale da conservare, a seguito del terremoto, parte della resistenza e rigidezza per azioni verticali ed un margine di sicurezza nei confronti del collasso per azioni sismiche orizzontali; nonostante rotture e crolli dei componenti non strutturali e significativi danni dei componenti strutturali.

STRUTTURA PLATEA E PALCO

- Dati per gli spettri di risposta delle componenti orizzontali allo SLD:
 - Probabilità P_{VR} di superamento in V_R : 63%;
 - **Periodo di ritorno dell'azione sismica T_R** : 201;
 - a_g : 0,1078 g;
 - F_0 : 2,4612;
 - T^*_C : 0,344 s
 - Coefficiente di amplificazione stratigrafica S_S : 1,00

- Coefficiente S: 1,00
 - T_B : 0,11 s
 - T_C : 0,34 s
 - T_D : 2,03 s
- Dati per gli spettri di risposta delle componenti orizzontali allo SLV:
- Probabilità P_{VR} di superamento in V_R : 10%;
 - **Periodo di ritorno dell'azione sismica** T_R : 1898,2;
 - a_g : 0,3465 g;
 - F_O : 2,3179;
 - T^*_C : 0,392 s
 - Coefficiente di amplificazione stratigrafica S_S : 1,00
 - Coefficiente S: 1,00
 - T_B : 0,13 s
 - T_C : 0,39 s
 - T_D : 2,99 s

STRUTTURA GRATTICIA

- Dati per gli spettri di risposta delle componenti orizzontali allo SLD:
- Probabilità P_{VR} di superamento in V_R : 63%;
 - **Periodo di ritorno dell'azione sismica** T_R : 201;
 - a_g : 0,1078 g;
 - F_O : 2,4612;
 - T^*_C : 0,344 s
 - Coefficiente di amplificazione stratigrafica S_S : 1,00
 - Coefficiente S: 1,00
 - T_B : 0,11 s
 - T_C : 0,34 s
 - T_D : 2,03 s
- Dati per gli spettri di risposta delle componenti orizzontali allo SLV:
- Probabilità P_{VR} di superamento in V_R : 10%;
 - **Periodo di ritorno dell'azione sismica** T_R : 1898,2;
 - a_g : 0,3465 g;
 - F_O : 2,3179;
 - T^*_C : 0,392 s
 - Coefficiente di amplificazione stratigrafica S_S : 1,00
 - Coefficiente S: 1,00
 - T_B : 0,13 s

- T_C : 0,39 s
- T_D : 2,99 s

5. ANALISI STRUTTURALE

5.1. DESCRIZIONE DEI MODELLI STRUTTURALI

Le strutture, così come descritte al punto 1.2, sono state schematizzate con un modello spaziale costituito da elementi finiti tipo beam, caricati da elementi piani, secondo l'effettiva realizzazione. I calcoli e le verifiche sono condotti con il metodo semiprobabilistico degli stati limite secondo le indicazioni del D.M. 14 gennaio 2008. Su tutti gli elementi strutturali è inoltre possibile applicare direttamente ulteriori azioni concentrate e/o distribuite. Le azioni introdotte direttamente sono combinate con le altre (carichi permanenti, accidentali e sisma) mediante le combinazioni di carico di seguito descritte; da esse si ottengono i valori probabilistici da impiegare successivamente nelle verifiche.

Le azioni sono state assegnate su aste e piastre, definendo le seguenti condizioni di carico:

STRUTTURA PLATEA E PALCO

Descrizione	Tipo
Peso Proprio	Automatica
QP Solai	Automatica
QFissi Solai	Automatica
QV Solai	Automatica
QV SolaiPsi0	Automatica
QV SolaiPsi1	Automatica
QV SolaiPsi2	Automatica
Carichi termici	Utente

STRUTTURA GRATTICIA

Descrizione	Tipo
Peso Proprio	Automatica
Carichi termici	Utente
QFissi Travi	Utente

5.2. TIPI DI ANALISI SVOLTE

Il calcolo delle azioni sismiche è stato eseguito in analisi dinamica modale, considerando il comportamento della struttura in regime elastico lineare, analizzando lo stato limite di danno (SLD) e lo stato limite di salvaguardia della vita (SLV) e adottando le seguenti combinazioni di carico:

Scenario di calcolo Struttura platea e palco										
Scenario : Set_NT_SLV_SLD_A2_STR/GEO										
Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
1) Solo Permanenti	STR				0.60					
						Peso Proprio	1.3	Si	Si	1
						QP Solai	1.3	Si	Si	1

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	1	No	No	1
2) AD QVSolai	STR+GEO				0.90					
						Peso Proprio	1.3	Si	Si	1
						QP Solai	1.3	Si	Si	1
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1.5	Si	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.9	Si	No	1
3) AD QVSolai	STR+GEO				0.90					
						Peso Proprio	1.3	Si	Si	1
						QP Solai	1.3	Si	Si	1
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1.5	Si	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.9	Si	No	1
4) AD Neve	STR+GEO				0.80					
						Peso Proprio	1.3	Si	Si	1
						QP Solai	1.3	Si	Si	1
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1.5	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.9	Si	No	1
5) AD Neve	STR+GEO				0.80					
						Peso Proprio	1.3	Si	Si	1
						QP Solai	1.3	Si	Si	1
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1.5	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.9	Si	No	1
6) AD VentoX Vert. Sfav	STR+GEO				0.90					
						Peso Proprio	1.3	Si	Si	1
						QP Solai	1.3	Si	Si	1
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1.5	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.9	Si	No	1
7) AD VentoY Vert. Sfav	STR+GEO				0.90					
						Peso Proprio	1.3	Si	Si	1
						QP Solai	1.3	Si	Si	1
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1.5	Si	No	1

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.9	Si	No	1
8) AD Termici	STR+GEO				1.00					
						Peso Proprio	1.3	Si	Si	1
						QP Solai	1.3	Si	Si	1
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1.5	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	1.5	Si	No	1
9) AD Termici	STR+GEO				1.00					
						Peso Proprio	1.3	Si	Si	1
						QP Solai	1.3	Si	Si	1
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1.5	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	1.5	Si	No	1
10) AD VentoX Vert fav	STR+GEO				0.90					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	No	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	1	No	No	1
11) AD VentoY Vert fav	STR+GEO				0.90					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	No	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	1	No	No	1
12) SISMAX_SLV	Modale STR+GEO	SpettroNT	1.15	0	1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Carichi termici	1	No	No	1
13) SISMAX_SLV	Modale STR+GEO	SpettroNT	1.15	90	1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Carichi termici	1	No	No	1
14) AD QVSolai	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	Si	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.6	Si	No	1
15) AD QVSolai	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	Si	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.6	Si	No	1
16) AD Neve	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.6	Si	No	1
17) AD Neve	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.6	Si	No	1
18) AD VentoX	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.6	Si	No	1
19) AD vento Y	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	0.6	Si	No	1

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
20) AD Termici	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	1	Si	No	1
21) AD Termici	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	1	Si	No	1
22) AD QVSolai	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	Si	No	1
						QV SolaiPsi2	1	No	Si	1
						Carichi termici	1	No	No	1
23) AD Neve	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Carichi termici	1	No	No	1
24) AD VentoX	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Carichi termici	1	No	No	1
25) AD Vento Y	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Carichi termici	1	No	No	1
26) AD Termici	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Carichi termici	0.2	Si	No	1
27) Quasi P1	SLE Q.Perm.				1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Carichi termici	1	No	No	1
28) SISMAX_SLD	Modale SLE	SpettroNT	1.15	0	1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Carichi termici	1	No	No	1
29) SISMAX_SLD	Modale SLE	SpettroNT	1.15	90	1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Carichi termici	1	No	No	1

Scenario di calcolo Struttura graticcia

Scenario : Set_NT_SLV_SLD_A2_STR/GEO

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
1) Solo Permanenti	STR				0.60					
						Peso Proprio	1.3	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1.3	Si	Si	1
2) AD QVSolai	STR+GEO				0.90					
						Peso Proprio	1.3	Si	Si	1
						Carichi termici	0.9	Si	No	1
						QFissi Travi	1.3	Si	Si	1
3) AD QVSolai	STR+GEO				0.90					
						Peso Proprio	1.3	Si	Si	1
						Carichi termici	0.9	Si	No	1
						QFissi Travi	1.3	Si	Si	1
4) AD Neve	STR+GEO				0.80					
						Peso Proprio	1.3	Si	Si	1
						Carichi termici	0.9	Si	No	1
						QFissi Travi	1.3	Si	Si	1

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
5) AD Neve	STR+GEO				0.80					
						Peso Proprio	1.3	Si	Si	1
						Carichi termici	0.9	Si	No	1
						QFissi Travi	1.3	Si	Si	1
6) AD VentoX Vert. Sfav	STR+GEO				0.90					
						Peso Proprio	1.3	Si	Si	1
						Carichi termici	0.9	Si	No	1
						QFissi Travi	1.3	Si	Si	1
7) AD VentoY Vert. Sfav	STR+GEO				0.90					
						Peso Proprio	1.3	Si	Si	1
						Carichi termici	0.9	Si	No	1
						QFissi Travi	1.3	Si	Si	1
8) AD Termici	STR+GEO				- 1.00					
						Peso Proprio	1.3	Si	Si	1
						Carichi termici	1.5	Si	No	1
						QFissi Travi	1.3	Si	Si	1
9) AD Termici	STR+GEO				- 1.00					
						Peso Proprio	1.3	Si	Si	1
						Carichi termici	1.5	Si	No	1
						QFissi Travi	1.3	Si	Si	1
10) AD VentoX Vert fav	STR+GEO				0.90					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1
11) AD VentoY Vert fav	STR+GEO				0.90					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1
12) SISMAX_SLV	Modale STR+GEO	SpettroNT	1	0	1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1
13) SISMAX_SLV	Modale STR+GEO	SpettroNT	1	90	1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1
14) AD QVSolai	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	0.6	Si	No	1
						QFissi Travi	1	Si	Si	1
15) AD QVSolai	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	0.6	Si	No	1
						QFissi Travi	1	Si	Si	1
16) AD Neve	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
						Carichi termici	0.6	Si	No	1
						QFissi Travi	1	Si	Si	1
17) AD Neve	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	0.6	Si	No	1
						QFissi Travi	1	Si	Si	1
18) AD VentoX	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	0.6	Si	No	1
						QFissi Travi	1	Si	Si	1
19) AD vento Y	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	0.6	Si	No	1
						QFissi Travi	1	Si	Si	1
20) AD Termici	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	Si	No	1
						QFissi Travi	1	Si	Si	1
21) AD Termici	SLE Rara				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	Si	No	1
						QFissi Travi	1	Si	Si	1
22) AD QVSolai	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1
23) AD Neve	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1
24) AD VentoX	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1
25) AD Vento Y	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1
26) AD Termici	SLE Freq.				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	0.2	Si	No	1
						QFissi Travi	1	Si	Si	1
27) Quasi P1	SLE Q.Perm.				1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1
28) SISMAX_SLD	Modale SLE	SpettroNT	1	0	1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
29) SISMAX_SLD	Modale SLE	SpettroNT	1	90	1.00					
						Peso Proprio	1	Si	Si	1
						Carichi termici	1	No	No	1
						QFissi Travi	1	Si	Si	1

5.3. CODICI DI CALCOLO UTILIZZATI

Origine e caratteristiche dei codici di calcolo

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Produzione e distribuzione	SOFT.LAB srl via Borgo II - 82030 PONTE (BN) tel. ++39 (824) 874392 fax ++39 (824) 874431 internet: http://www.soft.lab.it e.mail: info@soft.lab.it
Sigla:	IperSpaceMax 7.2.0
Licenza n.	Concesso in licenza a SISTO-CAMPANELLA-SBIROLI-CERT codice utente C00604

Il solutore agli elementi finiti impiegato nell'analisi è SpaceSolver, per il calcolo di strutture piane e spaziali schematizzabili da un insieme di elementi finiti tipo

- BEAM,
- PLATE-SHELL,
- WINK,
- BOUNDARY,

interagenti tra loro attraverso i nodi, con la possibilità di tenere in conto tutti i possibili disassamenti, mediante l'introduzione di concetti rigidi e traslazioni degli elementi bidimensionali.

Il solutore lavora in campo elastico lineare, si basa sulle routines di Matlab ed è stato sviluppato in collaborazione con l'Università di Roma – Tor Vergata. Il solutore offre la possibilità di risolvere anche travi su suolo alla Winkler con molle spalmate sull'intera suola, anziché sul solo asse, plinti diretti e su pali, pali singoli, platee, piastre sottili e spesse con controllo delle rotazioni attorno all'asse normale alla piastra (drilling). Inoltre, per gli elementi BEAM considera il centro di taglio e non il baricentro.

L'affidabilità del solutore è stata testata su una serie di esempi campioni calcolati con altri procedimenti o con formule note, di cui si rende disponibile la documentazione.

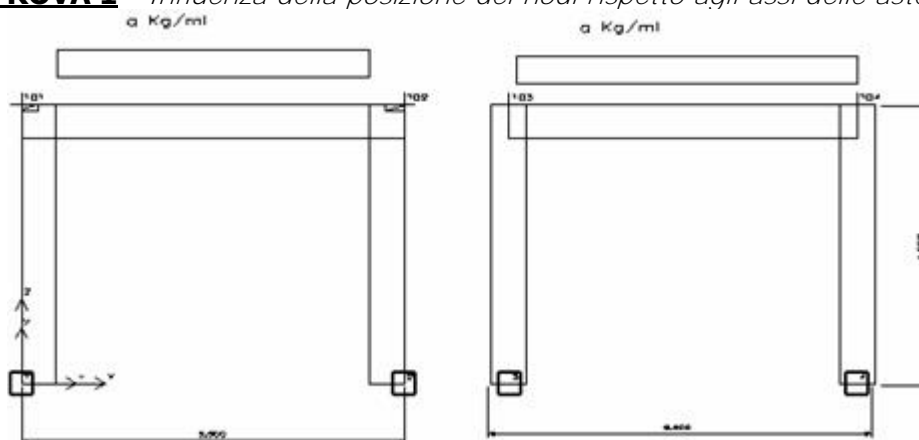
Affidabilità dei codici utilizzati

Il programma è dotato di una serie di filtri di auto diagnostica che segnalano i seguenti eventi:

- labilità della struttura;
- assenza di masse;
- nodi collegati ad aste nulle;
- mancanza di terreno sugli elementi in fondazione;
- controllo sull'assegnazione dei nodi all'impalcato;
- correttezza degli spettri di progetto;
- fattori di partecipazione modali;
- assegnazione dei criteri di progetto agli elementi;
- numerazione degli elementi strutturali;
- congruenza delle connessioni tra elementi shell;
- congruenza delle aree di carico;
- definizione delle caratteristiche d'inerzia delle sezioni;
- presenza del magrone sotto la travi tipo winkler;
- elementi non verificati per semi progetto allo SLU, con inserimento automatico delle armature secondo i criteri di progetto;
- elementi non verificati allo SLU per armature già inserite nell'elemento strutturale;
- elementi non verificati allo SLE per armature già inserite nell'elemento strutturale;

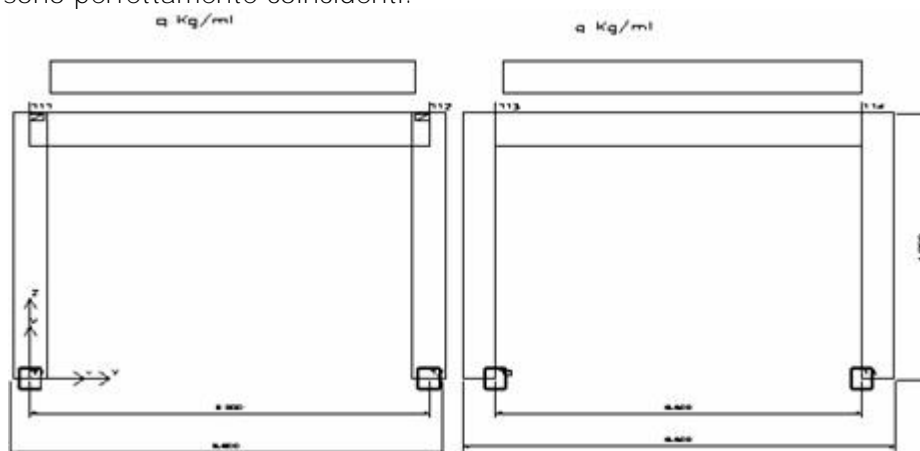
L'affidabilità dei codici utilizzati è stata testata attraverso la risoluzione di alcuni casi prova, che il Produttore fornisce all'Utente, e vengono di seguito documentati.

CASO PROVA 1 - *Influenza della posizione dei nodi rispetto agli assi delle aste*



I due portali sono due strutture identiche, ma il primo ha la luce teorica (da nodo a nodo) del traverso di lunghezza maggiore ($5.50 > 5.00$) e i risultati di calcolo sono

diversi; se però si introducono nel traverso del primo telaio dei conci rigidi pari a 25 cm, cioè mezzo pilastro, allora la luce flessibile dei due telai coincide praticamente e i risultati sono perfettamente coincidenti.

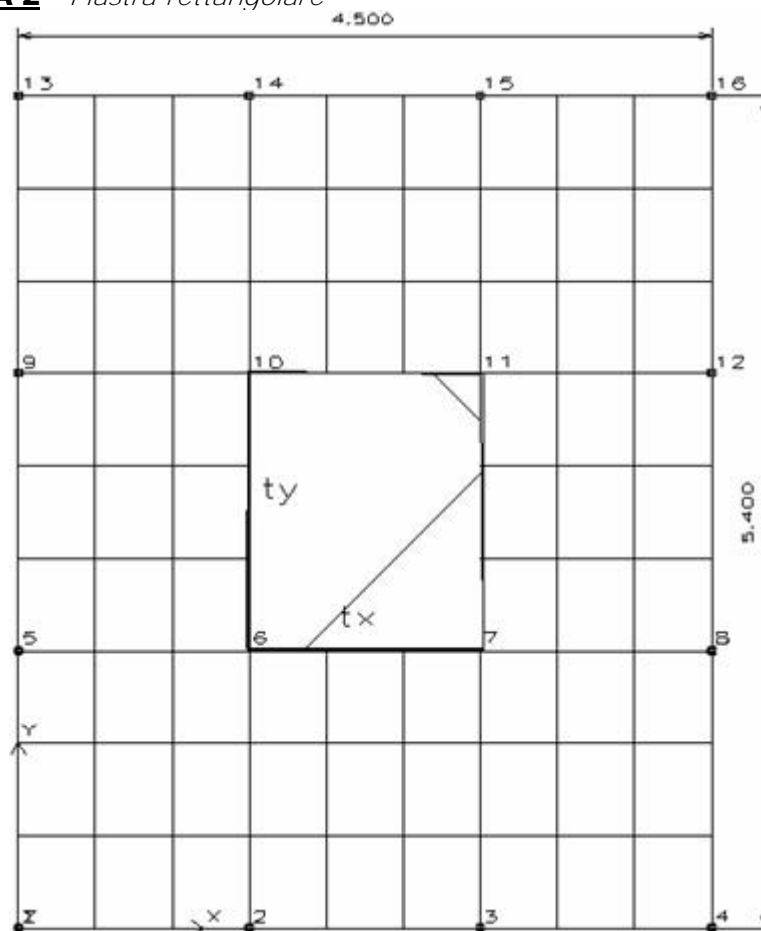


Anche in questo esempio i portali sono due strutture identiche, però il traverso del primo è più lungo e quindi i risultati saranno gli stessi se vengono introdotti sul traverso del primo portale dei conci rigidi pari a metà pilastro.

In entrambi gli esempi (anziché introdurre i conci rigidi) si potevano avere gli stessi risultati modificando il filo fisso del traverso del primo portale rispettivamente 8585 per l'esempio I e 8684 per l'esempio II.

Concludendo qualunque sia la posizione dei nodi rispetto agli assi delle travi e dei pilastri, le sollecitazioni (vengono prese sugli assi delle aste) sono sempre le stesse se la geometria 3D è la stessa e si scelgono oculatamente i fili fissi o si introducono i conci rigidi. Al riguardo si ribadisce che lo schema di calcolo è quello 3D e NON lo schema unifilare. Infine si fa notare che l'equilibrio nel nodo (ad esempio N° 101) non sussiste in quanto le sollecitazioni nel traverso vengono prese sull'asse dello stesso, mentre le sollecitazioni del pilastro vengono prese nel nodo e quindi in punti diversi. Per l'equilibrio quindi non bisogna prendere in considerazione solo i momenti, ma anche gli effetti delle altre sollecitazioni sul nodo rigido.

CASO PROVA 2 - *Piastra rettangolare*



Siano L_x ed L_y i lati della piastra ($L_y \geq L_x$) e t_x t_y i corrispondenti lati del rettangolo caricato, si ha:

p carico uniforme;

$P = p \cdot t_x \cdot t_y$ carico totale;

$M_{xm} = a_{xm} \cdot P$ momento al centro, agente parallelamente al lato L_x (cioè nella sezione di mezzeria parallela al lato L_y);

$M_{ym} = a_{ym} \cdot P$ momento al centro, agente parallelamente al lato L_y (cioè nella sezione di mezzeria parallela al lato L_x).

Nel caso in esame essendo:

$L_x = 4.5$ [m]; $L_y = 5.4$ [m]; $t_x = 1.5$ [m]; $t_y = 1.8$ [m]; $p = 5000$ [daN/mq];

si ha:

$P = 13500$ [daN]

e per $n = 0$ sarà: $a_{xm} = 0.1377$; $a_{ym} = 0.1050$ e pertanto si ha:

$M_{xm} = 1860$ [dNm]; $M_{ym} = 1418$ [dNm].

Se consideriamo la piastra discretizzata come in figura (9 x 9) con IperSpace si hanno i seguenti valori:

$M_{xx} = 1731$ [dNm]; $M_{yy} = 1314$ [dNm] con un errore $< 8 \%$

Se la discretizzazione è di 15 x 15 elementi i valori sono:

$$M_{xx} = 1810 \text{ [dNm]}; M_{yy} = 1382 \text{ [dNm]} \text{ con un errore } < 3 \%$$

Se la discretizzazione è di 21 x 21 elementi i valori sono:

$$M_{xx} = 1832 \text{ [dNm]}; M_{yy} = 1400 \text{ [dNm]} \text{ con un errore } < 1.5 \%$$

CASO PROVA 3 - *Mensola inflessa*

Prendiamo in considerazione la mensola di acciaio ($E = 20.000 \text{ kN/cm}^2$, e $\nu = 0.25$) delle dimensioni 48x4x1 cm, sollecitata all'estremità da un taglio di 40 kN, riportata a pag. 121 del testo di C.A. BREBBIA e J.J. CONNOR.

Il limite superiore dello spostamento all'estremo caricato, ottenuto con la Teoria delle travi è: cm 0.53374.

Nella tabella che segue vengono riportati i valori dello spostamento per vari tipi di elementi finiti e varie discretizzazioni.

Risultati estratti dal Testo di Trebbia e Connor

Tipo di elemento	Numero elementi	Freccia di estremità	Errore %
Elemento triangolare a deformazione costante	160	0.45834	14.59
	576	0.51282	3.92
Elemento triangolare a deformazione lineare	160	0.53259	0.22
	576	0.53353	0.04
Elemento triangolare a deformazione quadratica	68	0.53059	0.17
	214	0.53259	0.22
Elemento rettangolare di primo ordine	160	0.51679	3.18
Elemento rettangolare del terzo ordine	52	0.52807	1.25

Risultati del solutore di IperSpace

Tipo di elemento	Numero elementi	Freccia di estremità	Errore %
Elemento rettangolare	16	0.5198	2.60
"	36	0.5298	0.74
"	64	0.5311	0.49
"	100	0.5322	0.29
"	144	0.5328	0.18

L'elemento piastra consente, con una discretizzazione molto piccola ($12 \times 3 = 36$ elementi), di avere un errore inferiore all'1%. Per ottenere risultati simili occorre eseguire non solo discretizzazioni più spinte, ma scegliere anche elementi a

deformazione quadratica o di ordine superiore. L'impiego di tale elemento risulta particolarmente indicato per seguire le prescrizioni delle Norme Tecniche (D.M. 2005), che impongono la sostituzione ai pilastri snelli delle pareti. La risoluzione di questo problema di modellazione consente di evitare errori grossolani sulla stima di sforzi e deformazioni degli elementi bidimensionali.

CASO PROVA 4 - *Analisi Dinamica*

Si consideri la struttura a telaio riportata nelle successive figure, costituita da un materiale con modulo elastico $E=250.000$ daN/mq, nella quale le dimensioni delle sezioni trasversali dei pilastri sono:

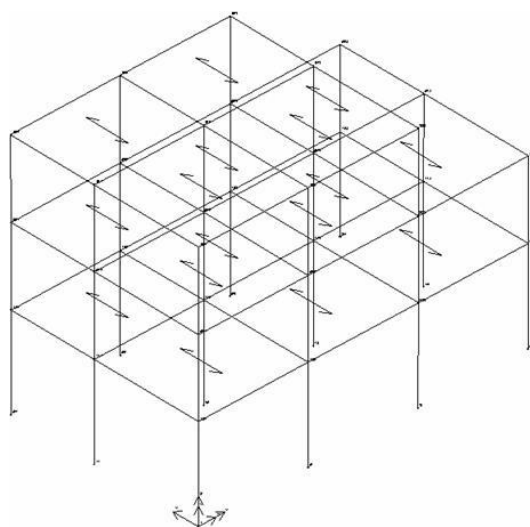
50x50 al primo piano

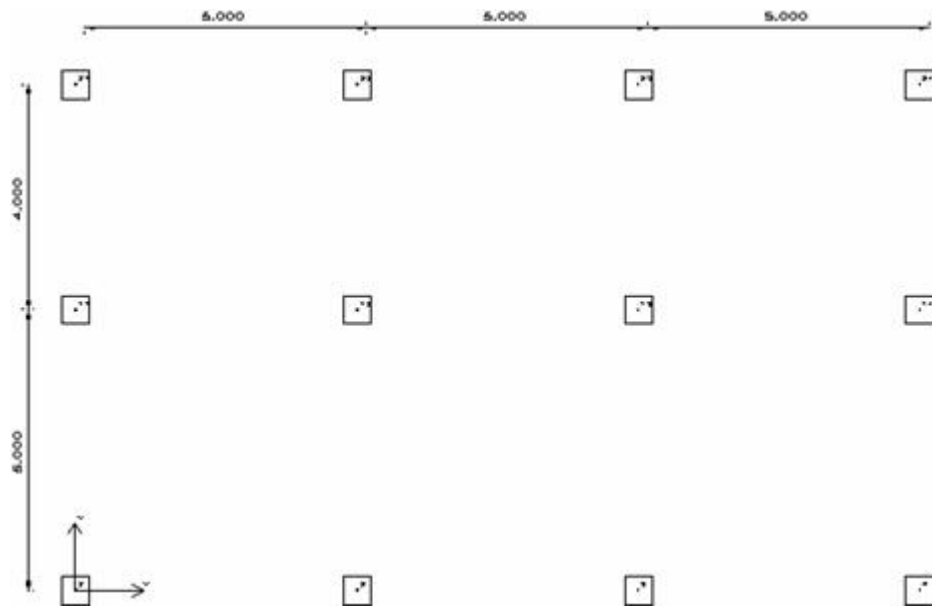
40x40 al secondo piano

35x35 al terzo piano

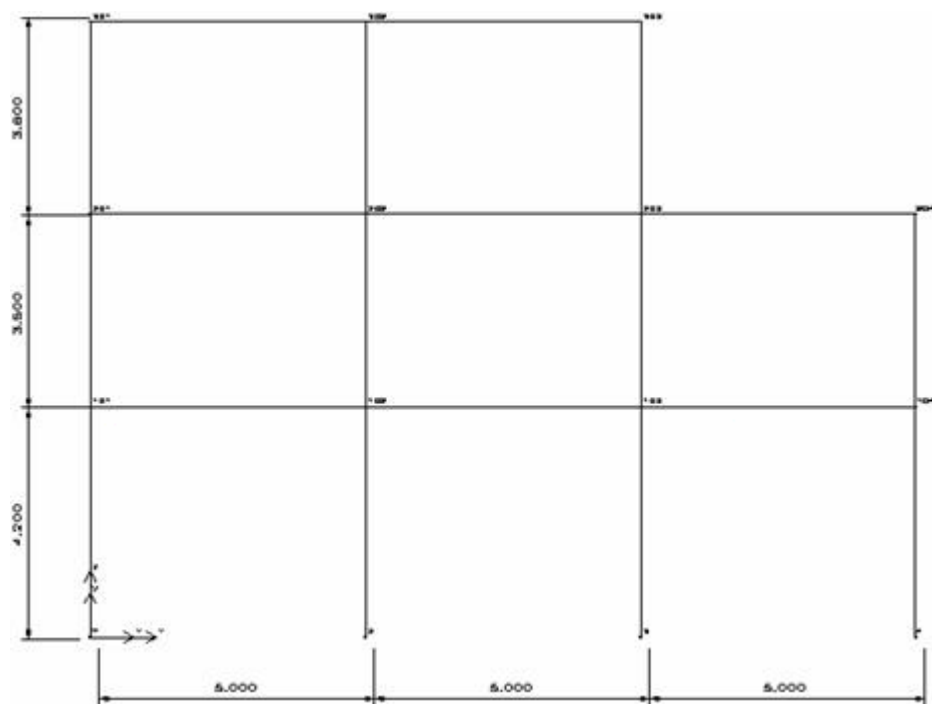
e le dimensioni delle sezioni trasversali delle travi sono tutte 25x60.

I carichi gravitazionali sono tutti nulli a meno di un carico uniformemente distribuito, dato attraverso le aree di carico costituite dai solai, sulla struttura è di 850 daN/mq.

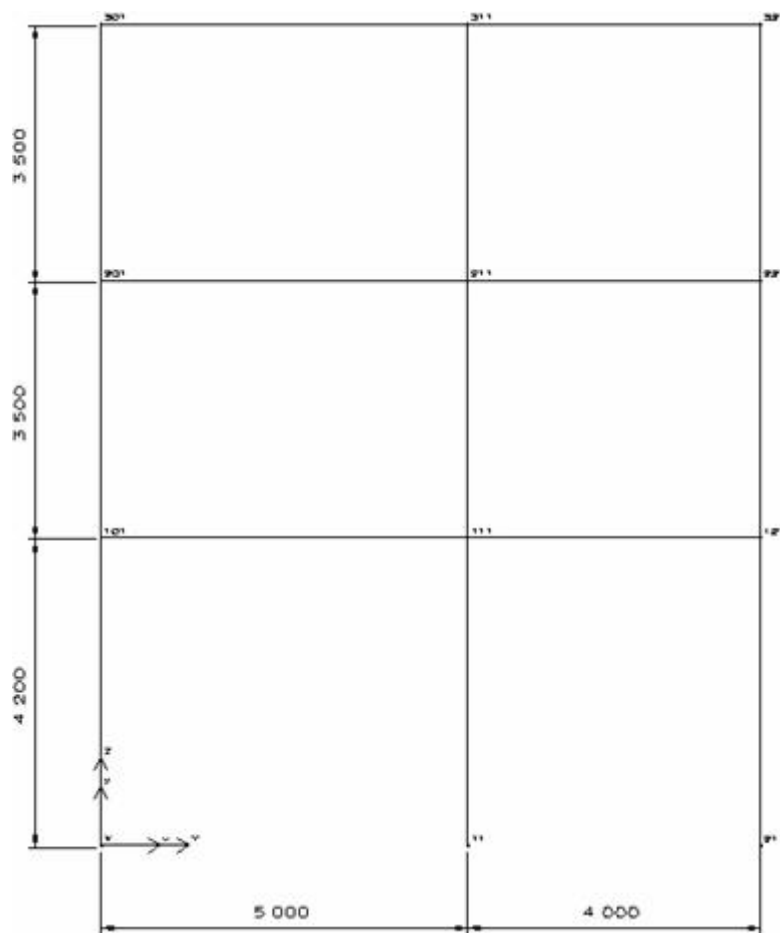




Pianta



Telaio 1



Telaio 4

Nell'ipotesi di telai shear-type, cioè con traversi infinitamente rigidi, il calcolo eseguito a mano dai proff. Carlo Greco e Roberto Ramasco dell' Università di Napoli (esempio riportato nella pubblicazione PROGETTAZIONE E PARTICOLARI ESECUTIVI IN ZONA SISMICA – ed. ANCE), fornisce, per $S=12$, i seguenti risultati:

Modo Periodo in sec.		Spostamenti dir y dei nodi del telaio 4 in mm	
1	0.3227	piano primo	1.204
2	0.3160	piano secondo	2.667
3	0.2175	piano terzo	4.332
4	0.1466		
5	0.1450		

I momenti nei pilastri del telaio 4, dovuti solo al primo modo di vibrare, (uguali al piede ed in testa di ogni pilastro, essendo i traversi infinitamente rigidi) sono:

$M_1=5309$ daNm; $M_2=3840$ daNm; $M_3=2622$ daNm.

Risultati di IperSpace:

a) traversi deformabili, cioè travi di sezione effettiva (25x60)

Modo	Periodo in sec	Spostamenti in mm dei nodi del pilastro N° 1	
1	0.431	piano primo	2.157
2	0.416	piano secondo	5.000
3	0.326	piano terzo	7.300
4	0.173		
5	0.170		

I momenti nel pilastro N° 1 (telaio N° 4), dovuti al primo modo (non più uguali in testa e piede come nel modello shear-type) sono :

M1 max=6633 dNm; M2max=3210 dNm; M3max=2045 dNm.

Dai risultati si evince che ci sono le seguenti variazioni:

- 25 % circa sul periodo del primo modo di vibrare;
- 40 % sullo spostamento del terzo piano;
- 20 % sul momento d'incastro al piede del piano primo.

b) traversi rigidi (travi di sezione 200x200 e modulo 21000000 dN/mq)

Modo	Periodo in sec.	Spostamenti in mm dei nodi del pilastro N° 1	
1	0.326	piano primo	1.244
2	0.317	piano secondo	2.728
3	0.251	piano terzo	4.203
4	0.151		
5	0.148		

I momenti nel pilastro N° 1, dovuti al primo modo (uguali in testa e piede) sono:

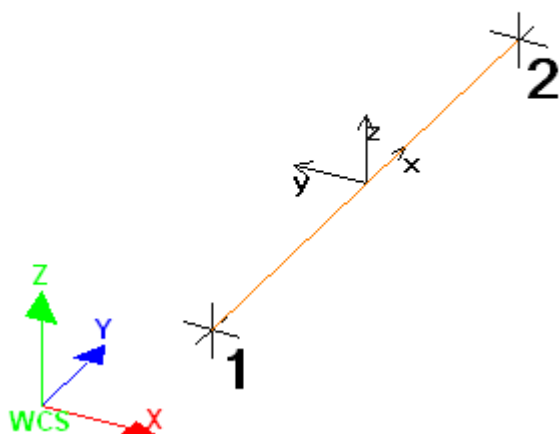
M1=5509 dNm; M2=3878 dNm; M3=2258 dNm.

In questo caso le variazioni sono contenute entro il 3 %. E' da presupporre che esse siano dovute essenzialmente al differente tipo di arrotondamento praticato tra il calcolo manuale ed il calcolo numerico, nonché al fatto che il calcolo eseguito da IperSpace è di tipo spaziale.

Si può concludere che il test su IperSpace è nettamente positivo e che il modello shear-type fornisce risultati tanto più grossolani quanto più ci si allontana dall'ipotesi di traversi infinitamente rigidi.

Presentazione dei risultati

E' stato impiegato il Sistema Internazionale per le unità di misura, con riferimento al daN per le forze.



Il sistema di riferimento globale rispetto al quale è stata riferita l'intera struttura è una terna di assi cartesiani sinistrorsa OXYZ (X,Y, e Z sono disposti e orientati rispettivamente secondo il pollice, l'indice ed il medio della mano destra, una volta posizionati questi ultimi a 90° tra loro).

La terna di riferimento locale per un'asta è pure una terna sinistrorsa O'xyz che ha l'asse x orientato dal nodo iniziale I dell'asta verso il nodo finale J e gli assi y e z diretti secondo gli assi geometrici della sezione con l'asse y orizzontale e orientato in modo da portarsi a coincidere con l'asse x a mezzo di una rotazione oraria di 90° e l'asse z di conseguenza.

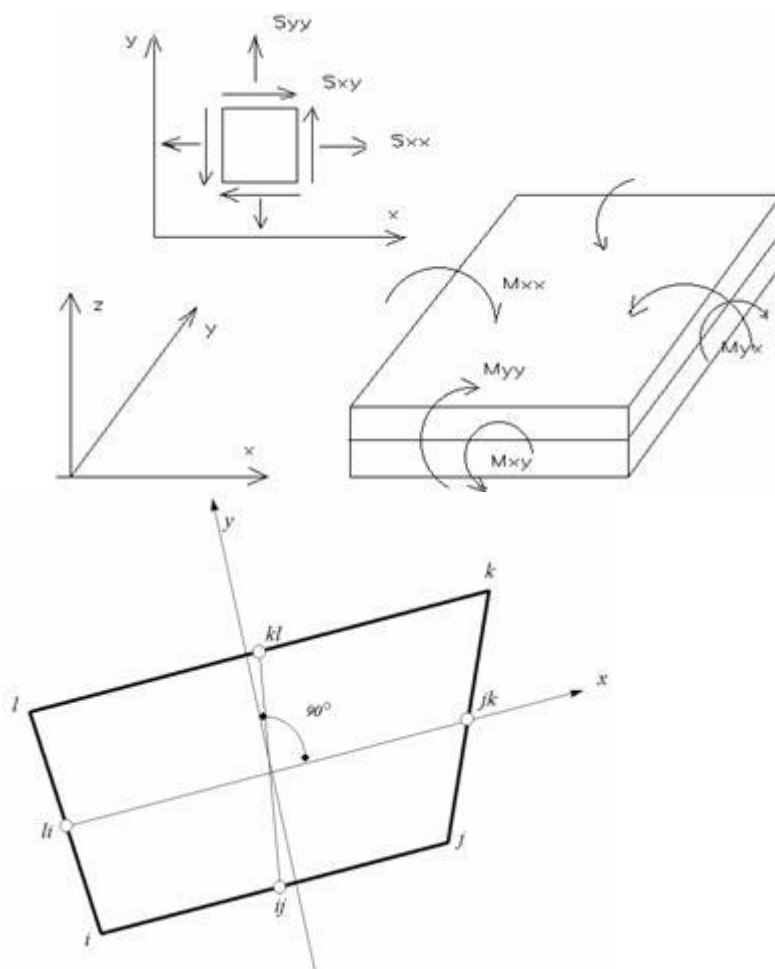
Per un'asta comunque disposta nello spazio la sua terna locale è orientata in modo tale da portarsi a coincidere con la terna globale a mezzo di rotazioni orarie degli assi locali inferiori a 180°.

- Le forze, sia sulle aste che sulle pareti o lastre, sono positive se opposte agli assi locali;
- Le forze nodali sono positive se opposte agli assi globali;
- Le coppie sono positive se sinistrorse.

Le caratteristiche di sollecitazione sono positive se sulla faccia di normale positiva sono rappresentate da vettori equiversi agli assi di riferimento locali; in particolare il vettore momento positivo rappresenta una coppia che ruota come le dita della mano destra che si chiudono quando il pollice è equiverso all'asse locale.

- Le traslazioni sono positive se concordi con gli assi globali;
- Le rotazioni sono positive se sinistrorse.

Il sistema di riferimento locale per gli elementi bidimensionali è quello riportato in figura:



La terna locale per l'elemento shell è costituita dall'asse x locale che va dal nodo li al nodo jk , l'asse y è diretto secondo il piano dell'elemento e orientato verso il nodo l e l'asse z di conseguenza in modo da formare la solita terna sinistrorsa. L'asse z locale rappresenta la normale positiva all'elemento.

Le sollecitazioni dell'elemento sono:

a) sforzi membranali.

$$S_{xx} = s_x$$

$$S_{yy} = s_y$$

$$S_{xy} = t_{xy}$$

b) sforzi flessionali:

M_{xx} momento flettente che genera s_x , cioè intorno ad y .

M_{yy} momento flettente che genera s_y , cioè intorno ad x

M_{xy} momento torcente che genera t_{xy} .

Le sollecitazioni principali dell'elemento sono:

$$M_{1,2} = \frac{M_{xx} + M_{yy}}{2} \pm \sqrt{\left(\frac{M_{xx} - M_{yy}}{2}\right)^2 + M_{xy}^2}$$

$$S_{1,2} = \frac{S_{xx} + S_{yy}}{2} \pm \sqrt{\left(\frac{S_{xx} - S_{yy}}{2}\right)^2 + S_{xy}^2}$$

$$\tan 2\theta = \frac{M_{xy}}{M_{xx} - M_{yy}}$$

dove θ è l'angolo formato dagli assi principali di M_1 e M_2 con quelli di riferimento e

$$\tan 2\Psi = \frac{S_{xy}}{S_{xx} - S_{yy}}$$

dove Ψ è l'angolo formato dagli assi principali di S_1 e S_2 con quelli di riferimento.

L'elemento shell usato come piastra dà i momenti flettenti e non i tagli in direzione ortogonale all'elemento che possono ottenersi come derivazione dei momenti flettenti:

$$T_{zx} = M_{xx,x} + M_{xy,y}$$

$$T_{zy} = M_{xy,y} + M_{yy,y}$$

quando invece viene usato come lastra ci restituisce una 's' costante ed una 't' costante non adatti a rappresentare momenti flettenti, ma solo sforzi normali e tagli nel piano della lastra.

I tabulati di calcolo contengono due sezioni principali: la descrizione del modello di calcolo e la presentazione dei risultati.

La descrizione del modello di calcolo contiene:

- i dati generali (dimensioni)
- le coordinate nodali;
- i vincoli dei nodi e i vincoli interni delle aste, con le eventuali sconnessioni;
- le caratteristiche sezionali;
- le caratteristiche dei solai;
- le caratteristiche delle aste;
- i carichi sulle aste, sui nodi e sui muri (inclusa la distribuzione delle distorsioni impresse, e delle variazioni e dei gradienti di temperatura);
- configurazione di sistemi che introducono stati coattivi;
- le caratteristiche dei materiali;
- legami costitutivi e criteri di progetto;
- le condizioni di carico;

La stampa dei risultati contiene:

- le combinazioni dei carichi;

- le forze sismiche agenti sulla struttura;
- le sollecitazioni sulle membrature per ogni combinazione di carico;
- la sollecitazione sul terreno sotto travi di fondazione o platee;
- deformate;
- diagrammi sollecitazioni.

Giudizio motivato dell'accettabilità dei risultati

La valutazione complessiva circa l'affidabilità dei risultati ottenuti dall'analisi automatica, è stata effettuata con il confronto con i risultati di semplici calcoli di larga massima, ottenuti con metodi tradizionali in forma analitica.

6. VERIFICHE

Per quanto riguarda le verifiche si rimanda al successivo "Tabulato dei calcoli".

TABULATO DEI CALCOLI

STRUTTURA PLATEA E PALCO

TABULATI DI INPUT

Dati generali

Nome struttura	Platea e palco
Fattore rigidità assiale pilastri	1
Numero di frequenze	120
% Filtro masse libere	0.1
% Coefficiente di smorzamento viscoso	5
Spostamenti modali con segno	Si
Deformabilità a taglio delle aste	Si
Spostamento ammissibile impalcati	0.0050*h

Impalcati

N°	Quota	Rigido	Incr.Soll.Pil	Inc.Soll.Par.
	mm			
0	0	No	1.000	1.000
1	120	Si	1.000	1.000
2	800	Si	1.000	1.000
3	1000	Si	1.000	1.000
4	1120	Si	1.000	1.000
5	1210	Si	1.000	1.000
6	1350	Si	1.000	1.000
7	1550	Si	1.000	1.000
8	1680	Si	1.000	1.000
9	1700	Si	1.000	1.000
10	1850	Si	1.000	1.000
11	2000	Si	1.000	1.000
12	2120	Si	1.000	1.000
13	2150	Si	1.000	1.000
14	2300	Si	1.000	1.000
15	2430	Si	1.000	1.000
16	2450	Si	1.000	1.000
17	2600	Si	1.000	1.000
18	2750	Si	1.000	1.000
19	2900	Si	1.000	1.000

Percentuali Spostamento masse impalcati

Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Combinazioni del Sisma in X e Y e Verticale

Comb	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
1	1	2	1	0.3	0
2	1	2	0.3	1	0
3	1	4	1	0.3	0
4	1	4	0.3	1	0

Comb	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
5	3	2	1	0.3	0
6	3	2	0.3	1	0
7	3	4	1	0.3	0
8	3	4	0.3	1	0

Comb. = Numero di combinazione dei sismi

Pos. SismaX = Posizione in cui viene scelto il sisma in direzione X

Pos. SismaY = Posizione in cui viene scelto il sisma in direzione Y

Fx = Fattore con cui il sisma X partecipa

Fy = Fattore con cui il sisma Y partecipa

Fz = Fattore con cui il sisma Verticale partecipa (quando richiesto)

Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz

Spettri di risposta

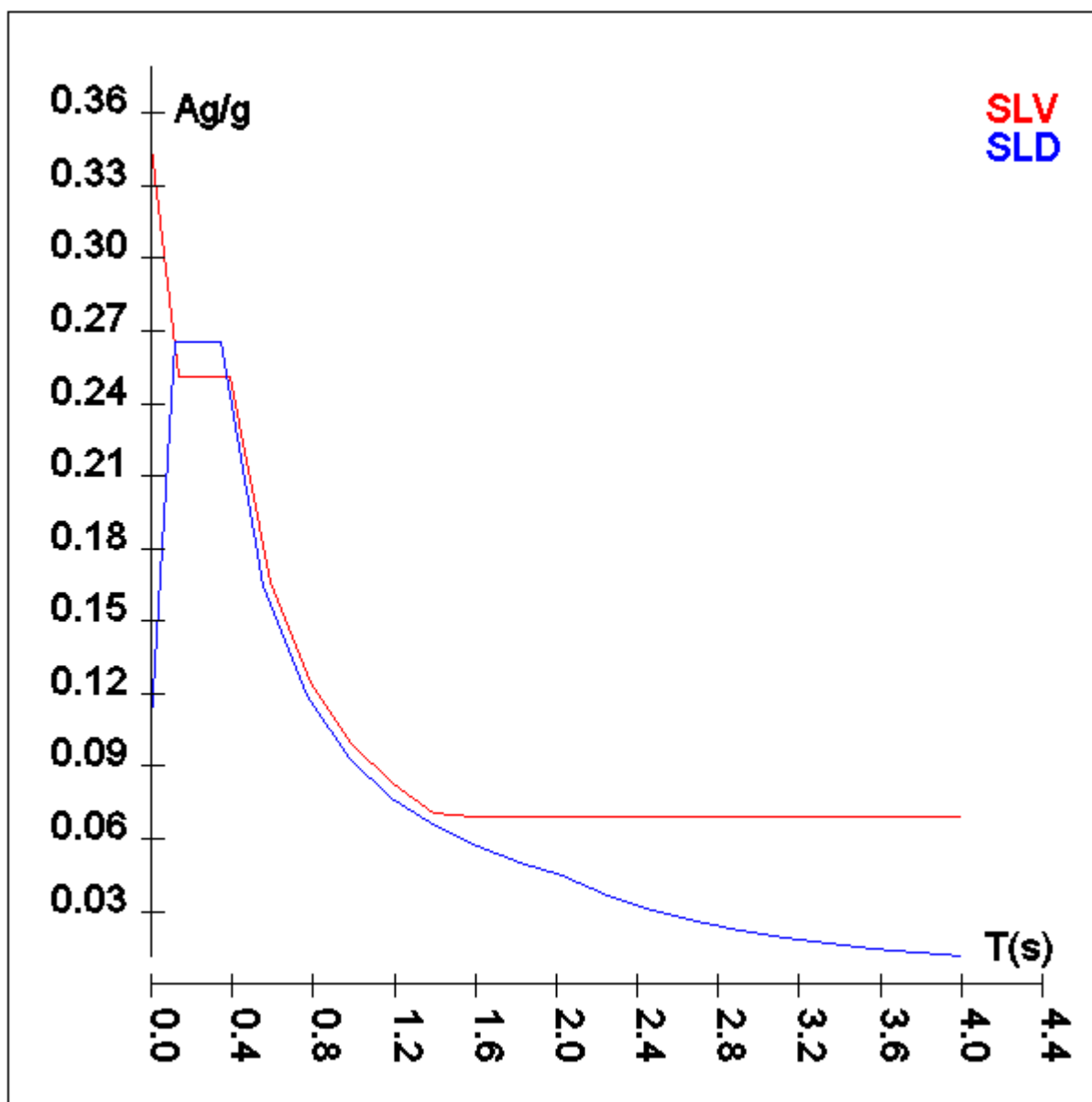
Spettro :SpettroNT

Il calcolo degli spettri e del fattore di struttura sono stati calcolati per la seguente tipologia di terreno e struttura

Vita della struttura	
Tipo	Opere ordinarie (50-100) 50 - 100 anni
Vita nominale(anni)	100.0
Classe d'uso	Classe IV
Coefficiente d'uso	2.000
Periodo di riferimento(anni)	200.000
Stato limite di esercizio - SLD	PVR=63.0%
Stato limite ultimo - SLV	PVR=10.0%
Periodo di ritorno SLD(anni)	TR=201.0
Periodo di ritorno SLV(anni)	TR=1898.2
Parametri del sito	
Comune	Andria - (BT)
Longitudine	16.2825
Latitudine	41.2216
Id reticolo del sito	31233-31455-31456-31234
Valori di riferimento del sito	
Ag/g(TR=201.0) SLD	0.1078
F0(TR=201.0) SLD	2.4612
T°C(TR=201.0) SLD	0.344
Ag/g(TR=1898.2) SLV	0.3465
F0(TR=1898.2) SLV	2.3179
T°C(TR=1898.2) SLV	0.392
Coefficiente Amplificazione Topografica	St=1.000
Categoria terreno A	
stato limite SLV	
	S=1.00
	TB=0.13
	TC=0.39
	TD=2.99
stato limite SLD	
	S=1.00
	TB=0.11
	TC=0.34
	TD=2.03
Fattore di struttura (SLV)	
Classe duttilità	B
Tipo struttura	Acciaio
Struttura non regolare in altezza	Kr=0.800000
	Kw=1.000
Regolare in pianta	NO (cfr.NTC7.3.1)
Tipologia : Strutture a telaio	Ce=4.000
Fattore di struttura $q=Kw*Kr*Ce$	3.200

TSLV [s]	SLV[a/g]	TSLD [s]	SLD[a/g]
0.00000	0.34645	0.00000	0.10785
0.13062	0.25095	0.11479	0.26544
0.39186	0.25095	0.34437	0.26544
0.59140	0.16628	0.55525	0.16463
0.79093	0.12433	0.76613	0.11932
0.99047	0.09929	0.97701	0.09356
1.19000	0.08264	1.18788	0.07695
1.38954	0.07077	1.39876	0.06535
1.58907	0.06929	1.60964	0.05679
1.78861	0.06929	1.82052	0.05021
1.98814	0.06929	2.03140	0.04500
2.18768	0.06929	2.25013	0.03668
2.38721	0.06929	2.46886	0.03046

2.58675	0.06929	2.68760	0.02571
2.78628	0.06929	2.90633	0.02198
2.98582	0.06929	3.12507	0.01901
3.23936	0.06929	3.34380	0.01661
3.49291	0.06929	3.56253	0.01463
3.74645	0.06929	3.78127	0.01299
4.00000	0.06929	4.00000	0.01161



Materiali

Materiale: Acciaio

Peso specifico	kg/mc	7850
Modulo di Young E	kg/cm ²	2E06
Modulo di Poisson ν		0.30
Coefficiente di dilatazione termica λ	1/°C	1.2e-005

Nodi - Geometria e vincoli

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
			Coordinate [mm]	Vincoli						
1	4220	11070	0	1	1	1	1	1	1	0
2	14950	11070	0	1	1	1	1	1	1	0
3	4650	11210	0	1	1	1	1	1	1	0
4	5170	11210	0	1	1	1	1	1	1	0
5	6370	11210	0	1	1	1	1	1	1	0
6	7570	11210	0	1	1	1	1	1	1	0
7	8770	11210	0	1	1	1	1	1	1	0
8	9970	11210	0	1	1	1	1	1	1	0
9	11170	11210	0	1	1	1	1	1	1	0
10	12370	11210	0	1	1	1	1	1	1	0
11	13570	11210	0	1	1	1	1	1	1	0
12	14560	11210	0	1	1	1	1	1	1	0
13	4650	12410	0	1	1	1	1	1	1	0
14	5170	12410	0	1	1	1	1	1	1	0
15	6370	12410	0	1	1	1	1	1	1	0
16	7570	12410	0	1	1	1	1	1	1	0
17	8770	12410	0	1	1	1	1	1	1	0
18	9970	12410	0	1	1	1	1	1	1	0
19	11170	12410	0	1	1	1	1	1	1	0
20	12370	12410	0	1	1	1	1	1	1	0
21	13570	12410	0	1	1	1	1	1	1	0
22	14560	12410	0	1	1	1	1	1	1	0
23	4650	13610	0	1	1	1	1	1	1	0
24	5170	13610	0	1	1	1	1	1	1	0
25	6370	13610	0	1	1	1	1	1	1	0
26	7570	13610	0	1	1	1	1	1	1	0
27	8770	13610	0	1	1	1	1	1	1	0
28	9970	13610	0	1	1	1	1	1	1	0
29	11170	13610	0	1	1	1	1	1	1	0
30	12370	13610	0	1	1	1	1	1	1	0
31	13570	13610	0	1	1	1	1	1	1	0
32	14560	13610	0	1	1	1	1	1	1	0
33	4650	14810	0	1	1	1	1	1	1	0
34	5170	14810	0	1	1	1	1	1	1	0
35	6370	14810	0	1	1	1	1	1	1	0
36	7570	14810	0	1	1	1	1	1	1	0
37	8770	14810	0	1	1	1	1	1	1	0
38	9970	14810	0	1	1	1	1	1	1	0
39	11170	14810	0	1	1	1	1	1	1	0
40	12370	14810	0	1	1	1	1	1	1	0
41	13570	14810	0	1	1	1	1	1	1	0
42	14560	14810	0	1	1	1	1	1	1	0
43	4650	16010	0	1	1	1	1	1	1	0
44	5170	16010	0	1	1	1	1	1	1	0
45	6370	16010	0	1	1	1	1	1	1	0
46	7570	16010	0	1	1	1	1	1	1	0
47	8770	16010	0	1	1	1	1	1	1	0
48	9970	16010	0	1	1	1	1	1	1	0
49	11170	16010	0	1	1	1	1	1	1	0
50	12370	16010	0	1	1	1	1	1	1	0
51	13570	16010	0	1	1	1	1	1	1	0
52	14560	16010	0	1	1	1	1	1	1	0
53	4650	17210	0	1	1	1	1	1	1	0
54	5170	17210	0	1	1	1	1	1	1	0
55	6370	17210	0	1	1	1	1	1	1	0
56	7570	17210	0	1	1	1	1	1	1	0
57	8770	17210	0	1	1	1	1	1	1	0
58	9970	17210	0	1	1	1	1	1	1	0
59	11170	17210	0	1	1	1	1	1	1	0
60	12370	17210	0	1	1	1	1	1	1	0
61	13570	17210	0	1	1	1	1	1	1	0

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
62	14560	17210	0	1	1	1	1	1	1	0
63	4650	18410	0	1	1	1	1	1	1	0
64	5170	18410	0	1	1	1	1	1	1	0
65	6370	18410	0	1	1	1	1	1	1	0
66	7570	18410	0	1	1	1	1	1	1	0
67	8770	18410	0	1	1	1	1	1	1	0
68	9970	18410	0	1	1	1	1	1	1	0
69	11170	18410	0	1	1	1	1	1	1	0
70	12370	18410	0	1	1	1	1	1	1	0
71	13570	18410	0	1	1	1	1	1	1	0
72	14560	18410	0	1	1	1	1	1	1	0
73	4650	19610	0	1	1	1	1	1	1	0
74	5170	19610	0	1	1	1	1	1	1	0
75	6370	19610	0	1	1	1	1	1	1	0
76	7570	19610	0	1	1	1	1	1	1	0
77	8770	19610	0	1	1	1	1	1	1	0
78	9970	19610	0	1	1	1	1	1	1	0
79	11170	19610	0	1	1	1	1	1	1	0
80	12370	19610	0	1	1	1	1	1	1	0
81	13570	19610	0	1	1	1	1	1	1	0
82	14560	19610	0	1	1	1	1	1	1	0
83	4650	20650	0	1	1	1	1	1	1	0
84	5170	20650	0	1	1	1	1	1	1	0
85	6370	20650	0	1	1	1	1	1	1	0
86	7570	20650	0	1	1	1	1	1	1	0
87	8770	20650	0	1	1	1	1	1	1	0
88	9970	20650	0	1	1	1	1	1	1	0
89	11170	20650	0	1	1	1	1	1	1	0
90	12370	20650	0	1	1	1	1	1	1	0
91	13570	20650	0	1	1	1	1	1	1	0
92	14560	20650	0	1	1	1	1	1	1	0
10004	5170	11210	120	0	0	0	0	0	0	1
10005	6370	11210	120	0	0	0	0	0	0	1
10006	7570	11210	120	0	0	0	0	0	0	1
10007	8770	11210	120	0	0	0	0	0	0	1
10008	9970	11210	120	0	0	0	0	0	0	1
10009	11170	11210	120	0	0	0	0	0	0	1
10010	12370	11210	120	0	0	0	0	0	0	1
10011	13570	11210	120	0	0	0	0	0	0	1
10014	5170	12410	120	0	0	0	0	0	0	1
10017	8770	12410	120	0	0	0	0	0	0	1
10018	9970	12410	120	0	0	0	0	0	0	1
10021	13570	12410	120	0	0	0	0	0	0	1
10024	5170	13610	120	0	0	0	0	0	0	1
10027	8770	13610	120	0	0	0	0	0	0	1
10028	9970	13610	120	0	0	0	0	0	0	1
10031	13570	13610	120	0	0	0	0	0	0	1
10034	5170	14810	120	0	0	0	0	0	0	1
10035	6370	14810	120	0	0	0	0	0	0	1
10036	7570	14810	120	0	0	0	0	0	0	1
10037	8770	14810	120	0	0	0	0	0	0	1
10038	9970	14810	120	0	0	0	0	0	0	1
10039	11170	14810	120	0	0	0	0	0	0	1
10040	12370	14810	120	0	0	0	0	0	0	1
10041	13570	14810	120	0	0	0	0	0	0	1
10044	5170	16010	120	0	0	0	0	0	0	1
10045	6370	16010	120	0	0	0	0	0	0	1
10046	7570	16010	120	0	0	0	0	0	0	1
10047	8770	16010	120	0	0	0	0	0	0	1
10048	9970	16010	120	0	0	0	0	0	0	1
10049	11170	16010	120	0	0	0	0	0	0	1
10050	12370	16010	120	0	0	0	0	0	0	1
10051	13570	16010	120	0	0	0	0	0	0	1
10054	5170	17210	120	0	0	0	0	0	0	1
10057	8770	17210	120	0	0	0	0	0	0	1
10058	9970	17210	120	0	0	0	0	0	0	1
10061	13570	17210	120	0	0	0	0	0	0	1
10064	5170	18410	120	0	0	0	0	0	0	1
10067	8770	18410	120	0	0	0	0	0	0	1
10068	9970	18410	120	0	0	0	0	0	0	1
10071	13570	18410	120	0	0	0	0	0	0	1
10074	5170	19610	120	0	0	0	0	0	0	1
10075	6370	19610	120	0	0	0	0	0	0	1
10076	7570	19610	120	0	0	0	0	0	0	1
10077	8770	19610	120	0	0	0	0	0	0	1
10078	9970	19610	120	0	0	0	0	0	0	1
10079	11170	19610	120	0	0	0	0	0	0	1
10080	12370	19610	120	0	0	0	0	0	0	1
10081	13570	19610	120	0	0	0	0	0	0	1

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
11498	11320	7550	700	1	1	1	1	1	1	2
11499	11320	8450	530	1	1	1	1	1	1	2
11500	11320	9350	360	1	1	1	1	1	1	2
11501	10160	7550	700	1	1	1	1	1	1	2
11502	10160	8450	530	1	1	1	1	1	1	2
11503	10160	9350	360	1	1	1	1	1	1	2
11504	9000	7550	700	1	1	1	1	1	1	2
11505	9000	8450	530	1	1	1	1	1	1	2
11506	9000	9350	360	1	1	1	1	1	1	2
11507	7840	7550	700	1	1	1	1	1	1	2
11508	7840	8450	530	1	1	1	1	1	1	2
11509	7840	9350	360	1	1	1	1	1	1	2
11510	11170	10010	240	1	1	1	1	1	1	2
11511	12370	10010	240	1	1	1	1	1	1	2
11512	13570	10010	240	1	1	1	1	1	1	2
11513	14560	10010	240	1	1	1	1	1	1	2
11514	9970	10010	240	1	1	1	1	1	1	2
11515	8770	10010	240	1	1	1	1	1	1	2
11516	7570	10010	240	1	1	1	1	1	1	2
11517	6370	10010	240	1	1	1	1	1	1	2
11518	5170	10010	240	1	1	1	1	1	1	2
11519	4650	10010	240	1	1	1	1	1	1	2
11520	11410	8460	530	1	1	1	1	1	1	2
11521	14669	9682	530	1	1	1	1	1	1	2
11522	14984	8839	700	1	1	1	1	1	1	2
11523	13898	8432	700	1	1	1	1	1	1	2
11524	13582	9274	530	1	1	1	1	1	1	2
11525	12812	8024	700	1	1	1	1	1	1	2
11526	12496	8867	530	1	1	1	1	1	1	2
11527	11726	7617	700	1	1	1	1	1	1	2
11528	7760	8470	530	1	1	1	1	1	1	2
11529	4189	8882	700	1	1	1	1	1	1	2
11530	5595	9304	530	1	1	1	1	1	1	2
11531	7436	7630	700	1	1	1	1	1	1	2
11532	5272	8465	700	1	1	1	1	1	1	2
11533	4513	9722	530	1	1	1	1	1	1	2
11534	6354	8047	700	1	1	1	1	1	1	2
11535	6678	8887	530	1	1	1	1	1	1	2
11536	3670	10490	530	1	1	1	1	1	1	2
11537	3050	9820	700	1	1	1	1	1	1	2
11538	15530	10450	530	1	1	1	1	1	1	2
11539	16150	9780	700	1	1	1	1	1	1	2
11540	14750	9730	530	1	1	1	1	1	1	2
11541	15370	9060	700	1	1	1	1	1	1	2
11542	4450	9760	530	1	1	1	1	1	1	2
11543	3830	9090	700	1	1	1	1	1	1	2
20770	7840	8450	800	0	0	0	0	0	0	2
20773	9000	8450	800	0	0	0	0	0	0	2
20776	10160	8450	800	0	0	0	0	0	0	2
20779	11320	8450	800	0	0	0	0	0	0	2
20782	11410	8460	800	0	0	0	0	0	0	2
20790	7760	8470	800	0	0	0	0	0	0	2
20802	12496	8867	800	0	0	0	0	0	0	2
20809	6678	8887	800	0	0	0	0	0	0	2
20821	13582	9274	800	0	0	0	0	0	0	2
20825	5595	9304	800	0	0	0	0	0	0	2
20828	7840	9350	800	0	0	0	0	0	0	2
20830	9000	9350	800	0	0	0	0	0	0	2
20832	10160	9350	800	0	0	0	0	0	0	2
20834	11320	9350	800	0	0	0	0	0	0	2
20844	14669	9682	800	0	0	0	0	0	0	2
20847	4513	9722	800	0	0	0	0	0	0	2
20854	4650	10010	800	0	0	0	0	0	0	2
20855	5170	10010	800	0	0	0	0	0	0	2
20856	6370	10010	800	0	0	0	0	0	0	2
20857	7570	10010	800	0	0	0	0	0	0	2
20858	8770	10010	800	0	0	0	0	0	0	2
20859	9970	10010	800	0	0	0	0	0	0	2
20860	11170	10010	800	0	0	0	0	0	0	2
20861	12370	10010	800	0	0	0	0	0	0	2
20862	13570	10010	800	0	0	0	0	0	0	2
20863	14560	10010	800	0	0	0	0	0	0	2
21498	11320	6650	870	1	1	1	1	1	1	3
21499	10160	6650	870	1	1	1	1	1	1	3
21500	9000	6650	870	1	1	1	1	1	1	3
21501	7840	6650	870	1	1	1	1	1	1	3
21502	15300	7996	870	1	1	1	1	1	1	3
21503	14214	7589	870	1	1	1	1	1	1	3
21504	13128	7182	870	1	1	1	1	1	1	3

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
21505	12042	6775	870	1	1	1	1	1	1	3
21506	3865	8042	870	1	1	1	1	1	1	3
21507	7113	6790	870	1	1	1	1	1	1	3
21508	4948	7625	870	1	1	1	1	1	1	3
21509	6030	7208	870	1	1	1	1	1	1	3
21510	2430	9160	870	1	1	1	1	1	1	3
21511	16770	9110	870	1	1	1	1	1	1	3
21512	15990	8390	870	1	1	1	1	1	1	3
21513	3210	8430	870	1	1	1	1	1	1	3
30635	7840	6650	1000	0	0	0	0	0	0	3
30638	9000	6650	1000	0	0	0	0	0	0	3
30641	10160	6650	1000	0	0	0	0	0	0	3
30644	11320	6650	1000	0	0	0	0	0	0	3
30653	12042	6775	1000	0	0	0	0	0	0	3
30662	7113	6790	1000	0	0	0	0	0	0	3
30687	13128	7182	1000	0	0	0	0	0	0	3
30695	6030	7208	1000	0	0	0	0	0	0	3
30704	7840	7550	1000	0	0	0	0	0	0	3
30707	9000	7550	1000	0	0	0	0	0	0	3
30710	10160	7550	1000	0	0	0	0	0	0	3
30713	11320	7550	1000	0	0	0	0	0	0	3
30718	14214	7589	1000	0	0	0	0	0	0	3
30722	11726	7617	1000	0	0	0	0	0	0	3
30726	4948	7625	1000	0	0	0	0	0	0	3
30731	7436	7630	1000	0	0	0	0	0	0	3
30738	15300	7996	1000	0	0	0	0	0	0	3
30746	12812	8024	1000	0	0	0	0	0	0	3
30750	3865	8042	1000	0	0	0	0	0	0	3
30754	6354	8047	1000	0	0	0	0	0	0	3
30762	15990	8390	1000	0	0	0	0	0	0	3
30764	3210	8430	1000	0	0	0	0	0	0	3
30765	13898	8432	1000	0	0	0	0	0	0	3
30786	5272	8465	1000	0	0	0	0	0	0	3
30798	14984	8839	1000	0	0	0	0	0	0	3
30805	4189	8882	1000	0	0	0	0	0	0	3
30816	15370	9060	1000	0	0	0	0	0	0	3
30817	3830	9090	1000	0	0	0	0	0	0	3
31498	11320	5750	1040	1	1	1	1	1	1	4
31499	10160	5750	1040	1	1	1	1	1	1	4
31500	9000	5750	1040	1	1	1	1	1	1	4
31501	7840	5750	1040	1	1	1	1	1	1	4
31502	15616	7153	1040	1	1	1	1	1	1	4
31503	14530	6746	1040	1	1	1	1	1	1	4
31504	13444	6339	1040	1	1	1	1	1	1	4
31505	12358	5932	1040	1	1	1	1	1	1	4
31506	5707	6368	1040	1	1	1	1	1	1	4
31507	4624	6785	1040	1	1	1	1	1	1	4
31508	3542	7202	1040	1	1	1	1	1	1	4
31509	6789	5951	1040	1	1	1	1	1	1	4
31510	1800	8500	1040	1	1	1	1	1	1	4
31511	17390	8450	1040	1	1	1	1	1	1	4
31512	16610	7730	1040	1	1	1	1	1	1	4
31513	2580	7770	1040	1	1	1	1	1	1	4
40004	5170	11210	1120	0	0	0	0	0	0	4
40005	6370	11210	1120	0	0	0	0	0	0	4
40006	7570	11210	1120	0	0	0	0	0	0	4
40007	8770	11210	1120	0	0	0	0	0	0	4
40008	9970	11210	1120	0	0	0	0	0	0	4
40009	11170	11210	1120	0	0	0	0	0	0	4
40010	12370	11210	1120	0	0	0	0	0	0	4
40011	13570	11210	1120	0	0	0	0	0	0	4
40014	5170	12410	1120	0	0	0	0	0	0	4
40015	6370	12410	1120	0	0	0	0	0	0	4
40016	7570	12410	1120	0	0	0	0	0	0	4
40017	8770	12410	1120	0	0	0	0	0	0	4
40018	9970	12410	1120	0	0	0	0	0	0	4
40019	11170	12410	1120	0	0	0	0	0	0	4
40020	12370	12410	1120	0	0	0	0	0	0	4
40021	13570	12410	1120	0	0	0	0	0	0	4
40024	5170	13610	1120	0	0	0	0	0	0	4
40025	6370	13610	1120	0	0	0	0	0	0	4
40026	7570	13610	1120	0	0	0	0	0	0	4
40027	8770	13610	1120	0	0	0	0	0	0	4
40028	9970	13610	1120	0	0	0	0	0	0	4
40029	11170	13610	1120	0	0	0	0	0	0	4
40030	12370	13610	1120	0	0	0	0	0	0	4
40031	13570	13610	1120	0	0	0	0	0	0	4
40034	5170	14810	1120	0	0	0	0	0	0	4
40035	6370	14810	1120	0	0	0	0	0	0	4

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
40036	7570	14810	1120	0	0	0	0	0	0	4
40037	8770	14810	1120	0	0	0	0	0	0	4
40038	9970	14810	1120	0	0	0	0	0	0	4
40039	11170	14810	1120	0	0	0	0	0	0	4
40040	12370	14810	1120	0	0	0	0	0	0	4
40041	13570	14810	1120	0	0	0	0	0	0	4
40044	5170	16010	1120	0	0	0	0	0	0	4
40045	6370	16010	1120	0	0	0	0	0	0	4
40046	7570	16010	1120	0	0	0	0	0	0	4
40047	8770	16010	1120	0	0	0	0	0	0	4
40048	9970	16010	1120	0	0	0	0	0	0	4
40049	11170	16010	1120	0	0	0	0	0	0	4
40050	12370	16010	1120	0	0	0	0	0	0	4
40051	13570	16010	1120	0	0	0	0	0	0	4
40054	5170	17210	1120	0	0	0	0	0	0	4
40055	6370	17210	1120	0	0	0	0	0	0	4
40056	7570	17210	1120	0	0	0	0	0	0	4
40057	8770	17210	1120	0	0	0	0	0	0	4
40058	9970	17210	1120	0	0	0	0	0	0	4
40059	11170	17210	1120	0	0	0	0	0	0	4
40060	12370	17210	1120	0	0	0	0	0	0	4
40061	13570	17210	1120	0	0	0	0	0	0	4
40064	5170	18410	1120	0	0	0	0	0	0	4
40065	6370	18410	1120	0	0	0	0	0	0	4
40066	7570	18410	1120	0	0	0	0	0	0	4
40067	8770	18410	1120	0	0	0	0	0	0	4
40068	9970	18410	1120	0	0	0	0	0	0	4
40069	11170	18410	1120	0	0	0	0	0	0	4
40070	12370	18410	1120	0	0	0	0	0	0	4
40071	13570	18410	1120	0	0	0	0	0	0	4
40074	5170	19610	1120	0	0	0	0	0	0	4
40075	6370	19610	1120	0	0	0	0	0	0	4
40076	7570	19610	1120	0	0	0	0	0	0	4
40077	8770	19610	1120	0	0	0	0	0	0	4
40078	9970	19610	1120	0	0	0	0	0	0	4
40079	11170	19610	1120	0	0	0	0	0	0	4
40080	12370	19610	1120	0	0	0	0	0	0	4
40081	13570	19610	1120	0	0	0	0	0	0	4
50445	7840	4850	1210	1	1	1	1	1	1	5
50449	9000	4850	1210	1	1	1	1	1	1	5
50453	10160	4850	1210	1	1	1	1	1	1	5
50457	11320	4850	1210	1	1	1	1	1	1	5
50466	11430	4880	1210	1	1	1	1	1	1	5
50470	7690	4900	1210	1	1	1	1	1	1	5
50486	12572	5085	1210	1	1	1	1	1	1	5
50490	12674	5089	1210	1	1	1	1	1	1	5
50499	6465	5111	1210	1	1	1	1	1	1	5
50503	6550	5117	1210	1	1	1	1	1	1	5
50527	13760	5496	1210	1	1	1	1	1	1	5
50540	5383	5528	1210	1	1	1	1	1	1	5
50570	14846	5903	1210	1	1	1	1	1	1	5
50580	4300	5945	1210	1	1	1	1	1	1	5
50603	15932	6311	1210	1	1	1	1	1	1	5
50612	3218	6363	1210	1	1	1	1	1	1	5
50622	16076	6393	1210	1	1	1	1	1	1	5
50626	3080	6435	1210	1	1	1	1	1	1	5
50668	17067	6994	1210	1	1	1	1	1	1	5
50672	2092	7045	1210	1	1	1	1	1	1	5
50676	17230	7060	1210	1	1	1	1	1	1	5
50682	1970	7110	1210	1	1	1	1	1	1	5
50717	1050	7580	1210	1	1	1	1	1	1	5
50736	18010	7780	1210	1	1	1	1	1	1	5
50737	1190	7840	1210	1	1	1	1	1	1	5
60445	7840	4850	1350	0	0	0	0	0	0	6
60449	9000	4850	1350	0	0	0	0	0	0	6
60453	10160	4850	1350	0	0	0	0	0	0	6
60457	11320	4850	1350	0	0	0	0	0	0	6
60466	11430	4880	1350	0	0	0	0	0	0	6
60470	7690	4900	1350	0	0	0	0	0	0	6
60486	12572	5085	1350	0	0	0	0	0	0	6
60490	12674	5089	1350	0	0	0	0	0	0	6
60499	6465	5111	1350	0	0	0	0	0	0	6
60503	6550	5117	1350	0	0	0	0	0	0	6
60527	13760	5496	1350	0	0	0	0	0	0	6
60540	5383	5528	1350	0	0	0	0	0	0	6
60554	7840	5750	1350	0	0	0	0	0	0	6
60557	9000	5750	1350	0	0	0	0	0	0	6
60560	10160	5750	1350	0	0	0	0	0	0	6
60563	11320	5750	1350	0	0	0	0	0	0	6

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
60570	14846	5903	1350	0	0	0	0	0	0	6
60576	12358	5932	1350	0	0	0	0	0	0	6
60580	4300	5945	1350	0	0	0	0	0	0	6
60585	6789	5951	1350	0	0	0	0	0	0	6
60603	15932	6311	1350	0	0	0	0	0	0	6
60608	13444	6339	1350	0	0	0	0	0	0	6
60612	3218	6363	1350	0	0	0	0	0	0	6
60617	5707	6368	1350	0	0	0	0	0	0	6
60622	16076	6393	1350	0	0	0	0	0	0	6
60626	3080	6435	1350	0	0	0	0	0	0	6
60649	14530	6746	1350	0	0	0	0	0	0	6
60658	4624	6785	1350	0	0	0	0	0	0	6
60668	17067	6994	1350	0	0	0	0	0	0	6
60672	2092	7045	1350	0	0	0	0	0	0	6
60676	17230	7060	1350	0	0	0	0	0	0	6
60682	1970	7110	1350	0	0	0	0	0	0	6
60683	15616	7153	1350	0	0	0	0	0	0	6
60691	3542	7202	1350	0	0	0	0	0	0	6
60734	16610	7730	1350	0	0	0	0	0	0	6
60735	2580	7770	1350	0	0	0	0	0	0	6
61498	11320	3950	1380	1	1	1	1	1	1	7
61499	10160	3950	1380	1	1	1	1	1	1	7
61500	9000	3950	1380	1	1	1	1	1	1	7
61501	7840	3950	1380	1	1	1	1	1	1	7
61502	16248	5468	1380	1	1	1	1	1	1	7
61503	15162	5061	1380	1	1	1	1	1	1	7
61504	14076	4654	1380	1	1	1	1	1	1	7
61505	12990	4246	1380	1	1	1	1	1	1	7
61506	5059	4688	1380	1	1	1	1	1	1	7
61507	3977	5106	1380	1	1	1	1	1	1	7
61508	2894	5523	1380	1	1	1	1	1	1	7
61509	6141	4271	1380	1	1	1	1	1	1	7
61510	12731	4199	1380	1	1	1	1	1	1	7
61511	11589	3994	1380	1	1	1	1	1	1	7
61512	7522	4016	1380	1	1	1	1	1	1	7
61513	6382	4233	1380	1	1	1	1	1	1	7
61514	16542	5623	1380	1	1	1	1	1	1	7
61515	17534	6225	1380	1	1	1	1	1	1	7
61516	1620	6279	1380	1	1	1	1	1	1	7
61517	2607	5669	1380	1	1	1	1	1	1	7
61518	18620	7110	1380	1	1	1	1	1	1	7
61519	17840	6390	1380	1	1	1	1	1	1	7
61520	630	6900	1380	1	1	1	1	1	1	7
70001	4220	11070	1550	0	0	0	0	0	0	7
70002	14950	11070	1550	0	0	0	0	0	0	7
70003	4650	11210	1550	0	0	0	0	0	0	7
70004	5170	11210	1550	0	0	0	0	0	0	7
70005	6370	11210	1550	0	0	0	0	0	0	7
70006	7570	11210	1550	0	0	0	0	0	0	7
70007	8770	11210	1550	0	0	0	0	0	0	7
70008	9970	11210	1550	0	0	0	0	0	0	7
70009	11170	11210	1550	0	0	0	0	0	0	7
70010	12370	11210	1550	0	0	0	0	0	0	7
70011	13570	11210	1550	0	0	0	0	0	0	7
70012	14560	11210	1550	0	0	0	0	0	0	7
70262	7840	3050	1550	1	1	1	1	1	1	7
70266	9000	3050	1550	1	1	1	1	1	1	7
70270	10160	3050	1550	1	1	1	1	1	1	7
70274	11320	3050	1550	1	1	1	1	1	1	7
70279	11748	3108	1550	1	1	1	1	1	1	7
70283	7354	3132	1550	1	1	1	1	1	1	7
70290	12890	3314	1550	1	1	1	1	1	1	7
70294	6214	3348	1550	1	1	1	1	1	1	7
70303	13306	3404	1550	1	1	1	1	1	1	7
70312	5818	3431	1550	1	1	1	1	1	1	7
70333	14392	3811	1550	1	1	1	1	1	1	7
70346	4735	3849	1550	1	1	1	1	1	1	7
70384	15478	4218	1550	1	1	1	1	1	1	7
70396	3653	4266	1550	1	1	1	1	1	1	7
70418	16564	4625	1550	1	1	1	1	1	1	7
70429	2571	4683	1550	1	1	1	1	1	1	7
70461	17009	4854	1550	1	1	1	1	1	1	7
70474	2134	4904	1550	1	1	1	1	1	1	7
70518	18001	5455	1550	1	1	1	1	1	1	7
70532	1147	5513	1550	1	1	1	1	1	1	7
70553	18460	5720	1550	1	1	1	1	1	1	7
70592	160	6130	1550	1	1	1	1	1	1	7
70630	19240	6440	1550	1	1	1	1	1	1	7
70770	7840	8450	1550	0	0	0	0	0	0	7

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
70773	9000	8450	1550	0	0	0	0	0	0	7
70776	10160	8450	1550	0	0	0	0	0	0	7
70779	11320	8450	1550	0	0	0	0	0	0	7
70782	11410	8460	1550	0	0	0	0	0	0	7
70790	7760	8470	1550	0	0	0	0	0	0	7
70802	12496	8867	1550	0	0	0	0	0	0	7
70809	6678	8887	1550	0	0	0	0	0	0	7
70812	7840	8900	1550	0	0	0	0	0	0	7
70813	9000	8900	1550	0	0	0	0	0	0	7
70814	10160	8900	1550	0	0	0	0	0	0	7
70815	11320	8900	1550	0	0	0	0	0	0	7
70821	13582	9274	1550	0	0	0	0	0	0	7
70825	5595	9304	1550	0	0	0	0	0	0	7
70828	7840	9350	1550	0	0	0	0	0	0	7
70830	9000	9350	1550	0	0	0	0	0	0	7
70832	10160	9350	1550	0	0	0	0	0	0	7
70834	11320	9350	1550	0	0	0	0	0	0	7
70838	12278	9439	1550	0	0	0	0	0	0	7
70840	6894	9449	1550	0	0	0	0	0	0	7
70842	13441	9642	1550	0	0	0	0	0	0	7
70843	5733	9657	1550	0	0	0	0	0	0	7
70844	14669	9682	1550	0	0	0	0	0	0	7
70847	4513	9722	1550	0	0	0	0	0	0	7
70850	14750	9730	1550	0	0	0	0	0	0	7
70851	4450	9760	1550	0	0	0	0	0	0	7
70854	4650	10010	1550	0	0	0	0	0	0	7
70855	5170	10010	1550	0	0	0	0	0	0	7
70856	6370	10010	1550	0	0	0	0	0	0	7
70857	7570	10010	1550	0	0	0	0	0	0	7
70858	8770	10010	1550	0	0	0	0	0	0	7
70859	9970	10010	1550	0	0	0	0	0	0	7
70860	11170	10010	1550	0	0	0	0	0	0	7
70861	12370	10010	1550	0	0	0	0	0	0	7
70862	13570	10010	1550	0	0	0	0	0	0	7
70863	14560	10010	1550	0	0	0	0	0	0	7
70866	5870	10010	1550	0	0	0	0	0	0	7
70868	7110	10010	1550	0	0	0	0	0	0	7
70870	7840	10010	1550	0	0	0	0	0	0	7
70872	9000	10010	1550	0	0	0	0	0	0	7
70874	10160	10010	1550	0	0	0	0	0	0	7
70876	11320	10010	1550	0	0	0	0	0	0	7
70877	12060	10010	1550	0	0	0	0	0	0	7
70879	13300	10010	1550	0	0	0	0	0	0	7
70884	5170	10410	1550	0	0	0	0	0	0	7
70885	6370	10410	1550	0	0	0	0	0	0	7
70886	7570	10410	1550	0	0	0	0	0	0	7
70887	8770	10410	1550	0	0	0	0	0	0	7
70888	9970	10410	1550	0	0	0	0	0	0	7
70889	11170	10410	1550	0	0	0	0	0	0	7
70890	12370	10410	1550	0	0	0	0	0	0	7
70891	13570	10410	1550	0	0	0	0	0	0	7
70892	4650	10410	1550	0	0	0	0	0	0	7
70893	14560	10410	1550	0	0	0	0	0	0	7
70894	15530	10450	1550	0	0	0	0	0	0	7
70895	3670	10490	1550	0	0	0	0	0	0	7
70896	15240	10760	1550	0	0	0	0	0	0	7
70897	3945	10780	1550	0	0	0	0	0	0	7
70898	5170	10810	1550	0	0	0	0	0	0	7
70899	6370	10810	1550	0	0	0	0	0	0	7
70900	7570	10810	1550	0	0	0	0	0	0	7
70901	8770	10810	1550	0	0	0	0	0	0	7
70902	9970	10810	1550	0	0	0	0	0	0	7
70903	11170	10810	1550	0	0	0	0	0	0	7
70904	12370	10810	1550	0	0	0	0	0	0	7
70905	13570	10810	1550	0	0	0	0	0	0	7
70906	4650	10810	1550	0	0	0	0	0	0	7
70907	14560	10810	1550	0	0	0	0	0	0	7
70908	4650	11070	1550	0	0	0	0	0	0	7
70909	14560	11070	1550	0	0	0	0	0	0	7
71498	942	5181	1620	1	1	1	1	1	1	8
80262	7840	3050	1680	0	0	0	0	0	0	8
80266	9000	3050	1680	0	0	0	0	0	0	8
80270	10160	3050	1680	0	0	0	0	0	0	8
80274	11320	3050	1680	0	0	0	0	0	0	8
80279	11748	3108	1680	0	0	0	0	0	0	8
80283	7354	3132	1680	0	0	0	0	0	0	8
80290	12890	3314	1680	0	0	0	0	0	0	8
80294	6214	3348	1680	0	0	0	0	0	0	8
80303	13306	3404	1680	0	0	0	0	0	0	8

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
80312	5818	3431	1680	0	0	0	0	0	0	8
80333	14392	3811	1680	0	0	0	0	0	0	8
80346	4735	3849	1680	0	0	0	0	0	0	8
80351	7840	3950	1680	0	0	0	0	0	0	8
80354	9000	3950	1680	0	0	0	0	0	0	8
80357	10160	3950	1680	0	0	0	0	0	0	8
80360	11320	3950	1680	0	0	0	0	0	0	8
80363	11589	3994	1680	0	0	0	0	0	0	8
80367	7522	4016	1680	0	0	0	0	0	0	8
80378	12731	4199	1680	0	0	0	0	0	0	8
80384	15478	4218	1680	0	0	0	0	0	0	8
80389	6382	4233	1680	0	0	0	0	0	0	8
80392	12990	4246	1680	0	0	0	0	0	0	8
80396	3653	4266	1680	0	0	0	0	0	0	8
80401	6141	4271	1680	0	0	0	0	0	0	8
80418	16564	4625	1680	0	0	0	0	0	0	8
80424	14076	4654	1680	0	0	0	0	0	0	8
80429	2571	4683	1680	0	0	0	0	0	0	8
80437	5059	4688	1680	0	0	0	0	0	0	8
80461	17009	4854	1680	0	0	0	0	0	0	8
80474	2134	4904	1680	0	0	0	0	0	0	8
80481	15162	5061	1680	0	0	0	0	0	0	8
80495	3977	5106	1680	0	0	0	0	0	0	8
80518	18001	5455	1680	0	0	0	0	0	0	8
80522	16248	5468	1680	0	0	0	0	0	0	8
80532	1147	5513	1680	0	0	0	0	0	0	8
80536	2894	5523	1680	0	0	0	0	0	0	8
80546	16542	5623	1680	0	0	0	0	0	0	8
80550	2607	5669	1680	0	0	0	0	0	0	8
80553	18460	5720	1680	0	0	0	0	0	0	8
80597	17534	6225	1680	0	0	0	0	0	0	8
80600	1620	6279	1680	0	0	0	0	0	0	8
80621	17840	6390	1680	0	0	0	0	0	0	8
90704	7840	7550	1700	0	0	0	0	0	0	9
90707	9000	7550	1700	0	0	0	0	0	0	9
90710	10160	7550	1700	0	0	0	0	0	0	9
90713	11320	7550	1700	0	0	0	0	0	0	9
90722	11726	7617	1700	0	0	0	0	0	0	9
90731	7436	7630	1700	0	0	0	0	0	0	9
90741	7840	8000	1700	0	0	0	0	0	0	9
90742	9000	8000	1700	0	0	0	0	0	0	9
90743	10160	8000	1700	0	0	0	0	0	0	9
90744	11320	8000	1700	0	0	0	0	0	0	9
90746	12812	8024	1700	0	0	0	0	0	0	9
90749	11568	8039	1700	0	0	0	0	0	0	9
90754	6354	8047	1700	0	0	0	0	0	0	9
90757	7598	8050	1700	0	0	0	0	0	0	9
90765	13898	8432	1700	0	0	0	0	0	0	9
90768	12654	8446	1700	0	0	0	0	0	0	9
90770	7840	8450	1700	0	0	0	0	0	0	9
90773	9000	8450	1700	0	0	0	0	0	0	9
90776	10160	8450	1700	0	0	0	0	0	0	9
90779	11320	8450	1700	0	0	0	0	0	0	9
90782	11410	8460	1700	0	0	0	0	0	0	9
90786	5272	8465	1700	0	0	0	0	0	0	9
90789	6516	8467	1700	0	0	0	0	0	0	9
90790	7760	8470	1700	0	0	0	0	0	0	9
90798	14984	8839	1700	0	0	0	0	0	0	9
90801	13740	8853	1700	0	0	0	0	0	0	9
90802	12496	8867	1700	0	0	0	0	0	0	9
90805	4189	8882	1700	0	0	0	0	0	0	9
90808	5433	8885	1700	0	0	0	0	0	0	9
90809	6678	8887	1700	0	0	0	0	0	0	9
90816	15370	9060	1700	0	0	0	0	0	0	9
90817	3830	9090	1700	0	0	0	0	0	0	9
90820	14827	9260	1700	0	0	0	0	0	0	9
90821	13582	9274	1700	0	0	0	0	0	0	9
90824	4351	9302	1700	0	0	0	0	0	0	9
90825	5595	9304	1700	0	0	0	0	0	0	9
90836	15060	9395	1700	0	0	0	0	0	0	9
90837	4140	9425	1700	0	0	0	0	0	0	9
90844	14669	9682	1700	0	0	0	0	0	0	9
90847	4513	9722	1700	0	0	0	0	0	0	9
90850	14750	9730	1700	0	0	0	0	0	0	9
90851	4450	9760	1700	0	0	0	0	0	0	9
90852	16150	9780	1700	0	0	0	0	0	0	9
90853	3050	9820	1700	0	0	0	0	0	0	9
90882	15840	10115	1700	0	0	0	0	0	0	9
90883	3360	10155	1700	0	0	0	0	0	0	9

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
90894	15530	10450	1700	0	0	0	0	0	0	9
90895	3670	10490	1700	0	0	0	0	0	0	9
91498	11320	2150	1720	1	1	1	1	1	1	10
91499	10160	2150	1720	1	1	1	1	1	1	10
91500	9000	2150	1720	1	1	1	1	1	1	10
91501	7840	2150	1720	1	1	1	1	1	1	10
91502	16880	3782	1720	1	1	1	1	1	1	10
91503	15794	3375	1720	1	1	1	1	1	1	10
91504	14708	2968	1720	1	1	1	1	1	1	10
91505	13621	2561	1720	1	1	1	1	1	1	10
91506	4412	3009	1720	1	1	1	1	1	1	10
91507	3329	3426	1720	1	1	1	1	1	1	10
91508	2247	3843	1720	1	1	1	1	1	1	10
91509	5494	2592	1720	1	1	1	1	1	1	10
91510	13049	2428	1720	1	1	1	1	1	1	10
91511	11908	2223	1720	1	1	1	1	1	1	10
91512	7185	2248	1720	1	1	1	1	1	1	10
91513	6046	2464	1720	1	1	1	1	1	1	10
91514	17475	4084	1720	1	1	1	1	1	1	10
91515	18467	4685	1720	1	1	1	1	1	1	10
91516	17772	3614	1830	1	1	1	1	1	1	10
91517	18764	4206	1830	1	1	1	1	1	1	10
91518	1662	4138	1720	1	1	1	1	1	1	10
91519	19860	5780	1720	1	1	1	1	1	1	10
91520	19080	5060	1720	1	1	1	1	1	1	10
91521	1083	4495	1720	1	1	1	1	1	1	10
91522	-0	5170	1720	1	1	1	1	1	1	10
100635	7840	6650	1850	0	0	0	0	0	0	10
100638	9000	6650	1850	0	0	0	0	0	0	10
100641	10160	6650	1850	0	0	0	0	0	0	10
100644	11320	6650	1850	0	0	0	0	0	0	10
100653	12042	6775	1850	0	0	0	0	0	0	10
100662	7113	6790	1850	0	0	0	0	0	0	10
100677	7840	7100	1850	0	0	0	0	0	0	10
100678	9000	7100	1850	0	0	0	0	0	0	10
100679	10160	7100	1850	0	0	0	0	0	0	10
100680	11320	7100	1850	0	0	0	0	0	0	10
100687	13128	7182	1850	0	0	0	0	0	0	10
100690	11884	7196	1850	0	0	0	0	0	0	10
100695	6030	7208	1850	0	0	0	0	0	0	10
100698	7274	7210	1850	0	0	0	0	0	0	10
100704	7840	7550	1850	0	0	0	0	0	0	10
100707	9000	7550	1850	0	0	0	0	0	0	10
100710	10160	7550	1850	0	0	0	0	0	0	10
100713	11320	7550	1850	0	0	0	0	0	0	10
100718	14214	7589	1850	0	0	0	0	0	0	10
100721	12970	7603	1850	0	0	0	0	0	0	10
100722	11726	7617	1850	0	0	0	0	0	0	10
100726	4948	7625	1850	0	0	0	0	0	0	10
100729	6192	7628	1850	0	0	0	0	0	0	10
100731	7436	7630	1850	0	0	0	0	0	0	10
100738	15300	7996	1850	0	0	0	0	0	0	10
100745	14056	8010	1850	0	0	0	0	0	0	10
100746	12812	8024	1850	0	0	0	0	0	0	10
100750	3865	8042	1850	0	0	0	0	0	0	10
100753	5110	8045	1850	0	0	0	0	0	0	10
100754	6354	8047	1850	0	0	0	0	0	0	10
100762	15990	8390	1850	0	0	0	0	0	0	10
100763	15142	8417	1850	0	0	0	0	0	0	10
100764	3210	8430	1850	0	0	0	0	0	0	10
100765	13898	8432	1850	0	0	0	0	0	0	10
100785	4027	8462	1850	0	0	0	0	0	0	10
100786	5272	8465	1850	0	0	0	0	0	0	10
100794	15680	8725	1850	0	0	0	0	0	0	10
100795	3520	8760	1850	0	0	0	0	0	0	10
100798	14984	8839	1850	0	0	0	0	0	0	10
100805	4189	8882	1850	0	0	0	0	0	0	10
100816	15370	9060	1850	0	0	0	0	0	0	10
100817	3830	9090	1850	0	0	0	0	0	0	10
100818	16770	9110	1850	0	0	0	0	0	0	10
100819	2430	9160	1850	0	0	0	0	0	0	10
100839	16460	9445	1850	0	0	0	0	0	0	10
100841	2740	9490	1850	0	0	0	0	0	0	10
100852	16150	9780	1850	0	0	0	0	0	0	10
100853	3050	9820	1850	0	0	0	0	0	0	10
101498	7840	1250	1890	1	1	1	1	1	1	11
101499	9000	1250	1890	1	1	1	1	1	1	11
101500	10160	1250	1890	1	1	1	1	1	1	11
101501	11320	1250	1890	1	1	1	1	1	1	11

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
101502	17565	1969	1960	1	1	1	1	1	1	11
101503	16110	2533	1890	1	1	1	1	1	1	11
101504	17196	2940	1890	1	1	1	1	1	1	11
101505	15024	2125	1890	1	1	1	1	1	1	11
101506	13937	1718	1890	1	1	1	1	1	1	11
101507	3006	2586	1890	1	1	1	1	1	1	11
101508	5170	1752	1890	1	1	1	1	1	1	11
101509	1923	3003	1890	1	1	1	1	1	1	11
101510	4088	2169	1890	1	1	1	1	1	1	11
101511	12067	1337	1890	1	1	1	1	1	1	11
101512	13209	1542	1890	1	1	1	1	1	1	11
101513	5878	1580	1890	1	1	1	1	1	1	11
101514	7017	1363	1890	1	1	1	1	1	1	11
101515	18330	2675	1940	1	1	1	1	1	1	11
101516	19202	3487	1920	1	1	1	1	1	1	11
101517	40	4320	1890	1	1	1	1	1	1	11
101518	1290	3550	1890	1	1	1	1	1	1	11
101519	20700	4870	1890	1	1	1	1	1	1	11
101520	19920	4150	1910	1	1	1	1	1	1	11
101521	110	3840	1900	1	1	1	1	1	1	11
101522	380	3140	1910	1	1	1	1	1	1	11
101523	700	2580	1920	1	1	1	1	1	1	11
101524	1040	2180	1930	1	1	1	1	1	1	11
101525	1540	1720	1940	1	1	1	1	1	1	11
101526	1730	1920	1940	1	1	1	1	1	1	11
110097	7840	0	2000	1	1	1	1	1	1	11
110098	9000	0	2000	1	1	1	1	1	1	11
110099	10160	0	2000	1	1	1	1	1	1	11
110101	11320	0	2000	1	1	1	1	1	1	11
110107	12288	107	2000	1	1	1	1	1	1	11
110109	6784	135	2000	1	1	1	1	1	1	11
110113	13430	312	2000	1	1	1	1	1	1	11
110115	5644	352	2000	1	1	1	1	1	1	11
110123	14376	548	2000	1	1	1	1	1	1	11
110124	4721	585	2000	1	1	1	1	1	1	11
110137	15462	955	2000	1	1	1	1	1	1	11
110139	3638	1003	2000	1	1	1	1	1	1	11
110145	7840	1250	2000	0	0	0	0	0	0	11
110146	9000	1250	2000	0	0	0	0	0	0	11
110147	10160	1250	2000	0	0	0	0	0	0	11
110150	11320	1250	2000	0	0	0	0	0	0	11
110154	12067	1337	2000	0	0	0	0	0	0	11
110158	16549	1362	2000	1	1	1	1	1	1	11
110162	7017	1363	2000	0	0	0	0	0	0	11
110164	2556	1420	2000	1	1	1	1	1	1	11
110165	13209	1542	2000	0	0	0	0	0	0	11
110168	5878	1580	2000	0	0	0	0	0	0	11
110173	13937	1718	2000	0	0	0	0	0	0	11
110176	5170	1752	2000	0	0	0	0	0	0	11
110189	15024	2125	2000	0	0	0	0	0	0	11
110192	7840	2150	2000	0	0	0	0	0	0	11
110195	9000	2150	2000	0	0	0	0	0	0	11
110198	10160	2150	2000	0	0	0	0	0	0	11
110201	11320	2150	2000	0	0	0	0	0	0	11
110204	4088	2169	2000	0	0	0	0	0	0	11
110211	11908	2223	2000	0	0	0	0	0	0	11
110214	7185	2248	2000	0	0	0	0	0	0	11
110217	13049	2428	2000	0	0	0	0	0	0	11
110221	6046	2464	2000	0	0	0	0	0	0	11
110224	16110	2533	2000	0	0	0	0	0	0	11
110228	13621	2561	2000	0	0	0	0	0	0	11
110232	3006	2586	2000	0	0	0	0	0	0	11
110234	5494	2592	2000	0	0	0	0	0	0	11
110248	17196	2940	2000	0	0	0	0	0	0	11
110251	14708	2968	2000	0	0	0	0	0	0	11
110256	1923	3003	2000	0	0	0	0	0	0	11
110258	4412	3009	2000	0	0	0	0	0	0	11
110299	15794	3375	2000	0	0	0	0	0	0	11
110308	3329	3426	2000	0	0	0	0	0	0	11
110322	1290	3550	2000	0	0	0	0	0	0	11
110325	17772	3614	2000	0	0	0	0	0	0	11
110328	16880	3782	2000	0	0	0	0	0	0	11
110339	2247	3843	2000	0	0	0	0	0	0	11
110370	17475	4084	2000	0	0	0	0	0	0	11
110373	1662	4138	2000	0	0	0	0	0	0	11
110382	18764	4206	2000	0	0	0	0	0	0	11
110433	18467	4685	2000	0	0	0	0	0	0	11
110554	7840	5750	2000	0	0	0	0	0	0	11
110557	9000	5750	2000	0	0	0	0	0	0	11

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
110560	10160	5750	2000	0	0	0	0	0	0	11
110563	11320	5750	2000	0	0	0	0	0	0	11
110576	12358	5932	2000	0	0	0	0	0	0	11
110585	6789	5951	2000	0	0	0	0	0	0	11
110593	7840	6200	2000	0	0	0	0	0	0	11
110594	9000	6200	2000	0	0	0	0	0	0	11
110595	10160	6200	2000	0	0	0	0	0	0	11
110596	11320	6200	2000	0	0	0	0	0	0	11
110608	13444	6339	2000	0	0	0	0	0	0	11
110611	12200	6353	2000	0	0	0	0	0	0	11
110617	5707	6368	2000	0	0	0	0	0	0	11
110620	6951	6371	2000	0	0	0	0	0	0	11
110635	7840	6650	2000	0	0	0	0	0	0	11
110638	9000	6650	2000	0	0	0	0	0	0	11
110641	10160	6650	2000	0	0	0	0	0	0	11
110644	11320	6650	2000	0	0	0	0	0	0	11
110649	14530	6746	2000	0	0	0	0	0	0	11
110652	13286	6760	2000	0	0	0	0	0	0	11
110653	12042	6775	2000	0	0	0	0	0	0	11
110658	4624	6785	2000	0	0	0	0	0	0	11
110661	5868	6788	2000	0	0	0	0	0	0	11
110662	7113	6790	2000	0	0	0	0	0	0	11
110683	15616	7153	2000	0	0	0	0	0	0	11
110686	14372	7168	2000	0	0	0	0	0	0	11
110687	13128	7182	2000	0	0	0	0	0	0	11
110691	3542	7202	2000	0	0	0	0	0	0	11
110694	4786	7205	2000	0	0	0	0	0	0	11
110695	6030	7208	2000	0	0	0	0	0	0	11
110716	15458	7575	2000	0	0	0	0	0	0	11
110718	14214	7589	2000	0	0	0	0	0	0	11
110725	3704	7622	2000	0	0	0	0	0	0	11
110726	4948	7625	2000	0	0	0	0	0	0	11
110734	16610	7730	2000	0	0	0	0	0	0	11
110735	2580	7770	2000	0	0	0	0	0	0	11
110738	15300	7996	2000	0	0	0	0	0	0	11
110750	3865	8042	2000	0	0	0	0	0	0	11
110758	16300	8060	2000	0	0	0	0	0	0	11
110759	2895	8100	2000	0	0	0	0	0	0	11
110762	15990	8390	2000	0	0	0	0	0	0	11
110764	3210	8430	2000	0	0	0	0	0	0	11
110769	17390	8450	2000	0	0	0	0	0	0	11
110793	1800	8500	2000	0	0	0	0	0	0	11
110796	17080	8780	2000	0	0	0	0	0	0	11
110797	2115	8830	2000	0	0	0	0	0	0	11
110818	16770	9110	2000	0	0	0	0	0	0	11
110819	2430	9160	2000	0	0	0	0	0	0	11
120003	4650	11210	2120	0	0	0	0	0	0	12
120004	5170	11210	2120	0	0	0	0	0	0	12
120005	6370	11210	2120	0	0	0	0	0	0	12
120006	7570	11210	2120	0	0	0	0	0	0	12
120007	8770	11210	2120	0	0	0	0	0	0	12
120008	9970	11210	2120	0	0	0	0	0	0	12
120009	11170	11210	2120	0	0	0	0	0	0	12
120010	12370	11210	2120	0	0	0	0	0	0	12
120011	13570	11210	2120	0	0	0	0	0	0	12
120012	14560	11210	2120	0	0	0	0	0	0	12
120013	4650	12410	2120	0	0	0	0	0	0	12
120014	5170	12410	2120	0	0	0	0	0	0	12
120015	6370	12410	2120	0	0	0	0	0	0	12
120016	7570	12410	2120	0	0	0	0	0	0	12
120017	8770	12410	2120	0	0	0	0	0	0	12
120018	9970	12410	2120	0	0	0	0	0	0	12
120019	11170	12410	2120	0	0	0	0	0	0	12
120020	12370	12410	2120	0	0	0	0	0	0	12
120021	13570	12410	2120	0	0	0	0	0	0	12
120022	14560	12410	2120	0	0	0	0	0	0	12
120023	4650	13610	2120	0	0	0	0	0	0	12
120024	5170	13610	2120	0	0	0	0	0	0	12
120025	6370	13610	2120	0	0	0	0	0	0	12
120026	7570	13610	2120	0	0	0	0	0	0	12
120027	8770	13610	2120	0	0	0	0	0	0	12
120028	9970	13610	2120	0	0	0	0	0	0	12
120029	11170	13610	2120	0	0	0	0	0	0	12
120030	12370	13610	2120	0	0	0	0	0	0	12
120031	13570	13610	2120	0	0	0	0	0	0	12
120032	14560	13610	2120	0	0	0	0	0	0	12
120033	4650	14810	2120	0	0	0	0	0	0	12
120034	5170	14810	2120	0	0	0	0	0	0	12
120035	6370	14810	2120	0	0	0	0	0	0	12

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
120036	7570	14810	2120	0	0	0	0	0	0	12
120037	8770	14810	2120	0	0	0	0	0	0	12
120038	9970	14810	2120	0	0	0	0	0	0	12
120039	11170	14810	2120	0	0	0	0	0	0	12
120040	12370	14810	2120	0	0	0	0	0	0	12
120041	13570	14810	2120	0	0	0	0	0	0	12
120042	14560	14810	2120	0	0	0	0	0	0	12
120043	4650	16010	2120	0	0	0	0	0	0	12
120044	5170	16010	2120	0	0	0	0	0	0	12
120045	6370	16010	2120	0	0	0	0	0	0	12
120046	7570	16010	2120	0	0	0	0	0	0	12
120047	8770	16010	2120	0	0	0	0	0	0	12
120048	9970	16010	2120	0	0	0	0	0	0	12
120049	11170	16010	2120	0	0	0	0	0	0	12
120050	12370	16010	2120	0	0	0	0	0	0	12
120051	13570	16010	2120	0	0	0	0	0	0	12
120052	14560	16010	2120	0	0	0	0	0	0	12
120053	4650	17210	2120	0	0	0	0	0	0	12
120054	5170	17210	2120	0	0	0	0	0	0	12
120055	6370	17210	2120	0	0	0	0	0	0	12
120056	7570	17210	2120	0	0	0	0	0	0	12
120057	8770	17210	2120	0	0	0	0	0	0	12
120058	9970	17210	2120	0	0	0	0	0	0	12
120059	11170	17210	2120	0	0	0	0	0	0	12
120060	12370	17210	2120	0	0	0	0	0	0	12
120061	13570	17210	2120	0	0	0	0	0	0	12
120062	14560	17210	2120	0	0	0	0	0	0	12
120063	4650	18410	2120	0	0	0	0	0	0	12
120064	5170	18410	2120	0	0	0	0	0	0	12
120065	6370	18410	2120	0	0	0	0	0	0	12
120066	7570	18410	2120	0	0	0	0	0	0	12
120067	8770	18410	2120	0	0	0	0	0	0	12
120068	9970	18410	2120	0	0	0	0	0	0	12
120069	11170	18410	2120	0	0	0	0	0	0	12
120070	12370	18410	2120	0	0	0	0	0	0	12
120071	13570	18410	2120	0	0	0	0	0	0	12
120072	14560	18410	2120	0	0	0	0	0	0	12
120073	4650	19610	2120	0	0	0	0	0	0	12
120074	5170	19610	2120	0	0	0	0	0	0	12
120075	6370	19610	2120	0	0	0	0	0	0	12
120076	7570	19610	2120	0	0	0	0	0	0	12
120077	8770	19610	2120	0	0	0	0	0	0	12
120078	9970	19610	2120	0	0	0	0	0	0	12
120079	11170	19610	2120	0	0	0	0	0	0	12
120080	12370	19610	2120	0	0	0	0	0	0	12
120081	13570	19610	2120	0	0	0	0	0	0	12
120082	14560	19610	2120	0	0	0	0	0	0	12
120083	4650	20650	2120	0	0	0	0	0	0	12
120084	5170	20650	2120	0	0	0	0	0	0	12
120085	6370	20650	2120	0	0	0	0	0	0	12
120086	7570	20650	2120	0	0	0	0	0	0	12
120087	8770	20650	2120	0	0	0	0	0	0	12
120088	9970	20650	2120	0	0	0	0	0	0	12
120089	11170	20650	2120	0	0	0	0	0	0	12
120090	12370	20650	2120	0	0	0	0	0	0	12
120091	13570	20650	2120	0	0	0	0	0	0	12
120092	14560	20650	2120	0	0	0	0	0	0	12
120938	5770	11210	2120	0	0	0	0	0	0	12
120940	6970	11210	2120	0	0	0	0	0	0	12
120942	8170	11210	2120	0	0	0	0	0	0	12
120944	9370	11210	2120	0	0	0	0	0	0	12
120946	10570	11210	2120	0	0	0	0	0	0	12
120948	11770	11210	2120	0	0	0	0	0	0	12
120950	12970	11210	2120	0	0	0	0	0	0	12
120952	14065	11210	2120	0	0	0	0	0	0	12
120972	4650	11810	2120	0	0	0	0	0	0	12
120973	5170	11810	2120	0	0	0	0	0	0	12
120974	6370	11810	2120	0	0	0	0	0	0	12
120975	7570	11810	2120	0	0	0	0	0	0	12
120976	8770	11810	2120	0	0	0	0	0	0	12
120977	9970	11810	2120	0	0	0	0	0	0	12
120978	11170	11810	2120	0	0	0	0	0	0	12
120979	12370	11810	2120	0	0	0	0	0	0	12
120980	13570	11810	2120	0	0	0	0	0	0	12
120981	14560	11810	2120	0	0	0	0	0	0	12
121006	5770	12410	2120	0	0	0	0	0	0	12
121008	6970	12410	2120	0	0	0	0	0	0	12
121010	8170	12410	2120	0	0	0	0	0	0	12
121012	9370	12410	2120	0	0	0	0	0	0	12

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
121014	10570	12410	2120	0	0	0	0	0	0	12
121016	11770	12410	2120	0	0	0	0	0	0	12
121018	12970	12410	2120	0	0	0	0	0	0	12
121020	14065	12410	2120	0	0	0	0	0	0	12
121040	4650	13010	2120	0	0	0	0	0	0	12
121041	5170	13010	2120	0	0	0	0	0	0	12
121042	6370	13010	2120	0	0	0	0	0	0	12
121043	7570	13010	2120	0	0	0	0	0	0	12
121044	8770	13010	2120	0	0	0	0	0	0	12
121045	9970	13010	2120	0	0	0	0	0	0	12
121046	11170	13010	2120	0	0	0	0	0	0	12
121047	12370	13010	2120	0	0	0	0	0	0	12
121048	13570	13010	2120	0	0	0	0	0	0	12
121049	14560	13010	2120	0	0	0	0	0	0	12
121074	5770	13610	2120	0	0	0	0	0	0	12
121076	6970	13610	2120	0	0	0	0	0	0	12
121078	8170	13610	2120	0	0	0	0	0	0	12
121080	9370	13610	2120	0	0	0	0	0	0	12
121082	10570	13610	2120	0	0	0	0	0	0	12
121084	11770	13610	2120	0	0	0	0	0	0	12
121086	12970	13610	2120	0	0	0	0	0	0	12
121088	14065	13610	2120	0	0	0	0	0	0	12
121108	4650	14210	2120	0	0	0	0	0	0	12
121109	5170	14210	2120	0	0	0	0	0	0	12
121110	6370	14210	2120	0	0	0	0	0	0	12
121111	7570	14210	2120	0	0	0	0	0	0	12
121112	8770	14210	2120	0	0	0	0	0	0	12
121113	9970	14210	2120	0	0	0	0	0	0	12
121114	11170	14210	2120	0	0	0	0	0	0	12
121115	12370	14210	2120	0	0	0	0	0	0	12
121116	13570	14210	2120	0	0	0	0	0	0	12
121117	14560	14210	2120	0	0	0	0	0	0	12
121146	5770	14810	2120	0	0	0	0	0	0	12
121148	6970	14810	2120	0	0	0	0	0	0	12
121150	8170	14810	2120	0	0	0	0	0	0	12
121152	9370	14810	2120	0	0	0	0	0	0	12
121154	10570	14810	2120	0	0	0	0	0	0	12
121156	11770	14810	2120	0	0	0	0	0	0	12
121158	12970	14810	2120	0	0	0	0	0	0	12
121160	14065	14810	2120	0	0	0	0	0	0	12
121190	4650	15410	2120	0	0	0	0	0	0	12
121191	5170	15410	2120	0	0	0	0	0	0	12
121192	6370	15410	2120	0	0	0	0	0	0	12
121193	7570	15410	2120	0	0	0	0	0	0	12
121194	8770	15410	2120	0	0	0	0	0	0	12
121195	9970	15410	2120	0	0	0	0	0	0	12
121196	11170	15410	2120	0	0	0	0	0	0	12
121197	12370	15410	2120	0	0	0	0	0	0	12
121198	13570	15410	2120	0	0	0	0	0	0	12
121199	14560	15410	2120	0	0	0	0	0	0	12
121218	5770	16010	2120	0	0	0	0	0	0	12
121220	6970	16010	2120	0	0	0	0	0	0	12
121222	8170	16010	2120	0	0	0	0	0	0	12
121224	9370	16010	2120	0	0	0	0	0	0	12
121226	10570	16010	2120	0	0	0	0	0	0	12
121228	11770	16010	2120	0	0	0	0	0	0	12
121230	12970	16010	2120	0	0	0	0	0	0	12
121232	14065	16010	2120	0	0	0	0	0	0	12
121252	4650	16610	2120	0	0	0	0	0	0	12
121253	5170	16610	2120	0	0	0	0	0	0	12
121254	6370	16610	2120	0	0	0	0	0	0	12
121255	7570	16610	2120	0	0	0	0	0	0	12
121256	8770	16610	2120	0	0	0	0	0	0	12
121257	9970	16610	2120	0	0	0	0	0	0	12
121258	11170	16610	2120	0	0	0	0	0	0	12
121259	12370	16610	2120	0	0	0	0	0	0	12
121260	13570	16610	2120	0	0	0	0	0	0	12
121261	14560	16610	2120	0	0	0	0	0	0	12
121286	5770	17210	2120	0	0	0	0	0	0	12
121288	6970	17210	2120	0	0	0	0	0	0	12
121290	8170	17210	2120	0	0	0	0	0	0	12
121292	9370	17210	2120	0	0	0	0	0	0	12
121294	10570	17210	2120	0	0	0	0	0	0	12
121296	11770	17210	2120	0	0	0	0	0	0	12
121298	12970	17210	2120	0	0	0	0	0	0	12
121300	14065	17210	2120	0	0	0	0	0	0	12
121330	4650	17810	2120	0	0	0	0	0	0	12
121331	5170	17810	2120	0	0	0	0	0	0	12
121332	6370	17810	2120	0	0	0	0	0	0	12

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
121333	7570	17810	2120	0	0	0	0	0	0	12
121334	8770	17810	2120	0	0	0	0	0	0	12
121335	9970	17810	2120	0	0	0	0	0	0	12
121336	11170	17810	2120	0	0	0	0	0	0	12
121337	12370	17810	2120	0	0	0	0	0	0	12
121338	13570	17810	2120	0	0	0	0	0	0	12
121339	14560	17810	2120	0	0	0	0	0	0	12
121354	5770	18410	2120	0	0	0	0	0	0	12
121356	6970	18410	2120	0	0	0	0	0	0	12
121358	8170	18410	2120	0	0	0	0	0	0	12
121360	9370	18410	2120	0	0	0	0	0	0	12
121362	10570	18410	2120	0	0	0	0	0	0	12
121364	11770	18410	2120	0	0	0	0	0	0	12
121366	12970	18410	2120	0	0	0	0	0	0	12
121368	14065	18410	2120	0	0	0	0	0	0	12
121398	4650	19010	2120	0	0	0	0	0	0	12
121399	5170	19010	2120	0	0	0	0	0	0	12
121400	6370	19010	2120	0	0	0	0	0	0	12
121401	7570	19010	2120	0	0	0	0	0	0	12
121402	8770	19010	2120	0	0	0	0	0	0	12
121403	9970	19010	2120	0	0	0	0	0	0	12
121404	11170	19010	2120	0	0	0	0	0	0	12
121405	12370	19010	2120	0	0	0	0	0	0	12
121406	13570	19010	2120	0	0	0	0	0	0	12
121407	14560	19010	2120	0	0	0	0	0	0	12
121426	5770	19610	2120	0	0	0	0	0	0	12
121428	6970	19610	2120	0	0	0	0	0	0	12
121430	8170	19610	2120	0	0	0	0	0	0	12
121432	9370	19610	2120	0	0	0	0	0	0	12
121434	10570	19610	2120	0	0	0	0	0	0	12
121436	11770	19610	2120	0	0	0	0	0	0	12
121438	12970	19610	2120	0	0	0	0	0	0	12
121440	14065	19610	2120	0	0	0	0	0	0	12
121470	4650	20210	2120	0	0	0	0	0	0	12
121471	5170	20210	2120	0	0	0	0	0	0	12
121472	6370	20210	2120	0	0	0	0	0	0	12
121473	7570	20210	2120	0	0	0	0	0	0	12
121474	8770	20210	2120	0	0	0	0	0	0	12
121475	9970	20210	2120	0	0	0	0	0	0	12
121476	11170	20210	2120	0	0	0	0	0	0	12
121477	12370	20210	2120	0	0	0	0	0	0	12
121478	13570	20210	2120	0	0	0	0	0	0	12
121479	14560	20210	2120	0	0	0	0	0	0	12
121482	5770	20650	2120	0	0	0	0	0	0	12
121484	6970	20650	2120	0	0	0	0	0	0	12
121486	8170	20650	2120	0	0	0	0	0	0	12
121488	9370	20650	2120	0	0	0	0	0	0	12
121490	10570	20650	2120	0	0	0	0	0	0	12
121492	11770	20650	2120	0	0	0	0	0	0	12
121494	12970	20650	2120	0	0	0	0	0	0	12
121496	14065	20650	2120	0	0	0	0	0	0	12
130445	7840	4850	2150	0	0	0	0	0	0	13
130449	9000	4850	2150	0	0	0	0	0	0	13
130453	10160	4850	2150	0	0	0	0	0	0	13
130457	11320	4850	2150	0	0	0	0	0	0	13
130466	11430	4880	2150	0	0	0	0	0	0	13
130470	7690	4900	2150	0	0	0	0	0	0	13
130486	12572	5085	2150	0	0	0	0	0	0	13
130490	12674	5089	2150	0	0	0	0	0	0	13
130499	6465	5111	2150	0	0	0	0	0	0	13
130503	6550	5117	2150	0	0	0	0	0	0	13
130513	7840	5300	2150	0	0	0	0	0	0	13
130514	9000	5300	2150	0	0	0	0	0	0	13
130515	10160	5300	2150	0	0	0	0	0	0	13
130516	11320	5300	2150	0	0	0	0	0	0	13
130527	13760	5496	2150	0	0	0	0	0	0	13
130531	12516	5510	2150	0	0	0	0	0	0	13
130540	5383	5528	2150	0	0	0	0	0	0	13
130544	6627	5531	2150	0	0	0	0	0	0	13
130554	7840	5750	2150	0	0	0	0	0	0	13
130557	9000	5750	2150	0	0	0	0	0	0	13
130560	10160	5750	2150	0	0	0	0	0	0	13
130563	11320	5750	2150	0	0	0	0	0	0	13
130570	14846	5903	2150	0	0	0	0	0	0	13
130574	13602	5918	2150	0	0	0	0	0	0	13
130576	12358	5932	2150	0	0	0	0	0	0	13
130580	4300	5945	2150	0	0	0	0	0	0	13
130584	5545	5948	2150	0	0	0	0	0	0	13
130585	6789	5951	2150	0	0	0	0	0	0	13

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
130603	15932	6311	2150	0	0	0	0	0	0	13
130607	14688	6325	2150	0	0	0	0	0	0	13
130608	13444	6339	2150	0	0	0	0	0	0	13
130612	3218	6363	2150	0	0	0	0	0	0	13
130616	4462	6365	2150	0	0	0	0	0	0	13
130617	5707	6368	2150	0	0	0	0	0	0	13
130622	16076	6393	2150	0	0	0	0	0	0	13
130626	3080	6435	2150	0	0	0	0	0	0	13
130648	15774	6732	2150	0	0	0	0	0	0	13
130649	14530	6746	2150	0	0	0	0	0	0	13
130657	3380	6782	2150	0	0	0	0	0	0	13
130658	4624	6785	2150	0	0	0	0	0	0	13
130668	17067	6994	2150	0	0	0	0	0	0	13
130672	2092	7045	2150	0	0	0	0	0	0	13
130676	17230	7060	2150	0	0	0	0	0	0	13
130682	1970	7110	2150	0	0	0	0	0	0	13
130683	15616	7153	2150	0	0	0	0	0	0	13
130691	3542	7202	2150	0	0	0	0	0	0	13
130701	16920	7395	2150	0	0	0	0	0	0	13
130702	2275	7440	2150	0	0	0	0	0	0	13
130734	16610	7730	2150	0	0	0	0	0	0	13
130735	2580	7770	2150	0	0	0	0	0	0	13
130736	18010	7780	2150	0	0	0	0	0	0	13
130737	1190	7840	2150	0	0	0	0	0	0	13
130760	17700	8115	2150	0	0	0	0	0	0	13
130761	1495	8170	2150	0	0	0	0	0	0	13
130769	17390	8450	2150	0	0	0	0	0	0	13
130793	1800	8500	2150	0	0	0	0	0	0	13
140351	7840	3950	2300	0	0	0	0	0	0	14
140354	9000	3950	2300	0	0	0	0	0	0	14
140357	10160	3950	2300	0	0	0	0	0	0	14
140360	11320	3950	2300	0	0	0	0	0	0	14
140363	11589	3994	2300	0	0	0	0	0	0	14
140367	7522	4016	2300	0	0	0	0	0	0	14
140378	12731	4199	2300	0	0	0	0	0	0	14
140389	6382	4233	2300	0	0	0	0	0	0	14
140392	12990	4246	2300	0	0	0	0	0	0	14
140401	6141	4271	2300	0	0	0	0	0	0	14
140405	7840	4400	2300	0	0	0	0	0	0	14
140406	9000	4400	2300	0	0	0	0	0	0	14
140407	10160	4400	2300	0	0	0	0	0	0	14
140408	11320	4400	2300	0	0	0	0	0	0	14
140409	11510	4437	2300	0	0	0	0	0	0	14
140412	7606	4458	2300	0	0	0	0	0	0	14
140423	12651	4642	2300	0	0	0	0	0	0	14
140424	14076	4654	2300	0	0	0	0	0	0	14
140427	12832	4668	2300	0	0	0	0	0	0	14
140428	6466	4675	2300	0	0	0	0	0	0	14
140437	5059	4688	2300	0	0	0	0	0	0	14
140440	6303	4691	2300	0	0	0	0	0	0	14
140445	7840	4850	2300	0	0	0	0	0	0	14
140449	9000	4850	2300	0	0	0	0	0	0	14
140453	10160	4850	2300	0	0	0	0	0	0	14
140457	11320	4850	2300	0	0	0	0	0	0	14
140466	11430	4880	2300	0	0	0	0	0	0	14
140470	7690	4900	2300	0	0	0	0	0	0	14
140481	15162	5061	2300	0	0	0	0	0	0	14
140485	13918	5075	2300	0	0	0	0	0	0	14
140486	12572	5085	2300	0	0	0	0	0	0	14
140490	12674	5089	2300	0	0	0	0	0	0	14
140495	3977	5106	2300	0	0	0	0	0	0	14
140498	5221	5108	2300	0	0	0	0	0	0	14
140499	6465	5111	2300	0	0	0	0	0	0	14
140503	6550	5117	2300	0	0	0	0	0	0	14
140522	16248	5468	2300	0	0	0	0	0	0	14
140526	15004	5482	2300	0	0	0	0	0	0	14
140527	13760	5496	2300	0	0	0	0	0	0	14
140536	2894	5523	2300	0	0	0	0	0	0	14
140539	4139	5525	2300	0	0	0	0	0	0	14
140540	5383	5528	2300	0	0	0	0	0	0	14
140546	16542	5623	2300	0	0	0	0	0	0	14
140550	2607	5669	2300	0	0	0	0	0	0	14
140568	16090	5889	2300	0	0	0	0	0	0	14
140570	14846	5903	2300	0	0	0	0	0	0	14
140579	3056	5943	2300	0	0	0	0	0	0	14
140580	4300	5945	2300	0	0	0	0	0	0	14
140588	16309	6008	2300	0	0	0	0	0	0	14
140589	2844	6052	2300	0	0	0	0	0	0	14
140597	17534	6225	2300	0	0	0	0	0	0	14

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
140600	1620	6279	2300	0	0	0	0	0	0	14
140603	15932	6311	2300	0	0	0	0	0	0	14
140612	3218	6363	2300	0	0	0	0	0	0	14
140621	17840	6390	2300	0	0	0	0	0	0	14
140622	16076	6393	2300	0	0	0	0	0	0	14
140626	3080	6435	2300	0	0	0	0	0	0	14
140633	17301	6609	2300	0	0	0	0	0	0	14
140634	1830	6619	2300	0	0	0	0	0	0	14
140647	17535	6725	2300	0	0	0	0	0	0	14
140665	630	6900	2300	0	0	0	0	0	0	14
140666	2040	6959	2300	0	0	0	0	0	0	14
140667	500	6980	2300	0	0	0	0	0	0	14
140668	17067	6994	2300	0	0	0	0	0	0	14
140672	2092	7045	2300	0	0	0	0	0	0	14
140676	17230	7060	2300	0	0	0	0	0	0	14
140681	18620	7110	2300	0	0	0	0	0	0	14
140682	1970	7110	2300	0	0	0	0	0	0	14
140699	840	7240	2300	0	0	0	0	0	0	14
140700	730	7305	2300	0	0	0	0	0	0	14
140703	18315	7445	2300	0	0	0	0	0	0	14
140717	1050	7580	2300	0	0	0	0	0	0	14
140730	960	7630	2300	0	0	0	0	0	0	14
140736	18010	7780	2300	0	0	0	0	0	0	14
140737	1190	7840	2300	0	0	0	0	0	0	14
150003	4650	11210	2430	0	0	0	0	0	0	15
150004	5170	11210	2430	0	0	0	0	0	0	15
150005	6370	11210	2430	0	0	0	0	0	0	15
150006	7570	11210	2430	0	0	0	0	0	0	15
150007	8770	11210	2430	0	0	0	0	0	0	15
150008	9970	11210	2430	0	0	0	0	0	0	15
150009	11170	11210	2430	0	0	0	0	0	0	15
150010	12370	11210	2430	0	0	0	0	0	0	15
150011	13570	11210	2430	0	0	0	0	0	0	15
150012	14560	11210	2430	0	0	0	0	0	0	15
150013	4650	12410	2430	0	0	0	0	0	0	15
150014	5170	12410	2430	0	0	0	0	0	0	15
150015	6370	12410	2430	0	0	0	0	0	0	15
150016	7570	12410	2430	0	0	0	0	0	0	15
150017	8770	12410	2430	0	0	0	0	0	0	15
150018	9970	12410	2430	0	0	0	0	0	0	15
150019	11170	12410	2430	0	0	0	0	0	0	15
150020	12370	12410	2430	0	0	0	0	0	0	15
150021	13570	12410	2430	0	0	0	0	0	0	15
150022	14560	12410	2430	0	0	0	0	0	0	15
150023	4650	13610	2430	0	0	0	0	0	0	15
150024	5170	13610	2430	0	0	0	0	0	0	15
150025	6370	13610	2430	0	0	0	0	0	0	15
150026	7570	13610	2430	0	0	0	0	0	0	15
150027	8770	13610	2430	0	0	0	0	0	0	15
150028	9970	13610	2430	0	0	0	0	0	0	15
150029	11170	13610	2430	0	0	0	0	0	0	15
150030	12370	13610	2430	0	0	0	0	0	0	15
150031	13570	13610	2430	0	0	0	0	0	0	15
150032	14560	13610	2430	0	0	0	0	0	0	15
150033	4650	14810	2430	0	0	0	0	0	0	15
150034	5170	14810	2430	0	0	0	0	0	0	15
150035	6370	14810	2430	0	0	0	0	0	0	15
150036	7570	14810	2430	0	0	0	0	0	0	15
150037	8770	14810	2430	0	0	0	0	0	0	15
150038	9970	14810	2430	0	0	0	0	0	0	15
150039	11170	14810	2430	0	0	0	0	0	0	15
150040	12370	14810	2430	0	0	0	0	0	0	15
150041	13570	14810	2430	0	0	0	0	0	0	15
150042	14560	14810	2430	0	0	0	0	0	0	15
150043	4650	16010	2430	0	0	0	0	0	0	15
150044	5170	16010	2430	0	0	0	0	0	0	15
150045	6370	16010	2430	0	0	0	0	0	0	15
150046	7570	16010	2430	0	0	0	0	0	0	15
150047	8770	16010	2430	0	0	0	0	0	0	15
150048	9970	16010	2430	0	0	0	0	0	0	15
150049	11170	16010	2430	0	0	0	0	0	0	15
150050	12370	16010	2430	0	0	0	0	0	0	15
150051	13570	16010	2430	0	0	0	0	0	0	15
150052	14560	16010	2430	0	0	0	0	0	0	15
150053	4650	17210	2430	0	0	0	0	0	0	15
150054	5170	17210	2430	0	0	0	0	0	0	15
150055	6370	17210	2430	0	0	0	0	0	0	15
150056	7570	17210	2430	0	0	0	0	0	0	15
150057	8770	17210	2430	0	0	0	0	0	0	15

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
150058	9970	17210	2430	0	0	0	0	0	0	15
150059	11170	17210	2430	0	0	0	0	0	0	15
150060	12370	17210	2430	0	0	0	0	0	0	15
150061	13570	17210	2430	0	0	0	0	0	0	15
150062	14560	17210	2430	0	0	0	0	0	0	15
150063	4650	18410	2430	0	0	0	0	0	0	15
150064	5170	18410	2430	0	0	0	0	0	0	15
150065	6370	18410	2430	0	0	0	0	0	0	15
150066	7570	18410	2430	0	0	0	0	0	0	15
150067	8770	18410	2430	0	0	0	0	0	0	15
150068	9970	18410	2430	0	0	0	0	0	0	15
150069	11170	18410	2430	0	0	0	0	0	0	15
150070	12370	18410	2430	0	0	0	0	0	0	15
150071	13570	18410	2430	0	0	0	0	0	0	15
150072	14560	18410	2430	0	0	0	0	0	0	15
150073	4650	19610	2430	0	0	0	0	0	0	15
150074	5170	19610	2430	0	0	0	0	0	0	15
150075	6370	19610	2430	0	0	0	0	0	0	15
150076	7570	19610	2430	0	0	0	0	0	0	15
150077	8770	19610	2430	0	0	0	0	0	0	15
150078	9970	19610	2430	0	0	0	0	0	0	15
150079	11170	19610	2430	0	0	0	0	0	0	15
150080	12370	19610	2430	0	0	0	0	0	0	15
150081	13570	19610	2430	0	0	0	0	0	0	15
150082	14560	19610	2430	0	0	0	0	0	0	15
150083	4650	20650	2430	0	0	0	0	0	0	15
150084	5170	20650	2430	0	0	0	0	0	0	15
150085	6370	20650	2430	0	0	0	0	0	0	15
150086	7570	20650	2430	0	0	0	0	0	0	15
150087	8770	20650	2430	0	0	0	0	0	0	15
150088	9970	20650	2430	0	0	0	0	0	0	15
150089	11170	20650	2430	0	0	0	0	0	0	15
150090	12370	20650	2430	0	0	0	0	0	0	15
150091	13570	20650	2430	0	0	0	0	0	0	15
150092	14560	20650	2430	0	0	0	0	0	0	15
150964	5770	11210	2430	0	0	0	0	0	0	15
150965	6970	11210	2430	0	0	0	0	0	0	15
150966	8170	11210	2430	0	0	0	0	0	0	15
150967	9370	11210	2430	0	0	0	0	0	0	15
150968	10570	11210	2430	0	0	0	0	0	0	15
150969	11770	11210	2430	0	0	0	0	0	0	15
150970	12970	11210	2430	0	0	0	0	0	0	15
150971	14065	11210	2430	0	0	0	0	0	0	15
150982	4650	11810	2430	0	0	0	0	0	0	15
150983	5170	11810	2430	0	0	0	0	0	0	15
150984	6370	11810	2430	0	0	0	0	0	0	15
150985	7570	11810	2430	0	0	0	0	0	0	15
150986	8770	11810	2430	0	0	0	0	0	0	15
150987	9970	11810	2430	0	0	0	0	0	0	15
150988	11170	11810	2430	0	0	0	0	0	0	15
150989	12370	11810	2430	0	0	0	0	0	0	15
150990	13570	11810	2430	0	0	0	0	0	0	15
150991	14560	11810	2430	0	0	0	0	0	0	15
151032	5770	12410	2430	0	0	0	0	0	0	15
151033	6970	12410	2430	0	0	0	0	0	0	15
151034	8170	12410	2430	0	0	0	0	0	0	15
151035	9370	12410	2430	0	0	0	0	0	0	15
151036	10570	12410	2430	0	0	0	0	0	0	15
151037	11770	12410	2430	0	0	0	0	0	0	15
151038	12970	12410	2430	0	0	0	0	0	0	15
151039	14065	12410	2430	0	0	0	0	0	0	15
151050	4650	13010	2430	0	0	0	0	0	0	15
151051	5170	13010	2430	0	0	0	0	0	0	15
151052	6370	13010	2430	0	0	0	0	0	0	15
151053	7570	13010	2430	0	0	0	0	0	0	15
151054	8770	13010	2430	0	0	0	0	0	0	15
151055	9970	13010	2430	0	0	0	0	0	0	15
151056	11170	13010	2430	0	0	0	0	0	0	15
151057	12370	13010	2430	0	0	0	0	0	0	15
151058	13570	13010	2430	0	0	0	0	0	0	15
151059	14560	13010	2430	0	0	0	0	0	0	15
151100	5770	13610	2430	0	0	0	0	0	0	15
151101	6970	13610	2430	0	0	0	0	0	0	15
151102	8170	13610	2430	0	0	0	0	0	0	15
151103	9370	13610	2430	0	0	0	0	0	0	15
151104	10570	13610	2430	0	0	0	0	0	0	15
151105	11770	13610	2430	0	0	0	0	0	0	15
151106	12970	13610	2430	0	0	0	0	0	0	15
151107	14065	13610	2430	0	0	0	0	0	0	15

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
151118	4650	14210	2430	0	0	0	0	0	0	15
151119	5170	14210	2430	0	0	0	0	0	0	15
151120	6370	14210	2430	0	0	0	0	0	0	15
151121	7570	14210	2430	0	0	0	0	0	0	15
151122	8770	14210	2430	0	0	0	0	0	0	15
151123	9970	14210	2430	0	0	0	0	0	0	15
151124	11170	14210	2430	0	0	0	0	0	0	15
151125	12370	14210	2430	0	0	0	0	0	0	15
151126	13570	14210	2430	0	0	0	0	0	0	15
151127	14560	14210	2430	0	0	0	0	0	0	15
151172	5770	14810	2430	0	0	0	0	0	0	15
151173	6970	14810	2430	0	0	0	0	0	0	15
151174	8170	14810	2430	0	0	0	0	0	0	15
151175	9370	14810	2430	0	0	0	0	0	0	15
151176	10570	14810	2430	0	0	0	0	0	0	15
151177	11770	14810	2430	0	0	0	0	0	0	15
151178	12970	14810	2430	0	0	0	0	0	0	15
151179	14065	14810	2430	0	0	0	0	0	0	15
151180	4650	15410	2430	0	0	0	0	0	0	15
151181	5170	15410	2430	0	0	0	0	0	0	15
151182	6370	15410	2430	0	0	0	0	0	0	15
151183	7570	15410	2430	0	0	0	0	0	0	15
151184	8770	15410	2430	0	0	0	0	0	0	15
151185	9970	15410	2430	0	0	0	0	0	0	15
151186	11170	15410	2430	0	0	0	0	0	0	15
151187	12370	15410	2430	0	0	0	0	0	0	15
151188	13570	15410	2430	0	0	0	0	0	0	15
151189	14560	15410	2430	0	0	0	0	0	0	15
151244	5770	16010	2430	0	0	0	0	0	0	15
151245	6970	16010	2430	0	0	0	0	0	0	15
151246	8170	16010	2430	0	0	0	0	0	0	15
151247	9370	16010	2430	0	0	0	0	0	0	15
151248	10570	16010	2430	0	0	0	0	0	0	15
151249	11770	16010	2430	0	0	0	0	0	0	15
151250	12970	16010	2430	0	0	0	0	0	0	15
151251	14065	16010	2430	0	0	0	0	0	0	15
151262	4650	16610	2430	0	0	0	0	0	0	15
151263	5170	16610	2430	0	0	0	0	0	0	15
151264	6370	16610	2430	0	0	0	0	0	0	15
151265	7570	16610	2430	0	0	0	0	0	0	15
151266	8770	16610	2430	0	0	0	0	0	0	15
151267	9970	16610	2430	0	0	0	0	0	0	15
151268	11170	16610	2430	0	0	0	0	0	0	15
151269	12370	16610	2430	0	0	0	0	0	0	15
151270	13570	16610	2430	0	0	0	0	0	0	15
151271	14560	16610	2430	0	0	0	0	0	0	15
151312	5770	17210	2430	0	0	0	0	0	0	15
151313	6970	17210	2430	0	0	0	0	0	0	15
151314	8170	17210	2430	0	0	0	0	0	0	15
151315	9370	17210	2430	0	0	0	0	0	0	15
151316	10570	17210	2430	0	0	0	0	0	0	15
151317	11770	17210	2430	0	0	0	0	0	0	15
151318	12970	17210	2430	0	0	0	0	0	0	15
151319	14065	17210	2430	0	0	0	0	0	0	15
151320	4650	17810	2430	0	0	0	0	0	0	15
151321	5170	17810	2430	0	0	0	0	0	0	15
151322	6370	17810	2430	0	0	0	0	0	0	15
151323	7570	17810	2430	0	0	0	0	0	0	15
151324	8770	17810	2430	0	0	0	0	0	0	15
151325	9970	17810	2430	0	0	0	0	0	0	15
151326	11170	17810	2430	0	0	0	0	0	0	15
151327	12370	17810	2430	0	0	0	0	0	0	15
151328	13570	17810	2430	0	0	0	0	0	0	15
151329	14560	17810	2430	0	0	0	0	0	0	15
151380	5770	18410	2430	0	0	0	0	0	0	15
151381	6970	18410	2430	0	0	0	0	0	0	15
151382	8170	18410	2430	0	0	0	0	0	0	15
151383	9370	18410	2430	0	0	0	0	0	0	15
151384	10570	18410	2430	0	0	0	0	0	0	15
151385	11770	18410	2430	0	0	0	0	0	0	15
151386	12970	18410	2430	0	0	0	0	0	0	15
151387	14065	18410	2430	0	0	0	0	0	0	15
151388	4650	19010	2430	0	0	0	0	0	0	15
151389	5170	19010	2430	0	0	0	0	0	0	15
151390	6370	19010	2430	0	0	0	0	0	0	15
151391	7570	19010	2430	0	0	0	0	0	0	15
151392	8770	19010	2430	0	0	0	0	0	0	15
151393	9970	19010	2430	0	0	0	0	0	0	15
151394	11170	19010	2430	0	0	0	0	0	0	15

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
151395	12370	19010	2430	0	0	0	0	0	0	15
151396	13570	19010	2430	0	0	0	0	0	0	15
151397	14560	19010	2430	0	0	0	0	0	0	15
151452	5770	19610	2430	0	0	0	0	0	0	15
151453	6970	19610	2430	0	0	0	0	0	0	15
151454	8170	19610	2430	0	0	0	0	0	0	15
151455	9370	19610	2430	0	0	0	0	0	0	15
151456	10570	19610	2430	0	0	0	0	0	0	15
151457	11770	19610	2430	0	0	0	0	0	0	15
151458	12970	19610	2430	0	0	0	0	0	0	15
151459	14065	19610	2430	0	0	0	0	0	0	15
151460	4650	20210	2430	0	0	0	0	0	0	15
151461	5170	20210	2430	0	0	0	0	0	0	15
151462	6370	20210	2430	0	0	0	0	0	0	15
151463	7570	20210	2430	0	0	0	0	0	0	15
151464	8770	20210	2430	0	0	0	0	0	0	15
151465	9970	20210	2430	0	0	0	0	0	0	15
151466	11170	20210	2430	0	0	0	0	0	0	15
151467	12370	20210	2430	0	0	0	0	0	0	15
151468	13570	20210	2430	0	0	0	0	0	0	15
151469	14560	20210	2430	0	0	0	0	0	0	15
151482	5770	20650	2430	0	0	0	0	0	0	15
151484	6970	20650	2430	0	0	0	0	0	0	15
151486	8170	20650	2430	0	0	0	0	0	0	15
151488	9370	20650	2430	0	0	0	0	0	0	15
151490	10570	20650	2430	0	0	0	0	0	0	15
151492	11770	20650	2430	0	0	0	0	0	0	15
151494	12970	20650	2430	0	0	0	0	0	0	15
151496	14065	20650	2430	0	0	0	0	0	0	15
160262	7840	3050	2450	0	0	0	0	0	0	16
160266	9000	3050	2450	0	0	0	0	0	0	16
160270	10160	3050	2450	0	0	0	0	0	0	16
160274	11320	3050	2450	0	0	0	0	0	0	16
160279	11748	3108	2450	0	0	0	0	0	0	16
160283	7354	3132	2450	0	0	0	0	0	0	16
160290	12890	3314	2450	0	0	0	0	0	0	16
160294	6214	3348	2450	0	0	0	0	0	0	16
160303	13306	3404	2450	0	0	0	0	0	0	16
160312	5818	3431	2450	0	0	0	0	0	0	16
160318	7840	3500	2450	0	0	0	0	0	0	16
160319	9000	3500	2450	0	0	0	0	0	0	16
160320	10160	3500	2450	0	0	0	0	0	0	16
160321	11320	3500	2450	0	0	0	0	0	0	16
160323	11669	3551	2450	0	0	0	0	0	0	16
160324	7438	3574	2450	0	0	0	0	0	0	16
160327	12811	3757	2450	0	0	0	0	0	0	16
160331	6298	3791	2450	0	0	0	0	0	0	16
160333	14392	3811	2450	0	0	0	0	0	0	16
160337	13148	3825	2450	0	0	0	0	0	0	16
160346	4735	3849	2450	0	0	0	0	0	0	16
160350	5980	3851	2450	0	0	0	0	0	0	16
160351	7840	3950	2450	0	0	0	0	0	0	16
160354	9000	3950	2450	0	0	0	0	0	0	16
160357	10160	3950	2450	0	0	0	0	0	0	16
160360	11320	3950	2450	0	0	0	0	0	0	16
160363	11589	3994	2450	0	0	0	0	0	0	16
160367	7522	4016	2450	0	0	0	0	0	0	16
160378	12731	4199	2450	0	0	0	0	0	0	16
160384	15478	4218	2450	0	0	0	0	0	0	16
160388	14234	4232	2450	0	0	0	0	0	0	16
160389	6382	4233	2450	0	0	0	0	0	0	16
160392	12990	4246	2450	0	0	0	0	0	0	16
160396	3653	4266	2450	0	0	0	0	0	0	16
160400	4897	4268	2450	0	0	0	0	0	0	16
160401	6141	4271	2450	0	0	0	0	0	0	16
160418	16564	4625	2450	0	0	0	0	0	0	16
160422	15320	4639	2450	0	0	0	0	0	0	16
160424	14076	4654	2450	0	0	0	0	0	0	16
160429	2571	4683	2450	0	0	0	0	0	0	16
160436	3815	4686	2450	0	0	0	0	0	0	16
160437	5059	4688	2450	0	0	0	0	0	0	16
160461	17009	4854	2450	0	0	0	0	0	0	16
160474	2134	4904	2450	0	0	0	0	0	0	16
160479	16406	5047	2450	0	0	0	0	0	0	16
160481	15162	5061	2450	0	0	0	0	0	0	16
160494	2733	5103	2450	0	0	0	0	0	0	16
160495	3977	5106	2450	0	0	0	0	0	0	16
160511	16775	5238	2450	0	0	0	0	0	0	16
160512	2371	5287	2450	0	0	0	0	0	0	16

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
160518	18001	5455	2450	0	0	0	0	0	0	16
160522	16248	5468	2450	0	0	0	0	0	0	16
160532	1147	5513	2450	0	0	0	0	0	0	16
160536	2894	5523	2450	0	0	0	0	0	0	16
160546	16542	5623	2450	0	0	0	0	0	0	16
160550	2607	5669	2450	0	0	0	0	0	0	16
160553	18460	5720	2450	0	0	0	0	0	0	16
160567	17767	5840	2450	0	0	0	0	0	0	16
160569	1383	5896	2450	0	0	0	0	0	0	16
160590	18150	6055	2450	0	0	0	0	0	0	16
160592	160	6130	2450	0	0	0	0	0	0	16
160597	17534	6225	2450	0	0	0	0	0	0	16
160600	1620	6279	2450	0	0	0	0	0	0	16
160621	17840	6390	2450	0	0	0	0	0	0	16
160630	19240	6440	2450	0	0	0	0	0	0	16
160631	395	6515	2450	0	0	0	0	0	0	16
160632	330	6555	2450	0	0	0	0	0	0	16
160656	18930	6775	2450	0	0	0	0	0	0	16
160665	630	6900	2450	0	0	0	0	0	0	16
160667	500	6980	2450	0	0	0	0	0	0	16
160681	18620	7110	2450	0	0	0	0	0	0	16
170192	7840	2150	2600	0	0	0	0	0	0	17
170195	9000	2150	2600	0	0	0	0	0	0	17
170198	10160	2150	2600	0	0	0	0	0	0	17
170201	11320	2150	2600	0	0	0	0	0	0	17
170211	11908	2223	2600	0	0	0	0	0	0	17
170214	7185	2248	2600	0	0	0	0	0	0	17
170217	13049	2428	2600	0	0	0	0	0	0	17
170221	6046	2464	2600	0	0	0	0	0	0	17
170228	13621	2561	2600	0	0	0	0	0	0	17
170234	5494	2592	2600	0	0	0	0	0	0	17
170237	7840	2600	2600	0	0	0	0	0	0	17
170238	9000	2600	2600	0	0	0	0	0	0	17
170239	10160	2600	2600	0	0	0	0	0	0	17
170240	11320	2600	2600	0	0	0	0	0	0	17
170242	11828	2665	2600	0	0	0	0	0	0	17
170244	7270	2690	2600	0	0	0	0	0	0	17
170245	12970	2871	2600	0	0	0	0	0	0	17
170247	6130	2906	2600	0	0	0	0	0	0	17
170251	14708	2968	2600	0	0	0	0	0	0	17
170254	13463	2982	2600	0	0	0	0	0	0	17
170258	4412	3009	2600	0	0	0	0	0	0	17
170261	5656	3011	2600	0	0	0	0	0	0	17
170262	7840	3050	2600	0	0	0	0	0	0	17
170266	9000	3050	2600	0	0	0	0	0	0	17
170270	10160	3050	2600	0	0	0	0	0	0	17
170274	11320	3050	2600	0	0	0	0	0	0	17
170279	11748	3108	2600	0	0	0	0	0	0	17
170283	7354	3132	2600	0	0	0	0	0	0	17
170290	12890	3314	2600	0	0	0	0	0	0	17
170294	6214	3348	2600	0	0	0	0	0	0	17
170299	15794	3375	2600	0	0	0	0	0	0	17
170302	14550	3389	2600	0	0	0	0	0	0	17
170303	13306	3404	2600	0	0	0	0	0	0	17
170308	3329	3426	2600	0	0	0	0	0	0	17
170311	4574	3429	2600	0	0	0	0	0	0	17
170312	5818	3431	2600	0	0	0	0	0	0	17
170328	16880	3782	2600	0	0	0	0	0	0	17
170332	15636	3797	2600	0	0	0	0	0	0	17
170333	14392	3811	2600	0	0	0	0	0	0	17
170339	2247	3843	2600	0	0	0	0	0	0	17
170344	3491	3846	2600	0	0	0	0	0	0	17
170346	4735	3849	2600	0	0	0	0	0	0	17
170370	17475	4084	2600	0	0	0	0	0	0	17
170373	1662	4138	2600	0	0	0	0	0	0	17
170381	16722	4204	2600	0	0	0	0	0	0	17
170384	15478	4218	2600	0	0	0	0	0	0	17
170395	2409	4263	2600	0	0	0	0	0	0	17
170396	3653	4266	2600	0	0	0	0	0	0	17
170413	17242	4469	2600	0	0	0	0	0	0	17
170414	1083	4495	2600	0	0	0	0	0	0	17
170416	1898	4521	2600	0	0	0	0	0	0	17
170418	16564	4625	2600	0	0	0	0	0	0	17
170429	2571	4683	2600	0	0	0	0	0	0	17
170433	18467	4685	2600	0	0	0	0	0	0	17
170442	674	4747	2600	0	0	0	0	0	0	17
170461	17009	4854	2600	0	0	0	0	0	0	17
170474	2134	4904	2600	0	0	0	0	0	0	17
170480	19080	5060	2600	0	0	0	0	0	0	17

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
170484	18234	5070	2600	0	0	0	0	0	0	17
170507	-0	5170	2600	0	0	0	0	0	0	17
170510	942	5181	2600	0	0	0	0	0	0	17
170517	18770	5390	2600	0	0	0	0	0	0	17
170518	18001	5455	2600	0	0	0	0	0	0	17
170532	1147	5513	2600	0	0	0	0	0	0	17
170545	239	5551	2600	0	0	0	0	0	0	17
170549	80	5650	2600	0	0	0	0	0	0	17
170553	18460	5720	2600	0	0	0	0	0	0	17
170566	19860	5780	2600	0	0	0	0	0	0	17
170575	477	5932	2600	0	0	0	0	0	0	17
170591	19550	6110	2600	0	0	0	0	0	0	17
170592	160	6130	2600	0	0	0	0	0	0	17
170630	19240	6440	2600	0	0	0	0	0	0	17
180141	16640	1110	2750	0	0	0	0	0	0	18
180144	2480	1230	2750	0	0	0	0	0	0	18
180145	7840	1250	2750	0	0	0	0	0	0	18
180146	9000	1250	2750	0	0	0	0	0	0	18
180147	10160	1250	2750	0	0	0	0	0	0	18
180150	11320	1250	2750	0	0	0	0	0	0	18
180154	12067	1337	2750	0	0	0	0	0	0	18
180158	16549	1362	2750	0	0	0	0	0	0	18
180162	7017	1363	2750	0	0	0	0	0	0	18
180164	2556	1420	2750	0	0	0	0	0	0	18
180165	13209	1542	2750	0	0	0	0	0	0	18
180168	5878	1580	2750	0	0	0	0	0	0	18
180169	7840	1700	2750	0	0	0	0	0	0	18
180170	9000	1700	2750	0	0	0	0	0	0	18
180171	10160	1700	2750	0	0	0	0	0	0	18
180172	11320	1700	2750	0	0	0	0	0	0	18
180173	13937	1718	2750	0	0	0	0	0	0	18
180174	1540	1720	2750	0	0	0	0	0	0	18
180176	5170	1752	2750	0	0	0	0	0	0	18
180179	16402	1752	2750	0	0	0	0	0	0	18
180180	11987	1780	2750	0	0	0	0	0	0	18
180182	1459	1794	2750	0	0	0	0	0	0	18
180183	7101	1805	2750	0	0	0	0	0	0	18
180184	2706	1809	2750	0	0	0	0	0	0	18
180185	1730	1920	2750	0	0	0	0	0	0	18
180186	17565	1969	2750	0	0	0	0	0	0	18
180187	13129	1985	2750	0	0	0	0	0	0	18
180188	5962	2022	2750	0	0	0	0	0	0	18
180189	15024	2125	2750	0	0	0	0	0	0	18
180190	13779	2140	2750	0	0	0	0	0	0	18
180192	7840	2150	2750	0	0	0	0	0	0	18
180195	9000	2150	2750	0	0	0	0	0	0	18
180198	10160	2150	2750	0	0	0	0	0	0	18
180201	11320	2150	2750	0	0	0	0	0	0	18
180204	4088	2169	2750	0	0	0	0	0	0	18
180207	5332	2172	2750	0	0	0	0	0	0	18
180208	1040	2180	2750	0	0	0	0	0	0	18
180209	1614	2197	2750	0	0	0	0	0	0	18
180210	2856	2197	2750	0	0	0	0	0	0	18
180211	11908	2223	2750	0	0	0	0	0	0	18
180214	7185	2248	2750	0	0	0	0	0	0	18
180217	13049	2428	2750	0	0	0	0	0	0	18
180220	17380	2455	2750	0	0	0	0	0	0	18
180221	6046	2464	2750	0	0	0	0	0	0	18
180224	16110	2533	2750	0	0	0	0	0	0	18
180227	14866	2547	2750	0	0	0	0	0	0	18
180228	13621	2561	2750	0	0	0	0	0	0	18
180231	700	2580	2750	0	0	0	0	0	0	18
180232	3006	2586	2750	0	0	0	0	0	0	18
180233	4250	2589	2750	0	0	0	0	0	0	18
180234	5494	2592	2750	0	0	0	0	0	0	18
180241	1769	2600	2750	0	0	0	0	0	0	18
180243	18330	2675	2750	0	0	0	0	0	0	18
180246	897	2903	2750	0	0	0	0	0	0	18
180248	17196	2940	2750	0	0	0	0	0	0	18
180250	15952	2954	2750	0	0	0	0	0	0	18
180251	14708	2968	2750	0	0	0	0	0	0	18
180255	18144	2988	2750	0	0	0	0	0	0	18
180256	1923	3003	2750	0	0	0	0	0	0	18
180257	3167	3006	2750	0	0	0	0	0	0	18
180258	4412	3009	2750	0	0	0	0	0	0	18
180278	995	3065	2750	0	0	0	0	0	0	18
180287	380	3140	2750	0	0	0	0	0	0	18
180288	1093	3227	2750	0	0	0	0	0	0	18
180289	17958	3301	2750	0	0	0	0	0	0	18

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
180298	17038	3361	2750	0	0	0	0	0	0	18
180299	15794	3375	2750	0	0	0	0	0	0	18
180307	2085	3423	2750	0	0	0	0	0	0	18
180308	3329	3426	2750	0	0	0	0	0	0	18
180316	19202	3487	2750	0	0	0	0	0	0	18
180317	597	3492	2750	0	0	0	0	0	0	18
180322	1290	3550	2750	0	0	0	0	0	0	18
180325	17772	3614	2750	0	0	0	0	0	0	18
180328	16880	3782	2750	0	0	0	0	0	0	18
180338	110	3840	2750	0	0	0	0	0	0	18
180339	2247	3843	2750	0	0	0	0	0	0	18
180342	813	3844	2750	0	0	0	0	0	0	18
180343	1476	3844	2750	0	0	0	0	0	0	18
180345	18983	3846	2750	0	0	0	0	0	0	18
180355	674	4747	2750	0	0	0	0	0	0	18
180366	206	3999	2750	0	0	0	0	0	0	18
180370	17475	4084	2750	0	0	0	0	0	0	18
180373	1662	4138	2750	0	0	0	0	0	0	18
180376	19920	4150	2750	0	0	0	0	0	0	18
180377	302	4158	2750	0	0	0	0	0	0	18
180382	18764	4206	2750	0	0	0	0	0	0	18
180404	40	4320	2750	0	0	0	0	0	0	18
180410	488	4453	2750	0	0	0	0	0	0	18
180411	19640	4453	2750	0	0	0	0	0	0	18
180414	1083	4495	2750	0	0	0	0	0	0	18
180417	226	4616	2750	0	0	0	0	0	0	18
180433	18467	4685	2750	0	0	0	0	0	0	18
180441	20	4745	2750	0	0	0	0	0	0	18
180444	19360	4757	2750	0	0	0	0	0	0	18
180465	20700	4870	2750	0	0	0	0	0	0	18
180478	412	4912	2750	0	0	0	0	0	0	18
180480	19080	5060	2750	0	0	0	0	0	0	18
180507	-0	5170	2750	0	0	0	0	0	0	18
180509	20420	5173	2750	0	0	0	0	0	0	18
180525	20140	5477	2750	0	0	0	0	0	0	18
180566	19860	5780	2750	0	0	0	0	0	0	18
190093	3800	0	2900	0	0	0	0	0	0	19
190094	4490	0	2900	0	0	0	0	0	0	19
190095	5580	0	2900	0	0	0	0	0	0	19
190096	6760	0	2900	0	0	0	0	0	0	19
190097	7840	0	2900	0	0	0	0	0	0	19
190098	9000	0	2900	0	0	0	0	0	0	19
190099	10160	0	2900	0	0	0	0	0	0	19
190101	11320	0	2900	0	0	0	0	0	0	19
190103	12300	0	2900	0	0	0	0	0	0	19
190104	13480	0	2900	0	0	0	0	0	0	19
190105	14580	0	2900	0	0	0	0	0	0	19
190106	15440	0	2900	0	0	0	0	0	0	19
190107	12288	107	2900	0	0	0	0	0	0	19
190109	6784	135	2900	0	0	0	0	0	0	19
190110	15720	260	2900	0	0	0	0	0	0	19
190111	14478	274	2900	0	0	0	0	0	0	19
190112	4605	293	2900	0	0	0	0	0	0	19
190113	13430	312	2900	0	0	0	0	0	0	19
190115	5644	352	2900	0	0	0	0	0	0	19
190116	3390	380	2900	0	0	0	0	0	0	19
190117	7840	417	2900	0	0	0	0	0	0	19
190118	9000	417	2900	0	0	0	0	0	0	19
190119	10160	417	2900	0	0	0	0	0	0	19
190120	11320	417	2900	0	0	0	0	0	0	19
190121	12214	517	2900	0	0	0	0	0	0	19
190122	6862	545	2900	0	0	0	0	0	0	19
190123	14376	548	2900	0	0	0	0	0	0	19
190124	4721	585	2900	0	0	0	0	0	0	19
190126	15591	607	2900	0	0	0	0	0	0	19
190127	3514	691	2900	0	0	0	0	0	0	19
190128	13356	722	2900	0	0	0	0	0	0	19
190129	5722	762	2900	0	0	0	0	0	0	19
190130	7840	833	2900	0	0	0	0	0	0	19
190131	9000	833	2900	0	0	0	0	0	0	19
190132	10160	833	2900	0	0	0	0	0	0	19
190133	11320	833	2900	0	0	0	0	0	0	19
190134	12141	927	2900	0	0	0	0	0	0	19
190135	14230	938	2900	0	0	0	0	0	0	19
190136	6939	954	2900	0	0	0	0	0	0	19
190137	15462	955	2900	0	0	0	0	0	0	19
190138	4871	974	2900	0	0	0	0	0	0	19
190139	3638	1003	2900	0	0	0	0	0	0	19
190141	16640	1110	2900	0	0	0	0	0	0	19

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
190142	13282	1132	2900	0	0	0	0	0	0	19
190143	5800	1171	2900	0	0	0	0	0	0	19
190144	2480	1230	2900	0	0	0	0	0	0	19
190145	7840	1250	2900	0	0	0	0	0	0	19
190146	9000	1250	2900	0	0	0	0	0	0	19
190147	10160	1250	2900	0	0	0	0	0	0	19
190150	11320	1250	2900	0	0	0	0	0	0	19
190153	14084	1328	2900	0	0	0	0	0	0	19
190154	12067	1337	2900	0	0	0	0	0	0	19
190157	15316	1345	2900	0	0	0	0	0	0	19
190158	16549	1362	2900	0	0	0	0	0	0	19
190161	5021	1363	2900	0	0	0	0	0	0	19
190162	7017	1363	2900	0	0	0	0	0	0	19
190163	3788	1391	2900	0	0	0	0	0	0	19
190164	2556	1420	2900	0	0	0	0	0	0	19
190165	13209	1542	2900	0	0	0	0	0	0	19
190168	5878	1580	2900	0	0	0	0	0	0	19
190173	13937	1718	2900	0	0	0	0	0	0	19
190175	15170	1735	2900	0	0	0	0	0	0	19
190176	5170	1752	2900	0	0	0	0	0	0	19
190179	16402	1752	2900	0	0	0	0	0	0	19
190181	3938	1780	2900	0	0	0	0	0	0	19
190184	2706	1809	2900	0	0	0	0	0	0	19
190189	15024	2125	2900	0	0	0	0	0	0	19
190191	16256	2142	2900	0	0	0	0	0	0	19
190204	4088	2169	2900	0	0	0	0	0	0	19
190210	2856	2197	2900	0	0	0	0	0	0	19
190224	16110	2533	2900	0	0	0	0	0	0	19
190232	3006	2586	2900	0	0	0	0	0	0	19

Input - Aste - Tabella sezioni tipo

Tipo	Nome	Area	Ix	Iy	It	Fx	Fy	Lx	Lx
G		mq	m^4	m^4	m^4			cm	cm
	Tubo40x40x4	0.0	1.260E-07	1.260E-07	1.977E-07	2.248	2.248	4	4
	Tubo40x60x4	0.0	3.450E-07	1.780E-07	3.696E-07	3.244	1.773	4	6

Tabella solai tipo

Sol.N°	Descrizione	Spessore	QP	QF	QVar.	ψ0	ψ1	ψ2	Luce netta	Def	%QX	%QY
		cm	kg/mq	kg/mq	kg/mq							
1	Palco	4	40	30	500	0.70	0.70	0.60	No	Si	50	50
2	Tribuna	6	35	155	500	0.70	0.70	0.60	No	Si	90	10

TABULATI DI VERIFICA

Centri di rigidezza e Centri di massa

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Centri rigidezze

Piano	Kx	Ky	Kxy	K ϕ	X	Y	r/l
	kg/cm	kg/cm	kg/cm	kg*cm/rad	cm	cm	
1	2.198984E06	2.206189E06	1.628790E02	3.561597E11	937	1540	1.172
6	1.056728E06	1.042502E06	1.798381E03	2.635461E11	961	570	1.113
9	1.724216E05	2.373062E05	7.021279E03	3.294639E10	979	982	0.961
12	3.921457E05	3.960719E05	1.512709E02	6.213653E10	937	1537	1.002
13	7.307530E05	7.251995E05	4.209022E03	1.846980E11	962	568	1.012
14	6.894460E05	5.715619E05	8.660106E03	1.665819E11	974	474	0.919
15	3.823312E05	3.844254E05	1.884469E02	6.095237E10	937	1538	1.008
16	9.934956E05	9.235892E05	6.935352E03	2.797850E11	982	420	0.942
17	7.113929E05	5.836625E05	7.005693E03	1.946803E11	984	320	0.892
18	8.460713E05	8.210973E05	1.630316E04	2.430507E11	979	270	0.875
19	3.128407E05	2.444310E05	1.936371E03	5.763533E10	960	169	1.033

Ellissi delle rigidezze

Piano	K $_{\xi}$	K $_{\eta}$	alfa	r $_{\xi}$	r $_{\eta}$
	kg/cm	kg/cm	°	cm	cm
1	2.198980E06	2.206193E06	-1	402	402
6	1.056952E06	1.042278E06	7	503	499
9	1.716706E05	2.380573E05	6	372	438
12	3.921399E05	3.960778E05	-2	396	398
13	7.330187E05	7.229338E05	28	505	502
14	6.900788E05	5.709291E05	4	540	491
15	3.823144E05	3.844422E05	5	398	399
16	9.941770E05	9.229078E05	-6	551	530
17	7.117759E05	5.832794E05	3	578	523
18	8.541201E05	8.130485E05	26	547	533
19	3.128954E05	2.443763E05	2	486	429

Baricentri masse per posizione masse

Piano	Pos.Masse	X	Y	Peso Sism.
		cm	cm	kg
0	1	0	0	0
1	1	979	1583	335
2	1	999	943	309
3	1	1006	781	347
4	1	979	1576	1097
5	1	0	0	0
6	1	1013	617	373
7	1	1015	1015	13082
8	1	1038	454	517
9	1	1008	881	6357
10	1	1012	798	7117
11	1	1043	713	8066
12	1	995	1643	1950
13	1	1019	638	8315
14	1	1018	559	8910
15	1	1010	1641	36314
16	1	1036	474	9611
17	1	1058	389	9776
18	1	1115	300	13849
19	1	1024	104	11249

Risultati Analisi Dinamica - Baricentri masse e masse

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Combinazione masse 1

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	0	0	0	0
1	Si	335	937	1499	12
2	Si	309	958	928	75
3	Si	347	958	757	100
4	Si	1097	937	1492	112
5	Si	0	0	0	0
6	Si	373	958	588	135
7	Si	13082	961	987	155
8	Si	517	976	421	168
9	Si	6357	959	852	170
10	Si	7117	960	767	185
11	Si	8066	962	634	200
12	Si	1950	946	1548	212
13	Si	8315	959	602	215
14	Si	8910	953	521	230
15	Si	36314	960	1546	243
16	Si	9611	969	434	245
17	Si	9776	989	348	260
18	Si	13849	1026	257	275
19	Si	11249	956	78	290

Combinazione masse 2

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	0	0	0	0
1	Si	335	979	1541	12
2	Si	309	999	935	75
3	Si	347	1006	769	100
4	Si	1097	979	1534	112
5	Si	0	0	0	0
6	Si	373	1013	603	135
7	Si	13082	1015	1001	155
8	Si	517	1038	438	168
9	Si	6357	1008	866	170
10	Si	7117	1012	783	185
11	Si	8066	1043	673	200
12	Si	1950	995	1595	212
13	Si	8315	1019	620	215
14	Si	8910	1018	540	230
15	Si	36314	1010	1593	243
16	Si	9611	1036	454	245
17	Si	9776	1058	368	260
18	Si	13849	1115	278	275
19	Si	11249	1024	91	290

Combinazione masse 3

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	0	0	0	0
1	Si	335	937	1583	12
2	Si	309	958	943	75
3	Si	347	958	781	100
4	Si	1097	937	1576	112
5	Si	0	0	0	0
6	Si	373	958	617	135
7	Si	13082	961	1015	155
8	Si	517	976	454	168
9	Si	6357	959	881	170
10	Si	7117	960	798	185
11	Si	8066	962	713	200
12	Si	1950	946	1643	212
13	Si	8315	959	638	215
14	Si	8910	953	559	230
15	Si	36314	960	1641	243
16	Si	9611	969	474	245
17	Si	9776	989	389	260
18	Si	13849	1026	300	275
19	Si	11249	956	104	290

Combinazione masse 4

Piano	Rigido	Massa	X	Y	Z
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COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	0	0	0	0
1	Si	335	895	1541	12
2	Si	309	916	935	75
3	Si	347	910	769	100
4	Si	1097	895	1534	112
5	Si	0	0	0	0
6	Si	373	902	603	135
7	Si	13082	906	1001	155
8	Si	517	913	438	168
9	Si	6357	910	866	170
10	Si	7117	907	783	185
11	Si	8066	880	673	200
12	Si	1950	896	1595	212
13	Si	8315	899	620	215
14	Si	8910	889	540	230
15	Si	36314	911	1593	243
16	Si	9611	902	454	245
17	Si	9776	919	368	260
18	Si	13849	936	278	275
19	Si	11249	888	91	290

Taglianti di piano

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

I taglianti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(I,II) Pm=posizione masse(1,2,...)

Azioni complessive, riferite al sistema WCS, con origine in (0,0,0), i momenti sono comprensivi dei momenti di trasporto $\Theta = F_z \cdot dr / (F_h \cdot H)$ con: F_z =forza verticale, dr =spost medio del piano rispetto al piano inferiore, F_h =tagliante, H =altezza del piano

Combinazione 12-I-1 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-12910	-1421	43597	-14458	-37168	-13458	9421	15885	0	--
1	12798	1375	-28161	4521	28820	7296	9370	15410	120	0.001034
2	0	0	0	0	0	0	0	0	0	0.000000
3	1193	124	-7046	80	-1572	1194	9585	8163	1000	0.004895
4	11658	1282	-37374	5487	10405	6570	9370	15410	1120	0.001010
5	0	0	0	0	0	0	0	0	0	0.000000
6	4110	-104	-15959	-826	3461	4192	9577	6032	1350	0.003478
7	3776	394	-18381	-6703	2753	2497	9515	9664	1550	0.010219
8	5184	-207	-18218	218	1029	6229	9977	4411	1680	0.011869
9	931	-146	-8736	1408	-1205	2461	9609	8719	1700	0.074865
10	2347	259	-10722	660	-61	4215	9574	7757	1850	0.003287
11	3543	561	-19549	9914	-1549	8750	10193	5570	2000	0.002308
12	10450	1356	-36681	-6564	8072	4578	9397	15750	2120	0.005027
13	3015	372	-12330	863	2494	3550	9504	6103	2150	0.027112
14	984	0	-11712	2721	-3394	978	9703	5535	2300	0.002154
15	10322	987	-35441	5423	-226	7231	9634	16084	2430	0.007273
16	3990	-16	-14189	1041	-754	5753	9839	4455	2450	0.054619
17	1414	-84	-12269	2312	1486	1139	9803	3798	2600	0.002059
18	4105	-25	-18020	3285	-199	9192	10012	2652	2750	0.000292
19	2765	-430	-10704	2009	-133	4453	9557	1089	2900	0.012137

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-12910	-1421	0	0	0	0	-12910	-1421
1	12798	1375	0	0	0	0	12798	1375
2	0	0	0	0	0	0	0	0
3	1193	124	0	0	0	0	1193	124
4	-223	-43	0	0	0	0	11658	1282
5	0	0	0	0	0	0	0	0
6	4110	-104	0	0	0	0	4110	-104
7	172	357	0	0	0	0	3776	394
8	5184	-207	0	0	0	0	5184	-207
9	222	-20	0	0	0	0	931	-146
10	-652	-259	0	0	0	0	2347	259
11	3470	633	0	0	0	0	3543	561
12	-327	626	0	0	0	0	10450	1356
13	-1243	53	0	0	0	0	3015	372
14	877	-22	0	0	0	0	984	0
15	-147	-449	0	0	0	0	10322	987
16	-1536	-172	0	0	0	0	3990	-16

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
17	1414	-84	0	0	0	0	1414	-84
18	-1399	-320	0	0	0	0	4105	-25
19	2765	-430	0	0	0	0	2765	-430

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 12-I-2 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-13228	-559	43617	-14206	-37603	-7904	9421	15885	0	--
1	13105	550	-28321	4221	29373	1762	9370	15410	120	0.001030
2	0	0	0	0	0	0	0	0	0	0.000000
3	1179	132	-7276	281	-2188	1160	9585	8163	1000	0.005037
4	11935	557	-36866	3746	12300	1601	9370	15410	1120	0.001079
5	0	0	0	0	0	0	0	0	0	0.000000
6	3934	49	-16028	-925	3463	4034	9577	6032	1350	0.003487
7	3452	413	-18468	-6915	1766	1149	9515	9664	1550	0.009900
8	5191	-230	-18078	219	1140	4191	9977	4411	1680	0.010302
9	1080	-188	-8900	1514	-1206	2052	9609	8719	1700	0.063297
10	2656	708	-10975	670	812	2003	9574	7757	1850	0.002597
11	3671	343	-19182	8928	-4103	5386	10193	5570	2000	0.002238
12	10540	444	-37629	-7357	10017	-1033	9397	15750	2120	0.005931
13	3045	485	-12281	1047	917	2111	9504	6103	2150	0.030875
14	1009	-111	-11522	2965	-4389	458	9703	5535	2300	0.003084
15	10242	556	-35860	5983	-464	4197	9634	16084	2430	0.008919
16	4055	331	-13603	1420	-1959	6575	9839	4455	2450	0.058207
17	1530	-825	-11901	2549	-567	-1381	9803	3798	2600	0.002805
18	4610	-472	-17928	3277	838	2733	10012	2652	2750	0.000949
19	2706	-580	-11043	2116	-1837	1489	9557	1089	2900	0.011213

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-13228	-559	0	0	0	0	-13228	-559
1	13105	550	0	0	0	0	13105	550
2	0	0	0	0	0	0	0	0
3	1179	132	0	0	0	0	1179	132
4	-235	-8	0	0	0	0	11935	557
5	0	0	0	0	0	0	0	0

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
6	3934	49	0	0	0	0	3934	49
7	370	250	0	0	0	0	3452	413
8	5191	-230	0	0	0	0	5191	-230
9	325	-3	0	0	0	0	1080	-188
10	-387	69	0	0	0	0	2656	708
11	3531	486	0	0	0	0	3671	343
12	-395	497	0	0	0	0	10540	444
13	-1057	-29	0	0	0	0	3045	485
14	906	-174	0	0	0	0	1009	-111
15	-207	-315	0	0	0	0	10242	556
16	-1392	95	0	0	0	0	4055	331
17	1530	-825	0	0	0	0	1530	-825
18	-882	-384	0	0	0	0	4610	-472
19	2706	-580	0	0	0	0	2706	-580

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	--	--	--
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	--	--	--
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 12-I-3 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-13415	-1238	42828	-13127	-35895	-2375	9421	15885	0	--
1	13269	1214	-28073	4627	28783	-3601	9370	15410	120	0.001019
2	0	0	0	0	0	0	0	0	0	0.000000
3	1136	89	-6958	75	-1910	1121	9585	8163	1000	0.004878
4	12086	1152	-35599	2909	8291	-3268	9370	15410	1120	0.001264
5	0	0	0	0	0	0	0	0	0	0.000000
6	4154	-123	-15967	-827	3647	313	9577	6032	1350	0.003396
7	3195	366	-18498	-6430	1946	611	9515	9664	1550	0.009897
8	5313	-589	-18330	130	-3047	936	9977	4411	1680	0.009500
9	1186	-100	-8698	1294	-849	1708	9609	8719	1700	0.061753
10	2793	278	-10618	568	1169	2598	9574	7757	1850	0.002624
11	3671	412	-19539	9889	-5616	4093	10193	5570	2000	0.002631
12	10544	821	-38400	-6165	11956	-6578	9397	15750	2120	0.006552
13	3410	640	-12421	887	2085	194	9504	6103	2150	0.031004
14	1330	206	-11419	3017	-5855	-3189	9703	5535	2300	0.000249
15	10259	583	-35840	6479	-898	-2793	9634	16084	2430	0.009432
16	4640	308	-14120	1258	-3905	-1540	9839	4455	2450	0.060516
17	1721	-623	-12150	2309	-1614	-2920	9803	3798	2600	0.002383

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
18	4746	-617	-17897	2928	-743	1861	10012	2652	2750	0.001080
19	2572	-529	-11177	1891	1350	825	9557	1089	2900	0.010002

Piano	FxPil/Isol. kg	FyPil/Isol. kg	FxPar kg	FyPar kg	FxShell kg	FyShell kg	FxTot kg	FyTot kg
0	-13415	-1238	0	0	0	0	-13415	-1238
1	13269	1214	0	0	0	0	13269	1214
2	0	0	0	0	0	0	0	0
3	1136	89	0	0	0	0	1136	89
4	-244	-31	0	0	0	0	12086	1152
5	0	0	0	0	0	0	0	0
6	4154	-123	0	0	0	0	4154	-123
7	513	430	0	0	0	0	3195	366
8	5313	-589	0	0	0	0	5313	-589
9	468	83	0	0	0	0	1186	-100
10	-322	-194	0	0	0	0	2793	278
11	3543	558	0	0	0	0	3671	412
12	-445	403	0	0	0	0	10544	821
13	-846	216	0	0	0	0	3410	640
14	1234	150	0	0	0	0	1330	206
15	-189	-252	0	0	0	0	10259	583
16	-945	400	0	0	0	0	4640	308
17	1721	-623	0	0	0	0	1721	-623
18	-622	-190	0	0	0	0	4746	-617
19	2572	-529	0	0	0	0	2572	-529

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 12-I-4 (SISMAX_SLV)

Piano	Fx kg	Fy kg	Fz kg	Mx kg*m	My kg*m	Mz kg*m	X mm	Y mm	Z mm	Θ
0	-13426	195	42485	-17520	-33355	-12497	9421	15885	0	--
1	13296	-236	-27009	7673	24342	6112	9370	15410	120	0.000982
2	0	0	0	0	0	0	0	0	0	0.000000
3	1153	89	-6725	-98	-2357	1070	9585	8163	1000	0.004640
4	12109	-203	-36916	5903	8557	5626	9370	15410	1120	0.001236
5	0	0	0	0	0	0	0	0	0	0.000000
6	4075	-42	-15901	-719	3405	2198	9577	6032	1350	0.003427

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
7	3524	747	-18727	-7989	3171	-193	9515	9664	1550	0.010248
8	5110	-365	-18609	-380	-1924	2923	9977	4411	1680	0.011510
9	888	-414	-8705	1244	-1206	2778	9609	8719	1700	0.072223
10	2330	-224	-10685	757	-538	5490	9574	7757	1850	0.003095
11	3517	535	-19673	10442	-2061	6752	10193	5570	2000	0.002503
12	10618	-294	-38313	-4852	10032	3235	9397	15750	2120	0.006303
13	3098	366	-12105	1000	2945	1150	9504	6103	2150	0.031045
14	1133	282	-11625	2744	-3132	-1206	9703	5535	2300	0.002023
15	10418	79	-35846	5370	-929	6134	9634	16084	2430	0.008580
16	4084	404	-14205	1198	-1423	966	9839	4455	2450	0.063596
17	1435	-252	-12247	2340	371	251	9803	3798	2600	0.002483
18	4180	1	-18475	3445	-1036	7896	10012	2652	2750	0.000118
19	2626	96	-11179	1864	-173	2506	9557	1089	2900	0.011533

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-13426	195	0	0	0	0	-13426	195
1	13296	-236	0	0	0	0	13296	-236
2	0	0	0	0	0	0	0	0
3	1153	89	0	0	0	0	1153	89
4	-242	2	0	0	0	0	12109	-203
5	0	0	0	0	0	0	0	0
6	4075	-42	0	0	0	0	4075	-42
7	419	619	0	0	0	0	3524	747
8	5110	-365	0	0	0	0	5110	-365
9	202	-285	0	0	0	0	888	-414
10	-682	-818	0	0	0	0	2330	-224
11	3441	609	0	0	0	0	3517	535
12	-438	368	0	0	0	0	10618	-294
13	-1143	197	0	0	0	0	3098	366
14	1060	235	0	0	0	0	1133	282
15	-106	-322	0	0	0	0	10418	79
16	-1340	346	0	0	0	0	4084	404
17	1435	-252	0	0	0	0	1435	-252
18	-1172	-74	0	0	0	0	4180	1
19	2626	96	0	0	0	0	2626	96

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	--	--	--
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Combinazione 13-I-1 (SISMAY_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-411	-13482	43603	17316	-7151	4744	9421	15885	0	--
1	433	13359	-27170	-25893	4418	-4456	9370	15410	120	0.000989
2	0	0	0	0	0	0	0	0	0	0.000000
3	70	448	-11298	317	-96	137	9585	8163	1000	0.011968
4	482	12183	-35923	-7248	4469	-4246	9370	15410	1120	0.002876
5	0	0	0	0	0	0	0	0	0	0.000000
6	532	2335	-15725	-2714	286	1588	9577	6032	1350	0.001698
7	-47	2726	-15779	-3458	2767	43	9515	9664	1550	0.013157
8	113	3478	-17939	-2430	-3154	1637	9977	4411	1680	0.017980
9	141	-2225	-10406	2910	-633	1410	9609	8719	1700	0.060918
10	64	737	-10739	740	93	406	9574	7757	1850	0.013245
11	-51	926	-24814	22718	-4716	2461	10193	5570	2000	0.005841
12	327	11076	-38321	-10666	7067	-3519	9397	15750	2120	0.008095
13	381	1239	-12447	827	2653	2094	9504	6103	2150	0.101942
14	82	628	-13050	3905	-443	2092	9703	5535	2300	0.006497
15	620	10844	-35929	4573	-1373	-4392	9634	16084	2430	0.008506
16	-54	2684	-14144	1042	803	3316	9839	4455	2450	0.103867
17	-187	1852	-14583	4867	3594	2173	9803	3798	2600	0.004126
18	-10	5537	-19556	3936	1510	1739	10012	2652	2750	0.001186
19	173	3427	-10899	1721	-1161	842	9557	1089	2900	0.000706

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-411	-13482	0	0	0	0	-411	-13482
1	433	13359	0	0	0	0	433	13359
2	0	0	0	0	0	0	0	0
3	70	448	0	0	0	0	70	448
4	-5	-247	0	0	0	0	482	12183
5	0	0	0	0	0	0	0	0
6	532	2335	0	0	0	0	532	2335
7	8	1269	0	0	0	0	-47	2726
8	113	3478	0	0	0	0	113	3478
9	-10	-2379	0	0	0	0	141	-2225
10	105	-3958	0	0	0	0	64	737
11	-5	873	0	0	0	0	-51	926
12	-24	306	0	0	0	0	327	11076
13	-271	-1327	0	0	0	0	381	1239
14	74	627	0	0	0	0	82	628
15	42	-552	0	0	0	0	620	10844
16	-232	-1217	0	0	0	0	-54	2684
17	-187	1852	0	0	0	0	-187	1852
18	-149	-270	0	0	0	0	-10	5537
19	173	3427	0	0	0	0	173	3427

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	--	--	--
5	--	--	--
6	100.00	0.00	0.00
7	--	--	--
8	100.00	0.00	0.00
9	--	--	--
10	100.00	0.00	0.00
11	--	--	--
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 13-I-2 (SISMAY_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-730	-12670	40704	14034	-10013	-2869	9421	15885	0	--
1	759	12546	-25490	-24425	9110	2869	9370	15410	120	0.000928
2	0	0	0	0	0	0	0	0	0	0.000000
3	196	427	-11019	49	2307	457	9585	8163	1000	0.010400
4	692	11436	-35140	1483	4012	2594	9370	15410	1120	0.002965
5	0	0	0	0	0	0	0	0	0	0.000000
6	829	2317	-15400	-2510	2702	4149	9577	6032	1350	0.001890
7	954	2294	-16617	-4867	2978	1195	9515	9664	1550	0.014283
8	888	2309	-18516	-2222	-3093	2843	9977	4411	1680	0.025262
9	313	-1905	-10412	2694	31	82	9609	8719	1700	0.069029
10	555	826	-10692	537	-296	1362	9574	7757	1850	0.008942
11	548	989	-24030	19299	339	3979	10193	5570	2000	0.004823
12	518	10581	-37648	-7976	10968	2888	9397	15750	2120	0.008212
13	801	1189	-12526	927	2107	998	9504	6103	2150	0.089482
14	502	361	-12985	3538	1952	-2047	9703	5535	2300	0.005766
15	494	8150	-36355	4806	204	-12646	9634	16084	2430	0.011074
16	735	1775	-14704	795	3396	2965	9839	4455	2450	0.149524
17	175	1270	-13944	4125	3265	1935	9803	3798	2600	0.005130
18	185	4159	-18881	3573	3188	3167	10012	2652	2750	0.001023
19	-254	2638	-10963	2084	516	5763	9557	1089	2900	0.001839

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-730	-12670	0	0	0	0	-730	-12670
1	759	12546	0	0	0	0	759	12546
2	0	0	0	0	0	0	0	0
3	196	427	0	0	0	0	196	427
4	-15	-235	0	0	0	0	692	11436
5	0	0	0	0	0	0	0	0
6	829	2317	0	0	0	0	829	2317
7	-149	1202	0	0	0	0	954	2294
8	888	2309	0	0	0	0	888	2309
9	147	-2085	0	0	0	0	313	-1905
10	221	-3386	0	0	0	0	555	826
11	636	890	0	0	0	0	548	989
12	-61	447	0	0	0	0	518	10581
13	-117	-1343	0	0	0	0	801	1189
14	470	374	0	0	0	0	502	361
15	78	-592	0	0	0	0	494	8150
16	-184	-1133	0	0	0	0	735	1775
17	175	1270	0	0	0	0	175	1270
18	-289	44	0	0	0	0	185	4159
19	-254	2638	0	0	0	0	-254	2638

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
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COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 13-I-3 (SISMAY_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-852	-12816	43538	15509	-7703	-955	9421	15885	0	--
1	852	12689	-27187	-23764	4396	1004	9370	15410	120	0.000988
2	0	0	0	0	0	0	0	0	0	0.000000
3	-9	459	-10994	-247	587	120	9585	8163	1000	0.010527
4	773	11563	-36191	-4731	3744	930	9370	15410	1120	0.002923
5	0	0	0	0	0	0	0	0	0	0.000000
6	112	2707	-15876	-2944	375	602	9577	6032	1350	0.001706
7	305	2546	-15730	-3935	2017	-490	9515	9664	1550	0.013459
8	-925	3730	-18346	-3038	-3360	-875	9977	4411	1680	0.016065
9	136	-1891	-10233	2492	-605	947	9609	8719	1700	0.066173
10	18	1038	-10862	529	-741	188	9574	7757	1850	0.009099
11	-689	1443	-25030	21369	-8044	1785	10193	5570	2000	0.000550
12	446	10490	-37898	-10313	6796	1109	9397	15750	2120	0.007509
13	-162	1647	-12461	767	1789	2885	9504	6103	2150	0.072161
14	-251	645	-13608	3677	-548	2834	9703	5535	2300	0.009753
15	-258	10100	-35853	4885	-905	-2358	9634	16084	2430	0.007548
16	-1270	3071	-14522	977	1102	2115	9839	4455	2450	0.080542
17	-735	2002	-14787	4472	3073	4095	9803	3798	2600	0.004475
18	-839	5712	-19139	3431	1705	1060	10012	2652	2750	0.001034
19	-294	3263	-10909	1954	-3106	187	9557	1089	2900	0.002006

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-852	-12816	0	0	0	0	-852	-12816
1	852	12689	0	0	0	0	852	12689
2	0	0	0	0	0	0	0	0
3	-9	459	0	0	0	0	-9	459
4	-28	-246	0	0	0	0	773	11563
5	0	0	0	0	0	0	0	0
6	112	2707	0	0	0	0	112	2707
7	95	1424	0	0	0	0	305	2546
8	-925	3730	0	0	0	0	-925	3730
9	76	-2103	0	0	0	0	136	-1891
10	110	-3278	0	0	0	0	18	1038
11	-590	1333	0	0	0	0	-689	1443
12	-130	269	0	0	0	0	446	10490
13	-324	-1265	0	0	0	0	-162	1647
14	-267	632	0	0	0	0	-251	645
15	86	-563	0	0	0	0	-258	10100
16	-360	-1098	0	0	0	0	-1270	3071
17	-735	2002	0	0	0	0	-735	2002
18	-58	-273	0	0	0	0	-839	5712
19	-294	3263	0	0	0	0	-294	3263

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	--	--	--
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 13-I-4 (SISMAY_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	--
0	-826	-13098	43447	15683	-7463	5284	9421	15885	0	--
1	825	12964	-27059	-24111	4727	-5119	9370	15410	120	0.000985
2	0	0	0	0	0	0	0	0	0	0.000000
3	-12	454	-10973	54	-2089	-119	9585	8163	1000	0.010762
4	746	11818	-36190	-3304	3536	-4654	9370	15410	1120	0.002948
5	0	0	0	0	0	0	0	0	0	0.000000
6	-660	2368	-15418	-2466	-1214	-3225	9577	6032	1350	0.001785
7	326	2630	-15874	-3765	2962	-706	9515	9664	1550	0.012969
8	-1032	3466	-18719	-2665	-3250	-5375	9977	4411	1680	0.017174
9	148	-1971	-10299	2626	-1798	2090	9609	8719	1700	0.066276
10	-450	842	-10765	559	375	-1117	9574	7757	1850	0.010184
11	-1040	1275	-24768	21896	-14029	-1503	10193	5570	2000	0.004058
12	598	10132	-37456	-13440	8427	-2593	9397	15750	2120	0.008246
13	-381	1526	-12486	836	1227	-1164	9504	6103	2150	0.078612
14	-222	831	-12997	3860	-1646	932	9703	5535	2300	0.007120
15	219	10592	-35286	4518	-211	-7469	9634	16084	2430	0.007120
16	-1080	2826	-14347	1054	-231	-3140	9839	4455	2450	0.086489
17	-244	1733	-14695	4548	11	1325	9803	3798	2600	0.005115
18	-143	5765	-18975	3838	1278	-5826	10012	2652	2750	0.000898
19	232	3331	-11218	2597	6217	-2170	9557	1089	2900	0.000529

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-826	-13098	0	0	0	0	-826	-13098
1	825	12964	0	0	0	0	825	12964
2	0	0	0	0	0	0	0	0
3	-12	454	0	0	0	0	-12	454
4	-30	-241	0	0	0	0	746	11818
5	0	0	0	0	0	0	0	0
6	-660	2368	0	0	0	0	-660	2368
7	201	1316	0	0	0	0	326	2630
8	-1032	3466	0	0	0	0	-1032	3466
9	-58	-2082	0	0	0	0	148	-1971
10	13	-3410	0	0	0	0	-450	842
11	-994	1222	0	0	0	0	-1040	1275
12	-96	276	0	0	0	0	598	10132
13	102	-1147	0	0	0	0	-381	1526
14	-174	880	0	0	0	0	-222	831
15	74	-491	0	0	0	0	219	10592
16	69	-1081	0	0	0	0	-1080	2826
17	-244	1733	0	0	0	0	-244	1733
18	155	-48	0	0	0	0	-143	5765
19	232	3331	0	0	0	0	232	3331

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 28-I-1 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-10217	-1115	43070	-16017	-29127	-11453	9421	15885	0	--
1	10113	1069	-27593	6117	21386	6552	9370	15410	120	0.001112
2	0	0	0	0	0	0	0	0	0	0.000000
3	947	111	-7029	75	-1367	879	9585	8163	1000	0.004895
4	10132	1083	-37035	5843	9432	6503	9370	15410	1120	0.001324
5	0	0	0	0	0	0	0	0	0	0.000000
6	3167	-28	-15955	-841	2643	3195	9577	6032	1350	0.003515
7	3600	528	-18433	-6761	2871	2643	9515	9664	1550	0.010886
8	3705	-121	-18457	-256	-2009	4304	9977	4411	1680	0.017236
9	711	-146	-8692	1380	-994	1469	9609	8719	1700	0.093527
10	1863	477	-10600	723	120	2545	9574	7757	1850	0.003843
11	2543	699	-19575	10036	-1588	7334	10193	5570	2000	0.002178
12	8966	1085	-36934	-6562	7925	4283	9397	15750	2120	0.006326
13	2349	431	-12255	923	2533	2637	9504	6103	2150	0.034738
14	693	6	-11658	2851	-2562	901	9703	5535	2300	0.003261
15	8789	897	-35539	5384	-392	6564	9634	16084	2430	0.008613
16	2823	164	-14076	1127	-545	4313	9839	4455	2450	0.077764
17	1010	-32	-12295	2381	1572	719	9803	3798	2600	0.002207
18	3652	235	-18030	3387	797	9754	10012	2652	2750	0.001496
19	2848	-278	-10854	1984	212	5267	9557	1089	2900	0.013704

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-10217	-1115	0	0	0	0	-10217	-1115
1	10113	1069	0	0	0	0	10113	1069
2	0	0	0	0	0	0	0	0
3	947	111	0	0	0	0	947	111
4	-200	-40	0	0	0	0	10132	1083
5	0	0	0	0	0	0	0	0
6	3167	-28	0	0	0	0	3167	-28
7	172	492	0	0	0	0	3600	528
8	3705	-121	0	0	0	0	3705	-121
9	105	-32	0	0	0	0	711	-146
10	-528	-217	0	0	0	0	1863	477
11	2478	763	0	0	0	0	2543	699
12	-328	546	0	0	0	0	8966	1085

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
13	-960	71	0	0	0	0	2349	431
14	621	-3	0	0	0	0	693	6
15	-109	-400	0	0	0	0	8789	897
16	-1138	-115	0	0	0	0	2823	164
17	1010	-32	0	0	0	0	1010	-32
18	-937	-235	0	0	0	0	3652	235
19	2848	-278	0	0	0	0	2848	-278

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	--	--	--
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 28-I-2 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-10478	-470	43615	-14283	-31670	-7124	9421	15885	0	--
1	10361	459	-28294	4271	24274	2314	9370	15410	120	0.001129
2	0	0	0	0	0	0	0	0	0	0.000000
3	934	127	-7211	251	-1935	879	9585	8163	1000	0.004986
4	10379	489	-36312	3110	9699	2308	9370	15410	1120	0.001358
5	0	0	0	0	0	0	0	0	0	0.000000
6	2960	-130	-16004	-805	2440	3781	9577	6032	1350	0.003594
7	3311	412	-18325	-6845	1259	922	9515	9664	1550	0.010677
8	3718	-256	-17840	722	-1806	2764	9977	4411	1680	0.014925
9	735	-281	-8527	1548	-2172	2501	9609	8719	1700	0.082914
10	1922	470	-10746	691	409	3083	9574	7757	1850	0.003586
11	2631	288	-19175	9629	-2950	4948	10193	5570	2000	0.001989
12	9008	386	-37733	-7566	9477	-887	9397	15750	2120	0.007626
13	2110	162	-12311	992	1000	3808	9504	6103	2150	0.047135
14	723	-103	-11283	3149	-3998	540	9703	5535	2300	0.003122
15	8667	556	-35891	5447	-694	3668	9634	16084	2430	0.010599
16	2964	-62	-13556	1683	-2207	4129	9839	4455	2450	0.080260
17	1123	-611	-12010	2574	104	-679	9803	3798	2600	0.003092
18	4007	-293	-17870	3392	1635	3860	10012	2652	2750	0.001282
19	2769	-294	-11165	2080	-1407	2127	9557	1089	2900	0.012756

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-10478	-470	0	0	0	0	-10478	-470
1	10361	459	0	0	0	0	10361	459

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
2	0	0	0	0	0	0	0	0
3	934	127	0	0	0	0	934	127
4	-213	-11	0	0	0	0	10379	489
5	0	0	0	0	0	0	0	0
6	2960	-130	0	0	0	0	2960	-130
7	379	262	0	0	0	0	3311	412
8	3718	-256	0	0	0	0	3718	-256
9	89	-108	0	0	0	0	735	-281
10	-474	-117	0	0	0	0	1922	470
11	2504	418	0	0	0	0	2631	288
12	-405	489	0	0	0	0	9008	386
13	-964	-158	0	0	0	0	2110	162
14	653	-143	0	0	0	0	723	-103
15	-159	-171	0	0	0	0	8667	556
16	-894	-135	0	0	0	0	2964	-62
17	1123	-611	0	0	0	0	1123	-611
18	-530	-329	0	0	0	0	4007	-293
19	2769	-294	0	0	0	0	2769	-294

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 28-I-3 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-10706	-1040	43406	-14668	-29385	-1665	9421	15885	0	--
1	10566	1020	-28051	4624	23690	-3022	9370	15410	120	0.001117
2	0	0	0	0	0	0	0	0	0	0.000000
3	900	103	-6955	78	-1777	794	9585	8163	1000	0.004926
4	10585	1396	-36206	3600	7221	-4060	9370	15410	1120	0.001494
5	0	0	0	0	0	0	0	0	0	0.000000
6	3274	-104	-15955	-818	2721	-92	9577	6032	1350	0.003438
7	3102	337	-18581	-7089	2475	445	9515	9664	1550	0.010848
8	3826	-309	-18319	115	-3376	181	9977	4411	1680	0.014164
9	1012	-129	-8441	1336	-2017	1267	9609	8719	1700	0.068419
10	2314	130	-10449	690	225	879	9574	7757	1850	0.002879
11	2777	370	-19629	10035	-4704	2453	10193	5570	2000	0.002628
12	9043	725	-38436	-6319	11657	-6998	9397	15750	2120	0.008146
13	2738	219	-12417	853	2150	544	9504	6103	2150	0.040383

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
14	1024	192	-11459	3003	-5297	-3111	9703	5535	2300	0.000165
15	8749	732	-35713	6267	-1180	-2668	9634	16084	2430	0.011131
16	3501	312	-14063	1274	-3249	-2550	9839	4455	2450	0.080799
17	1284	-459	-12187	2142	-462	-2586	9803	3798	2600	0.002978
18	4110	-173	-17592	3508	-194	1889	10012	2652	2750	0.000987
19	2524	-375	-11097	1905	1435	2730	9557	1089	2900	0.011414

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-10706	-1040	0	0	0	0	-10706	-1040
1	10566	1020	0	0	0	0	10566	1020
2	0	0	0	0	0	0	0	0
3	900	103	0	0	0	0	900	103
4	-224	-32	0	0	0	0	10585	1396
5	0	0	0	0	0	0	0	0
6	3274	-104	0	0	0	0	3274	-104
7	536	388	0	0	0	0	3102	337
8	3826	-309	0	0	0	0	3826	-309
9	392	39	0	0	0	0	1012	-129
10	-211	-221	0	0	0	0	2314	130
11	2658	505	0	0	0	0	2777	370
12	-465	397	0	0	0	0	9043	725
13	-607	-28	0	0	0	0	2738	219
14	959	157	0	0	0	0	1024	192
15	-127	-251	0	0	0	0	8749	732
16	-566	285	0	0	0	0	3501	312
17	1284	-459	0	0	0	0	1284	-459
18	-253	-213	0	0	0	0	4110	-173
19	2524	-375	0	0	0	0	2524	-375

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 28-I-4 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-10701	75	42710	-16903	-28386	-10511	9421	15885	0	--
1	10576	-117	-27230	6933	20255	5437	9370	15410	120	0.001086
2	0	0	0	0	0	0	0	0	0	0.000000

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
3	911	94	-6783	-77	-2078	813	9585	8163	1000	0.004677
4	10595	-134	-36641	4955	9033	5451	9370	15410	1120	0.001551
5	0	0	0	0	0	0	0	0	0	0.000000
6	3173	-34	-15923	-767	2569	1505	9577	6032	1350	0.003487
7	3408	432	-18884	-8094	2953	890	9515	9664	1550	0.011287
8	3683	-230	-18536	-325	-2446	1658	9977	4411	1680	0.016702
9	692	-324	-8655	1265	-923	2151	9609	8719	1700	0.094279
10	1815	-146	-10666	792	-228	4570	9574	7757	1850	0.004150
11	2396	566	-19665	10441	-2142	7544	10193	5570	2000	0.002537
12	9130	42	-38041	-5957	10338	2343	9397	15750	2120	0.007865
13	2417	433	-12189	993	2625	482	9504	6103	2150	0.040814
14	692	114	-11671	2729	-3071	563	9703	5535	2300	0.003483
15	8897	94	-35800	5406	-780	4390	9634	16084	2430	0.010165
16	2858	337	-14141	1225	-1224	1675	9839	4455	2450	0.090851
17	1051	-155	-12291	2383	715	-6	9803	3798	2600	0.002935
18	3607	43	-18491	3614	-298	7398	10012	2652	2750	0.000657
19	2682	-134	-11112	1931	-448	2886	9557	1089	2900	0.012675

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-10701	75	0	0	0	0	-10701	75
1	10576	-117	0	0	0	0	10576	-117
2	0	0	0	0	0	0	0	0
3	911	94	0	0	0	0	911	94
4	-220	-10	0	0	0	0	10595	-134
5	0	0	0	0	0	0	0	0
6	3173	-34	0	0	0	0	3173	-34
7	423	307	0	0	0	0	3408	432
8	3683	-230	0	0	0	0	3683	-230
9	104	-205	0	0	0	0	692	-324
10	-550	-744	0	0	0	0	1815	-146
11	2327	635	0	0	0	0	2396	566
12	-445	638	0	0	0	0	9130	42
13	-900	184	0	0	0	0	2417	433
14	645	87	0	0	0	0	692	114
15	-74	-510	0	0	0	0	8897	94
16	-1057	154	0	0	0	0	2858	337
17	1051	-155	0	0	0	0	1051	-155
18	-794	-115	0	0	0	0	3607	43
19	2682	-134	0	0	0	0	2682	-134

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 29-I-1 (SISMAX_SLD)

Piano	Fx kg	Fy kg	Fz kg	Mx kg*m	My kg*m	Mz kg*m	X mm	Y mm	Z mm	Θ
0	-363	-10611	43702	10567	-7181	2833	9421	15885	0	--
1	387	10497	-27390	-19468	4389	-2694	9370	15410	120	0.001095
2	0	0	0	0	0	0	0	0	0	0.000000
3	22	389	-10478	275	-140	51	9585	8163	1000	0.010552
4	389	10518	-35880	-5024	3947	-2698	9370	15410	1120	0.002977
5	0	0	0	0	0	0	0	0	0	0.000000
6	322	1762	-15817	-2222	266	766	9577	6032	1350	0.001638
7	-29	2340	-16157	-3952	2549	5	9515	9664	1550	0.013484
8	86	2434	-18261	-1682	-3771	849	9977	4411	1680	0.022559
9	117	-1893	-10044	2611	-555	1095	9609	8719	1700	0.059329
10	87	545	-10700	774	385	381	9574	7757	1850	0.015027
11	-24	721	-23327	19304	-3679	1418	10193	5570	2000	0.007061
12	674	9594	-38137	-10272	6830	-2783	9397	15750	2120	0.008791
13	304	888	-12405	847	2492	1446	9504	6103	2150	0.129980
14	122	290	-12750	3692	-1218	502	9703	5535	2300	0.009485
15	618	9439	-35827	4635	-1355	-3495	9634	16084	2430	0.009474
16	-39	1965	-14115	1236	-412	2120	9839	4455	2450	0.133563
17	-157	1318	-13904	4175	2982	1403	9803	3798	2600	0.004071
18	-69	4090	-19160	3861	472	1680	10012	2652	2750	0.000747
19	176	2527	-10701	1831	-493	624	9557	1089	2900	0.000582

Piano	FxPil/Isol. kg	FyPil/Isol. kg	FxPar kg	FyPar kg	FxShell kg	FyShell kg	FxTot kg	FyTot kg
0	-363	-10611	0	0	0	0	-363	-10611
1	387	10497	0	0	0	0	387	10497
2	0	0	0	0	0	0	0	0
3	22	389	0	0	0	0	22	389
4	-2	-214	0	0	0	0	389	10518
5	0	0	0	0	0	0	0	0
6	322	1762	0	0	0	0	322	1762
7	8	1131	0	0	0	0	-29	2340
8	86	2434	0	0	0	0	86	2434
9	-39	-2013	0	0	0	0	117	-1893
10	125	-3319	0	0	0	0	87	545
11	4	688	0	0	0	0	-24	721
12	-25	366	0	0	0	0	674	9594
13	-159	-1083	0	0	0	0	304	888
14	123	297	0	0	0	0	122	290
15	40	-537	0	0	0	0	618	9439
16	-173	-875	0	0	0	0	-39	1965
17	-157	1318	0	0	0	0	-157	1318
18	-75	-130	0	0	0	0	-69	4090
19	176	2527	0	0	0	0	176	2527

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	--	--	--
5	--	--	--
6	100.00	0.00	0.00
7	--	--	--
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	--	--	--
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 29-I-2 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-606	-9912	41527	2594	-9839	-3728	9421	15885	0	--
1	638	9800	-26163	-12688	8026	3574	9370	15410	120	0.001045
2	0	0	0	0	0	0	0	0	0	0.000000
3	152	363	-10260	39	2325	386	9585	8163	1000	0.009460
4	673	9815	-35354	2175	4115	3545	9370	15410	1120	0.003025
5	0	0	0	0	0	0	0	0	0	0.000000
6	583	1717	-15616	-2097	1952	3206	9577	6032	1350	0.001908
7	843	1916	-16347	-4500	166	1310	9515	9664	1550	0.014550
8	570	1724	-18846	-1690	-2471	2476	9977	4411	1680	0.030275
9	328	-1610	-10052	2425	209	-99	9609	8719	1700	0.067087
10	392	671	-10691	616	-127	1024	9574	7757	1850	0.010060
11	451	738	-23024	17441	2884	2436	10193	5570	2000	0.004584
12	513	9027	-37943	-8268	11225	3976	9397	15750	2120	0.008692
13	448	1077	-12443	832	2297	2752	9504	6103	2150	0.097947
14	327	207	-12772	3377	372	-1213	9703	5535	2300	0.008057
15	655	9016	-35711	4982	-1655	-3041	9634	16084	2430	0.009343
16	539	1371	-14423	1004	836	1663	9839	4455	2450	0.177486
17	126	943	-13634	3722	3952	1650	9803	3798	2600	0.005431
18	58	3075	-18678	3487	1995	2918	10012	2652	2750	0.001257
19	-242	1820	-10642	1972	-674	5030	9557	1089	2900	0.002905

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-606	-9912	0	0	0	0	-606	-9912
1	638	9800	0	0	0	0	638	9800
2	0	0	0	0	0	0	0	0
3	152	363	0	0	0	0	152	363
4	-15	-204	0	0	0	0	673	9815
5	0	0	0	0	0	0	0	0
6	583	1717	0	0	0	0	583	1717
7	-135	1015	0	0	0	0	843	1916
8	570	1724	0	0	0	0	570	1724
9	172	-1763	0	0	0	0	328	-1610
10	216	-2837	0	0	0	0	392	671
11	520	659	0	0	0	0	451	738
12	-61	411	0	0	0	0	513	9027
13	-267	-855	0	0	0	0	448	1077
14	308	223	0	0	0	0	327	207
15	70	-604	0	0	0	0	655	9016
16	-64	-860	0	0	0	0	539	1371
17	126	943	0	0	0	0	126	943
18	-325	-3	0	0	0	0	58	3075
19	-242	1820	0	0	0	0	-242	1820

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	--	--	--
19	100.00	0.00	0.00

Combinazione 29-I-3 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-510	-10119	43606	9078	-7734	-1654	9421	15885	0	--
1	512	9999	-27350	-17741	4428	1712	9370	15410	120	0.001091
2	0	0	0	0	0	0	0	0	0	0.000000
3	-26	388	-10278	-241	426	83	9585	8163	1000	0.009652
4	506	10012	-36062	-3243	3344	1739	9370	15410	1120	0.002996
5	0	0	0	0	0	0	0	0	0	0.000000
6	82	1982	-15932	-2388	356	404	9577	6032	1350	0.001667
7	496	2192	-15961	-4431	2278	-39	9515	9664	1550	0.013867
8	-669	2680	-18350	-2180	-3219	-636	9977	4411	1680	0.019985
9	124	-1604	-9966	2260	-503	739	9609	8719	1700	0.069276
10	-6	820	-10689	631	173	63	9574	7757	1850	0.010255
11	-471	847	-23503	18003	-6362	1481	10193	5570	2000	0.002257
12	336	9024	-37978	-9741	7186	1451	9397	15750	2120	0.008424
13	-149	1195	-12456	712	1620	2480	9504	6103	2150	0.094093
14	-229	469	-13088	3321	-901	1735	9703	5535	2300	0.011425
15	121	8644	-35791	5020	-976	-1626	9634	16084	2430	0.008483
16	-950	2378	-14499	1109	1647	1543	9839	4455	2450	0.098374
17	-419	1442	-14118	3788	2538	3388	9803	3798	2600	0.005178
18	-564	4354	-18793	3400	1655	412	10012	2652	2750	0.001186
19	-244	2293	-10666	2149	-3198	167	9557	1089	2900	0.003412

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-510	-10119	0	0	0	0	-510	-10119
1	512	9999	0	0	0	0	512	9999
2	0	0	0	0	0	0	0	0
3	-26	388	0	0	0	0	-26	388
4	-25	-214	0	0	0	0	506	10012
5	0	0	0	0	0	0	0	0
6	82	1982	0	0	0	0	82	1982
7	85	1280	0	0	0	0	496	2192
8	-669	2680	0	0	0	0	-669	2680
9	56	-1786	0	0	0	0	124	-1604
10	116	-2780	0	0	0	0	-6	820
11	-394	759	0	0	0	0	-471	847
12	-128	264	0	0	0	0	336	9024
13	-281	-1002	0	0	0	0	-149	1195
14	-233	470	0	0	0	0	-229	469
15	77	-578	0	0	0	0	121	8644
16	-252	-733	0	0	0	0	-950	2378
17	-419	1442	0	0	0	0	-419	1442
18	-8	44	0	0	0	0	-564	4354
19	-244	2293	0	0	0	0	-244	2293

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	--	--	--
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Combinazione 29-I-4 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-669	-10360	43504	9182	-7436	4710	9421	15885	0	--
1	668	10236	-27230	-17970	4719	-4610	9370	15410	120	0.001087
2	0	0	0	0	0	0	0	0	0	0.000000
3	-16	382	-10238	3	-2273	-143	9585	8163	1000	0.009818
4	766	10252	-36330	-2325	5803	-4790	9370	15410	1120	0.003048
5	0	0	0	0	0	0	0	0	0	0.000000
6	-482	1736	-15422	-2125	-1037	-2774	9577	6032	1350	0.001754
7	81	2243	-16292	-4279	2762	-1002	9515	9664	1550	0.013781
8	-671	2469	-18442	-1974	-2504	-4330	9977	4411	1680	0.021073
9	134	-1673	-9967	2351	-1764	1908	9609	8719	1700	0.066592
10	-315	668	-10746	631	235	-940	9574	7757	1850	0.011509
11	-639	740	-23298	18648	-10552	-1031	10193	5570	2000	0.005004
12	608	9345	-37880	-10361	6982	-4429	9397	15750	2120	0.008287
13	-433	1084	-12359	778	2191	-1282	9504	6103	2150	0.095916
14	-236	539	-12748	3562	-2547	1106	9703	5535	2300	0.008456
15	383	9059	-35511	4381	-932	-5872	9634	16084	2430	0.007864
16	-673	2111	-14339	1035	-65	-2596	9839	4455	2450	0.108298
17	-142	1220	-14034	3941	-527	542	9803	3798	2600	0.005677
18	32	4305	-18683	3657	1476	-5217	10012	2652	2750	0.001017
19	304	2348	-10908	2414	4053	-1927	9557	1089	2900	0.003515

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-669	-10360	0	0	0	0	-669	-10360
1	668	10236	0	0	0	0	668	10236
2	0	0	0	0	0	0	0	0
3	-16	382	0	0	0	0	-16	382
4	-23	-210	0	0	0	0	766	10252
5	0	0	0	0	0	0	0	0
6	-482	1736	0	0	0	0	-482	1736
7	241	1186	0	0	0	0	81	2243
8	-671	2469	0	0	0	0	-671	2469
9	-59	-1762	0	0	0	0	134	-1673
10	14	-2884	0	0	0	0	-315	668
11	-609	705	0	0	0	0	-639	740
12	-93	333	0	0	0	0	608	9345
13	67	-905	0	0	0	0	-433	1084
14	-197	582	0	0	0	0	-236	539
15	73	-485	0	0	0	0	383	9059
16	39	-759	0	0	0	0	-673	2111
17	-142	1220	0	0	0	0	-142	1220
18	143	102	0	0	0	0	32	4305

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
19	304	2348	0	0	0	0	304	2348

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00
4	100.00	0.00	0.00
5	--	--	--
6	100.00	0.00	0.00
7	100.00	0.00	0.00
8	100.00	0.00	0.00
9	100.00	0.00	0.00
10	100.00	0.00	0.00
11	100.00	0.00	0.00
12	100.00	0.00	0.00
13	100.00	0.00	0.00
14	100.00	0.00	0.00
15	100.00	0.00	0.00
16	100.00	0.00	0.00
17	100.00	0.00	0.00
18	100.00	0.00	0.00
19	100.00	0.00	0.00

Verifica Degli Spostamenti Relativi

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Interp.	Comb.	ηXv mm	ηXh mm	ηYv mm	ηYh mm	Nodo1	Nodo2	η mm	ηAmm mm	Cs
0-7	(28+29)-IV-3	0.00	0.10	0.07	0.87	1	70001	0.94	7.75	8.3
0-7	(28+29)-V-3	0.00	0.94	0.09	0.67	2	70002	0.94	7.75	8.2
0-7	(28+29)-V-4	0.00	0.81	0.08	0.11	3	70003	0.82	7.75	9.5
0-1	(28+29)-I-4	0.01	0.09	0.00	0.01	4	10004	0.10	0.60	6.0
0-1	(28+29)-IV-4	0.00	0.00	0.00	0.10	5	10005	0.10	0.60	6.1
0-1	(28+29)-IV-4	0.00	0.00	0.00	0.08	6	10006	0.08	0.60	7.2
0-1	(28+29)-I-4	0.00	0.09	0.00	0.03	7	10007	0.10	0.60	6.3
0-1	(28+29)-V-4	0.00	0.09	0.00	0.02	8	10008	0.09	0.60	6.5
0-1	(28+29)-II-3	0.00	0.00	0.00	0.08	9	10009	0.08	0.60	7.1
0-1	(28+29)-II-4	0.00	0.00	0.00	0.09	10	10010	0.09	0.60	6.5
0-1	(28+29)-V-3	0.01	0.09	0.00	0.00	11	10011	0.10	0.60	6.0
0-7	(28+29)-V-3	0.00	0.82	0.09	0.16	12	70012	0.82	7.75	9.5
0-12	(28+29)-VIII-4	0.00	0.08	0.01	0.56	13	120013	0.57	10.60	19
0-1	(28+29)-III-4	0.01	0.09	0.00	0.00	14	10014	0.09	0.60	6.5
0-4	(28+29)-IV-4	0.03	0.08	0.05	0.24	15	40015	0.29	5.60	19
0-4	(28+29)-II-4	0.04	0.21	0.05	0.08	16	40016	0.25	5.60	23
0-1	(28+29)-III-4	0.00	0.09	0.00	0.00	17	10017	0.09	0.60	6.7
0-1	(28+29)-I-3	0.00	0.09	0.00	0.00	18	10018	0.09	0.60	6.9
0-4	(28+29)-I-3	0.04	0.20	0.05	0.08	19	40019	0.24	5.60	23
0-4	(28+29)-II-4	0.03	0.04	0.05	0.22	20	40020	0.27	5.60	21
0-1	(28+29)-I-4	0.00	0.08	0.00	0.00	21	10021	0.09	0.60	6.7
0-12	(28+29)-VI-3	0.01	0.07	0.05	1.87	22	120022	1.92	10.60	5.5
0-12	(28+29)-VIII-4	0.00	0.09	0.01	0.56	23	120023	0.57	10.60	19

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
0-1	(28+29)-III-3	0.01	0.10	0.00	0.00	24	10024	0.11	0.60	5.7
0-4	(28+29)-IV-4	0.02	0.08	0.04	0.22	25	40025	0.26	5.60	21
0-4	(28+29)-III-4	0.04	0.23	0.04	0.03	26	40026	0.27	5.60	21
0-1	(28+29)-III-4	0.00	0.10	0.00	0.00	27	10027	0.10	0.60	6.1
0-1	(28+29)-I-3	0.00	0.09	0.00	0.00	28	10028	0.10	0.60	6.3
0-4	(28+29)-I-3	0.04	0.22	0.04	0.09	29	40029	0.27	5.60	21
0-4	(28+29)-I-3	0.03	0.22	0.04	0.04	30	40030	0.25	5.60	22
0-1	(28+29)-I-4	0.00	0.10	0.00	0.00	31	10031	0.10	0.60	5.9
0-12	(28+29)-VI-3	0.01	0.08	0.05	1.87	32	120032	1.92	10.60	5.5
0-12	(28+29)-VIII-4	0.00	0.10	0.01	0.56	33	120033	0.57	10.60	19
0-1	(28+29)-IV-4	0.01	0.03	0.00	0.09	34	10034	0.09	0.60	6.3
0-1	(28+29)-IV-4	0.00	0.00	0.00	0.10	35	10035	0.10	0.60	6.1
0-1	(28+29)-IV-3	0.00	0.00	0.00	0.09	36	10036	0.09	0.60	6.8
0-1	(28+29)-IV-4	0.00	0.02	0.00	0.09	37	10037	0.09	0.60	6.7
0-1	(28+29)-II-3	0.00	0.03	0.00	0.08	38	10038	0.09	0.60	6.9
0-1	(28+29)-II-3	0.00	0.00	0.00	0.09	39	10039	0.09	0.60	6.6
0-1	(28+29)-II-4	0.00	0.00	0.00	0.09	40	10040	0.09	0.60	6.5
0-1	(28+29)-VI-4	0.00	0.01	0.00	0.09	41	10041	0.09	0.60	6.7
0-12	(28+29)-VI-3	0.01	0.09	0.05	1.88	42	120042	1.93	10.60	5.5
0-12	(28+29)-VIII-4	0.00	0.08	0.01	0.56	43	120043	0.57	10.60	19
0-1	(28+29)-IV-4	0.01	0.02	0.00	0.09	44	10044	0.09	0.60	6.6
0-1	(28+29)-IV-4	0.00	0.00	0.00	0.09	45	10045	0.09	0.60	6.6
0-1	(28+29)-VIII-4	0.00	0.00	0.00	0.09	46	10046	0.09	0.60	6.9
0-1	(28+29)-IV-4	0.00	0.02	0.00	0.08	47	10047	0.09	0.60	7.0
0-1	(28+29)-II-3	0.00	0.02	0.00	0.08	48	10048	0.08	0.60	7.3
0-1	(28+29)-VI-4	0.00	0.00	0.00	0.09	49	10049	0.09	0.60	6.7
0-1	(28+29)-II-4	0.00	0.00	0.00	0.09	50	10050	0.09	0.60	7.0
0-1	(28+29)-VI-4	0.00	0.02	0.00	0.09	51	10051	0.09	0.60	6.9
0-12	(28+29)-VI-3	0.01	0.11	0.05	1.88	52	120052	1.93	10.60	5.5
0-12	(28+29)-VIII-4	0.00	0.11	0.01	0.56	53	120053	0.57	10.60	18
0-1	(28+29)-VII-4	0.01	0.09	0.00	0.00	54	10054	0.10	0.60	5.9
0-4	(28+29)-IV-4	0.02	0.03	0.04	0.22	55	40055	0.25	5.60	22
0-4	(28+29)-VII-3	0.04	0.23	0.04	0.05	56	40056	0.27	5.60	21
0-1	(28+29)-VII-3	0.00	0.10	0.00	0.00	57	10057	0.10	0.60	6.0
0-1	(28+29)-V-4	0.00	0.10	0.00	0.00	58	10058	0.10	0.60	6.2
0-4	(28+29)-V-4	0.04	0.22	0.04	0.07	59	40059	0.26	5.60	21
0-4	(28+29)-V-4	0.03	0.22	0.04	0.08	60	40060	0.25	5.60	22
0-1	(28+29)-V-4	0.00	0.09	0.00	0.00	61	10061	0.10	0.60	6.1
0-12	(28+29)-VI-3	0.01	0.10	0.05	1.88	62	120062	1.93	10.60	5.5
0-12	(28+29)-VIII-4	0.00	0.13	0.01	0.56	63	120063	0.57	10.60	18
0-1	(28+29)-VII-4	0.01	0.10	0.00	0.00	64	10064	0.10	0.60	5.7
0-4	(28+29)-VII-4	0.02	0.23	0.03	0.04	65	40065	0.26	5.60	22
0-4	(28+29)-VII-4	0.04	0.23	0.03	0.07	66	40066	0.27	5.60	21
0-1	(28+29)-VII-4	0.00	0.10	0.00	0.00	67	10067	0.10	0.60	6.0
0-1	(28+29)-V-4	0.00	0.10	0.00	0.00	68	10068	0.10	0.60	6.2
0-4	(28+29)-V-4	0.04	0.23	0.03	0.08	69	40069	0.27	5.60	21
0-4	(28+29)-V-4	0.03	0.22	0.03	0.08	70	40070	0.25	5.60	22
0-1	(28+29)-V-4	0.00	0.10	0.00	0.00	71	10071	0.10	0.60	5.9
0-12	(28+29)-VI-3	0.01	0.10	0.05	1.88	72	120072	1.93	10.60	5.5
0-12	(28+29)-VIII-4	0.00	0.16	0.01	0.57	73	120073	0.57	10.60	18
0-1	(28+29)-V-4	0.01	0.11	0.00	0.02	74	10074	0.11	0.60	5.4
0-1	(28+29)-VIII-3	0.00	0.00	0.00	0.09	75	10075	0.09	0.60	6.5
0-1	(28+29)-IV-3	0.00	0.00	0.00	0.08	76	10076	0.09	0.60	6.9
0-1	(28+29)-V-4	0.00	0.11	0.00	0.03	77	10077	0.11	0.60	5.6
0-1	(28+29)-V-4	0.00	0.10	0.00	0.02	78	10078	0.10	0.60	5.8
0-1	(28+29)-VI-4	0.00	0.00	0.00	0.09	79	10079	0.09	0.60	6.7
0-1	(28+29)-VI-4	0.00	0.00	0.00	0.09	80	10080	0.09	0.60	6.8
0-1	(28+29)-V-3	0.00	0.10	0.00	0.05	81	10081	0.11	0.60	5.5
0-12	(28+29)-VI-3	0.01	0.05	0.04	1.88	82	120082	1.93	10.60	5.5
0-12	(28+29)-V-3	0.00	2.46	0.01	0.26	83	120083	2.46	10.60	4.3
0-12	(28+29)-V-3	0.00	2.46	0.00	0.01	84	120084	2.47	10.60	4.3
0-12	(28+29)-V-3	0.01	2.47	0.01	0.10	85	120085	2.47	10.60	4.3
0-12	(28+29)-V-3	0.01	2.47	0.01	0.05	86	120086	2.47	10.60	4.3
0-12	(28+29)-V-3	0.01	2.47	0.01	0.08	87	120087	2.48	10.60	4.3
0-12	(28+29)-V-3	0.01	2.47	0.01	0.09	88	120088	2.48	10.60	4.3
0-12	(28+29)-V-3	0.01	2.47	0.01	0.08	89	120089	2.48	10.60	4.3
0-12	(28+29)-V-3	0.01	2.47	0.01	0.07	90	120090	2.48	10.60	4.3
0-12	(28+29)-V-3	0.01	2.46	0.00	0.00	91	120091	2.48	10.60	4.3
0-12	(28+29)-V-3	0.01	2.46	0.04	1.17	92	120092	2.48	10.60	4.3
1-4	(28+29)-IV-3	0.03	0.02	0.04	0.15	10004	40004	0.19	5.00	27
1-4	(28+29)-I-4	0.02	0.22	0.05	0.06	10005	40005	0.25	5.00	20
1-4	(28+29)-I-4	0.03	0.23	0.05	0.04	10006	40006	0.26	5.00	19
1-4	(28+29)-V-4	0.04	0.15	0.05	0.04	10007	40007	0.19	5.00	26
1-4	(28+29)-V-4	0.04	0.15	0.05	0.03	10008	40008	0.19	5.00	26
1-4	(28+29)-I-4	0.04	0.22	0.05	0.02	10009	40009	0.26	5.00	19
1-4	(28+29)-V-3	0.03	0.23	0.05	0.03	10010	40010	0.25	5.00	20
1-4	(28+29)-V-3	0.04	0.15	0.05	0.00	10011	40011	0.19	5.00	26
1-4	(28+29)-IV-3	0.03	0.03	0.03	0.22	10014	40014	0.25	5.00	20
1-4	(28+29)-IV-4	0.04	0.05	0.05	0.20	10017	40017	0.25	5.00	20

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
1-4	(28+29)-II-3	0.04	0.04	0.04	0.19	10018	40018	0.24	5.00	21
1-4	(28+29)-II-4	0.03	0.00	0.04	0.20	10021	40021	0.24	5.00	21
1-4	(28+29)-IV-4	0.03	0.07	0.03	0.23	10024	40024	0.26	5.00	20
1-4	(28+29)-IV-4	0.04	0.04	0.04	0.21	10027	40027	0.26	5.00	20
1-4	(28+29)-II-3	0.04	0.04	0.04	0.21	10028	40028	0.25	5.00	20
1-4	(28+29)-II-4	0.03	0.01	0.04	0.21	10031	40031	0.25	5.00	20
1-4	(28+29)-IV-4	0.03	0.05	0.03	0.14	10034	40034	0.17	5.00	29
1-4	(28+29)-III-4	0.02	0.21	0.04	0.04	10035	40035	0.23	5.00	21
1-4	(28+29)-II-4	0.04	0.21	0.04	0.02	10036	40036	0.25	5.00	20
1-4	(28+29)-IV-4	0.04	0.05	0.04	0.13	10037	40037	0.17	5.00	29
1-4	(28+29)-II-3	0.04	0.05	0.04	0.13	10038	40038	0.17	5.00	29
1-4	(28+29)-III-4	0.04	0.20	0.04	0.01	10039	40039	0.25	5.00	20
1-4	(28+29)-I-3	0.03	0.20	0.04	0.03	10040	40040	0.23	5.00	22
1-4	(28+29)-II-4	0.03	0.03	0.04	0.13	10041	40041	0.17	5.00	29
1-4	(28+29)-IV-4	0.03	0.03	0.03	0.14	10044	40044	0.16	5.00	31
1-4	(28+29)-VII-3	0.02	0.18	0.04	0.05	10045	40045	0.21	5.00	24
1-4	(28+29)-VII-3	0.04	0.19	0.04	0.04	10046	40046	0.22	5.00	22
1-4	(28+29)-IV-4	0.04	0.02	0.04	0.13	10047	40047	0.17	5.00	30
1-4	(28+29)-VI-3	0.04	0.04	0.04	0.13	10048	40048	0.16	5.00	30
1-4	(28+29)-VII-3	0.04	0.18	0.04	0.03	10049	40049	0.22	5.00	23
1-4	(28+29)-V-3	0.03	0.18	0.04	0.02	10050	40050	0.21	5.00	24
1-4	(28+29)-II-4	0.03	0.03	0.03	0.13	10051	40051	0.16	5.00	31
1-4	(28+29)-IV-4	0.03	0.00	0.02	0.22	10054	40054	0.24	5.00	21
1-4	(28+29)-IV-4	0.04	0.02	0.04	0.21	10057	40057	0.24	5.00	20
1-4	(28+29)-II-3	0.04	0.02	0.04	0.20	10058	40058	0.24	5.00	21
1-4	(28+29)-VI-4	0.03	0.04	0.03	0.21	10061	40061	0.24	5.00	21
1-4	(28+29)-IV-4	0.03	0.02	0.02	0.22	10064	40064	0.24	5.00	21
1-4	(28+29)-IV-4	0.04	0.02	0.03	0.21	10067	40067	0.24	5.00	21
1-4	(28+29)-II-3	0.04	0.02	0.03	0.20	10068	40068	0.23	5.00	22
1-4	(28+29)-VI-3	0.03	0.04	0.03	0.21	10071	40071	0.24	5.00	21
1-4	(28+29)-V-4	0.03	0.16	0.03	0.03	10074	40074	0.19	5.00	26
1-4	(28+29)-V-4	0.02	0.26	0.04	0.00	10075	40075	0.28	5.00	18
1-4	(28+29)-V-4	0.03	0.26	0.04	0.03	10076	40076	0.29	5.00	17
1-4	(28+29)-V-4	0.04	0.16	0.04	0.04	10077	40077	0.19	5.00	26
1-4	(28+29)-V-4	0.04	0.15	0.04	0.03	10078	40078	0.19	5.00	26
1-4	(28+29)-V-4	0.04	0.25	0.04	0.04	10079	40079	0.29	5.00	17
1-4	(28+29)-V-3	0.03	0.25	0.04	0.03	10080	40080	0.28	5.00	18
1-4	(28+29)-V-3	0.03	0.16	0.04	0.07	10081	40081	0.19	5.00	27
2-3	(28+29)-I-4	0.01	0.16	0.00	0.03	11498	30713	0.17	1.50	8.9
2-7	(28+29)-I-4	0.00	0.27	0.02	0.12	11499	70779	0.27	5.10	19
2-7	(28+29)-III-4	0.00	0.70	0.03	0.12	11500	70834	0.70	5.95	8.5
2-3	(28+29)-I-4	0.00	0.16	0.00	0.01	11501	30710	0.16	1.50	9.2
2-7	(28+29)-VI-3	0.00	0.01	0.02	0.32	11502	70776	0.34	5.10	15
2-7	(28+29)-III-4	0.00	0.70	0.02	0.06	11503	70832	0.70	5.95	8.6
2-3	(28+29)-I-4	0.00	0.17	0.00	0.03	11504	30707	0.17	1.50	8.7
2-7	(28+29)-IV-4	0.00	0.01	0.02	0.34	11505	70773	0.36	5.10	14
2-7	(28+29)-III-4	0.00	0.70	0.02	0.15	11506	70830	0.70	5.95	8.5
2-3	(28+29)-I-4	0.01	0.16	0.00	0.00	11507	30704	0.17	1.50	8.6
2-7	(28+29)-III-3	0.00	0.27	0.03	0.12	11508	70770	0.27	5.10	19
2-7	(28+29)-III-3	0.00	0.70	0.03	0.13	11509	70828	0.70	5.95	8.5
2-7	(28+29)-III-3	0.01	0.84	0.03	0.00	11510	70860	0.85	6.55	7.7
2-7	(28+29)-II-4	0.00	0.40	0.02	1.02	11511	70861	1.04	6.55	6.3
2-7	(28+29)-III-3	0.01	0.82	0.06	0.19	11512	70862	0.83	6.55	7.9
2-7	(28+29)-III-3	0.01	0.80	0.09	0.22	11513	70863	0.82	6.55	8.0
2-7	(28+29)-III-3	0.00	0.84	0.02	0.19	11514	70859	0.85	6.55	7.7
2-7	(28+29)-III-3	0.00	0.84	0.03	0.11	11515	70858	0.84	6.55	7.8
2-7	(28+29)-III-3	0.00	0.83	0.02	0.24	11516	70857	0.83	6.55	7.9
2-7	(28+29)-IV-3	0.00	0.43	0.03	1.20	11517	70856	1.23	6.55	5.3
2-7	(28+29)-III-3	0.00	0.79	0.07	0.45	11518	70855	0.80	6.55	8.2
2-7	(28+29)-III-3	0.01	0.78	0.08	0.39	11519	70854	0.79	6.55	8.3
2-7	(28+29)-I-4	0.00	0.27	0.03	0.11	11520	70782	0.28	5.10	18
2-7	(28+29)-VI-3	0.02	0.01	0.08	0.29	11521	70844	0.37	5.10	14
2-3	(28+29)-I-3	0.01	0.14	0.01	0.04	11522	30798	0.15	1.50	9.9
2-3	(28+29)-I-4	0.01	0.15	0.01	0.07	11523	30765	0.16	1.50	9.6
2-7	(28+29)-II-4	0.01	0.07	0.06	0.49	11524	70821	0.55	5.10	9.3
2-3	(28+29)-I-4	0.00	0.16	0.01	0.08	11525	30746	0.17	1.50	9.0
2-7	(28+29)-II-3	0.00	0.26	0.02	0.57	11526	70802	0.59	5.10	8.7
2-3	(28+29)-I-4	0.01	0.16	0.00	0.05	11527	30722	0.16	1.50	9.1
2-7	(28+29)-III-3	0.00	0.28	0.03	0.11	11528	70790	0.28	5.10	18
2-3	(28+29)-I-4	0.01	0.15	0.01	0.04	11529	30805	0.16	1.50	9.4
2-7	(28+29)-IV-3	0.01	0.08	0.05	0.47	11530	70825	0.52	5.10	9.8
2-3	(28+29)-I-4	0.01	0.15	0.00	0.02	11531	30731	0.16	1.50	9.5
2-3	(28+29)-III-4	0.01	0.16	0.01	0.02	11532	30786	0.17	1.50	9.0
2-7	(28+29)-VIII-3	0.01	0.01	0.07	0.35	11533	70847	0.43	5.10	12
2-3	(28+29)-I-4	0.00	0.15	0.01	0.01	11534	30754	0.15	1.50	9.8
2-7	(28+29)-IV-3	0.01	0.06	0.02	0.41	11535	70809	0.43	5.10	12
2-7	(28+29)-VIII-4	0.01	0.40	0.07	0.62	11536	70895	0.69	5.10	7.4
2-9	(28+29)-VIII-4	0.01	0.50	0.05	0.67	11537	90853	0.71	5.00	7.0
2-7	(28+29)-V-3	0.01	0.58	0.08	0.59	11538	70894	0.67	5.10	7.6

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
2-9	(28+29)-V-3	0.02	0.62	0.06	0.72	11539	90852	0.77	5.00	6.5
2-7	(28+29)-VI-3	0.02	0.02	0.08	0.27	11540	70850	0.35	5.10	15
2-3	(28+29)-VI-3	0.01	0.05	0.00	0.08	11541	30816	0.09	1.50	17
2-7	(28+29)-VII-3	0.01	0.00	0.07	0.34	11542	70851	0.41	5.10	12
2-3	(28+29)-VIII-4	0.01	0.05	0.00	0.09	11543	30817	0.09	1.50	16
3-10	(28+29)-VI-4	0.00	0.03	0.01	0.08	21498	100644	0.09	4.90	55
3-10	(28+29)-VI-3	0.00	0.00	0.01	0.10	21499	100641	0.11	4.90	44
3-10	(28+29)-IV-4	0.00	0.01	0.01	0.11	21500	100638	0.11	4.90	43
3-10	(28+29)-VIII-3	0.00	0.03	0.01	0.08	21501	100635	0.09	4.90	54
3-10	(28+29)-VI-3	0.00	0.00	0.01	0.11	21502	100738	0.13	4.90	39
3-10	(28+29)-VI-4	0.00	0.02	0.01	0.15	21503	100718	0.16	4.90	30
3-10	(28+29)-II-3	0.00	0.08	0.01	0.17	21504	100687	0.18	4.90	27
3-10	(28+29)-VI-3	0.00	0.00	0.01	0.09	21505	100653	0.09	4.90	53
3-10	(28+29)-VIII-3	0.00	0.01	0.01	0.13	21506	100750	0.15	4.90	34
3-10	(28+29)-VIII-3	0.00	0.03	0.00	0.08	21507	100662	0.09	4.90	57
3-10	(28+29)-VIII-4	0.00	0.07	0.01	0.15	21508	100726	0.16	4.90	30
3-10	(28+29)-VIII-3	0.00	0.02	0.01	0.13	21509	100695	0.15	4.90	33
3-10	(28+29)-VIII-4	0.01	0.58	0.04	0.69	21510	100819	0.73	4.90	6.7
3-10	(28+29)-V-3	0.03	0.68	0.05	0.79	21511	100818	0.84	4.90	5.8
3-10	(28+29)-V-3	0.00	0.09	0.01	0.16	21512	100762	0.17	4.90	29
3-10	(28+29)-VIII-4	0.00	0.06	0.01	0.16	21513	100764	0.18	4.90	27
3-9	(28+29)-IV-3	0.01	0.05	0.01	0.10	30704	90704	0.12	3.50	29
3-9	(28+29)-IV-4	0.00	0.07	0.01	0.16	30707	90707	0.17	3.50	20
3-9	(28+29)-VI-3	0.01	0.00	0.02	0.15	30710	90710	0.17	3.50	21
3-9	(28+29)-II-4	0.01	0.02	0.01	0.11	30713	90713	0.12	3.50	29
3-9	(28+29)-VI-3	0.00	0.00	0.01	0.12	30722	90722	0.13	3.50	26
3-9	(28+29)-IV-4	0.01	0.08	0.02	0.10	30731	90731	0.12	3.50	29
3-9	(28+29)-II-3	0.01	0.17	0.03	0.28	30746	90746	0.31	3.50	11
3-9	(28+29)-IV-3	0.00	0.03	0.03	0.19	30754	90754	0.22	3.50	16
3-9	(28+29)-II-4	0.01	0.03	0.02	0.22	30765	90765	0.23	3.50	15
3-9	(28+29)-IV-3	0.01	0.05	0.02	0.21	30786	90786	0.23	3.50	15
3-9	(28+29)-VI-3	0.01	0.02	0.02	0.15	30798	90798	0.17	3.50	20
3-9	(28+29)-IV-4	0.01	0.04	0.02	0.18	30805	90805	0.20	3.50	18
3-9	(28+29)-I-4	0.01	0.11	0.03	0.14	30816	90816	0.16	3.50	22
3-9	(28+29)-VIII-4	0.01	0.06	0.02	0.18	30817	90817	0.21	3.50	17
4-6	(28+29)-I-4	0.01	0.26	0.00	0.02	31498	60563	0.26	1.55	5.9
4-6	(28+29)-I-4	0.00	0.26	0.00	0.02	31499	60560	0.26	1.55	6.0
4-6	(28+29)-I-4	0.00	0.26	0.00	0.01	31500	60557	0.26	1.55	6.0
4-6	(28+29)-I-4	0.01	0.26	0.00	0.02	31501	60554	0.26	1.55	5.9
4-6	(28+29)-I-4	0.01	0.24	0.00	0.10	31502	60683	0.25	1.55	6.1
4-6	(28+29)-V-4	0.00	0.24	0.00	0.10	31503	60649	0.25	1.55	6.3
4-6	(28+29)-I-4	0.01	0.25	0.00	0.09	31504	60608	0.25	1.55	6.2
4-6	(28+29)-I-4	0.00	0.24	0.00	0.09	31505	60576	0.24	1.55	6.4
4-6	(28+29)-I-4	0.01	0.24	0.00	0.06	31506	60617	0.25	1.55	6.3
4-6	(28+29)-V-4	0.00	0.24	0.00	0.08	31507	60658	0.24	1.55	6.4
4-6	(28+29)-I-4	0.01	0.24	0.00	0.10	31508	60691	0.25	1.55	6.2
4-6	(28+29)-I-4	0.00	0.24	0.00	0.09	31509	60585	0.24	1.55	6.5
4-11	(28+29)-VIII-4	0.01	0.65	0.04	0.76	31510	110793	0.80	4.80	6.0
4-11	(28+29)-V-3	0.03	0.78	0.06	0.89	31511	110769	0.95	4.80	5.0
4-6	(28+29)-V-3	0.01	0.08	0.00	0.10	31512	60734	0.10	1.55	15
4-6	(28+29)-VII-4	0.01	0.07	0.00	0.10	31513	60735	0.10	1.55	15
4-7	(28+29)-V-4	0.02	0.57	0.02	0.25	40004	70004	0.59	2.15	3.7
4-7	(28+29)-IV-3	0.02	0.06	0.03	0.96	40005	70005	0.99	2.15	2.2
4-7	(28+29)-V-4	0.04	0.55	0.04	0.06	40006	70006	0.59	2.15	3.6
4-7	(28+29)-V-4	0.04	0.54	0.03	0.01	40007	70007	0.57	2.15	3.8
4-7	(28+29)-V-4	0.04	0.54	0.04	0.00	40008	70008	0.58	2.15	3.7
4-7	(28+29)-V-3	0.04	0.58	0.03	0.03	40009	70009	0.62	2.15	3.5
4-7	(28+29)-VI-3	0.03	0.24	0.03	0.78	40010	70010	0.81	2.15	2.6
4-7	(28+29)-V-3	0.03	0.56	0.01	0.05	40011	70011	0.59	2.15	3.7
4-12	(28+29)-IV-4	0.02	0.05	0.04	0.20	40014	120014	0.24	5.00	21
4-12	(28+29)-IV-4	0.02	0.06	0.05	0.15	40015	120015	0.20	5.00	25
4-12	(28+29)-IV-3	0.04	0.04	0.05	0.18	40016	120016	0.23	5.00	21
4-12	(28+29)-IV-4	0.04	0.04	0.05	0.18	40017	120017	0.23	5.00	22
4-12	(28+29)-VI-4	0.04	0.01	0.05	0.18	40018	120018	0.23	5.00	22
4-12	(28+29)-II-3	0.04	0.05	0.05	0.17	40019	120019	0.22	5.00	22
4-12	(28+29)-II-4	0.03	0.03	0.05	0.15	40020	120020	0.20	5.00	25
4-12	(28+29)-VI-4	0.04	0.01	0.05	0.17	40021	120021	0.22	5.00	23
4-12	(28+29)-VIII-4	0.02	0.03	0.03	0.16	40024	120024	0.19	5.00	27
4-12	(28+29)-IV-4	0.02	0.05	0.04	0.16	40025	120025	0.20	5.00	25
4-12	(28+29)-III-4	0.04	0.16	0.04	0.03	40026	120026	0.20	5.00	25
4-12	(28+29)-IV-4	0.04	0.05	0.04	0.16	40027	120027	0.20	5.00	25
4-12	(28+29)-VI-4	0.04	0.03	0.04	0.16	40028	120028	0.20	5.00	25
4-12	(28+29)-III-4	0.04	0.17	0.04	0.02	40029	120029	0.21	5.00	24
4-12	(28+29)-III-4	0.03	0.16	0.04	0.05	40030	120030	0.19	5.00	26
4-12	(28+29)-VI-4	0.04	0.02	0.03	0.15	40031	120031	0.19	5.00	27
4-12	(28+29)-IV-4	0.02	0.05	0.03	0.15	40034	120034	0.18	5.00	29
4-12	(28+29)-I-3	0.02	0.17	0.04	0.00	40035	120035	0.19	5.00	27
4-12	(28+29)-I-4	0.04	0.15	0.04	0.02	40036	120036	0.20	5.00	25
4-12	(28+29)-IV-4	0.04	0.04	0.04	0.15	40037	120037	0.19	5.00	27

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
4-12	(28+29)-VI-4	0.04	0.03	0.04	0.15	40038	120038	0.19	5.00	27
4-12	(28+29)-III-4	0.04	0.16	0.04	0.02	40039	120039	0.20	5.00	25
4-12	(28+29)-III-4	0.03	0.15	0.04	0.05	40040	120040	0.19	5.00	27
4-12	(28+29)-I-3	0.04	0.14	0.03	0.00	40041	120041	0.18	5.00	27
4-12	(28+29)-IV-4	0.02	0.03	0.03	0.15	40044	120044	0.18	5.00	28
4-12	(28+29)-IV-4	0.02	0.04	0.04	0.14	40045	120045	0.18	5.00	28
4-12	(28+29)-V-4	0.04	0.14	0.04	0.04	40046	120046	0.18	5.00	28
4-12	(28+29)-IV-4	0.04	0.04	0.04	0.14	40047	120047	0.19	5.00	27
4-12	(28+29)-VI-4	0.04	0.04	0.04	0.15	40048	120048	0.19	5.00	27
4-12	(28+29)-VII-4	0.04	0.14	0.04	0.04	40049	120049	0.18	5.00	28
4-12	(28+29)-II-4	0.03	0.04	0.04	0.13	40050	120050	0.17	5.00	29
4-12	(28+29)-VI-4	0.04	0.04	0.04	0.14	40051	120051	0.18	5.00	27
4-12	(28+29)-IV-4	0.02	0.03	0.03	0.17	40054	120054	0.20	5.00	25
4-12	(28+29)-IV-4	0.02	0.03	0.04	0.16	40055	120055	0.20	5.00	25
4-12	(28+29)-VII-4	0.04	0.16	0.04	0.05	40056	120056	0.20	5.00	25
4-12	(28+29)-IV-4	0.04	0.04	0.04	0.16	40057	120057	0.21	5.00	24
4-12	(28+29)-VI-4	0.04	0.04	0.04	0.17	40058	120058	0.21	5.00	24
4-12	(28+29)-V-3	0.04	0.16	0.04	0.04	40059	120059	0.20	5.00	25
4-12	(28+29)-VII-3	0.03	0.16	0.04	0.02	40060	120060	0.19	5.00	26
4-12	(28+29)-VI-4	0.04	0.05	0.04	0.16	40061	120061	0.21	5.00	24
4-12	(28+29)-IV-4	0.02	0.02	0.02	0.16	40064	120064	0.18	5.00	27
4-12	(28+29)-V-4	0.02	0.17	0.03	0.01	40065	120065	0.19	5.00	26
4-12	(28+29)-V-4	0.04	0.16	0.03	0.04	40066	120066	0.20	5.00	24
4-12	(28+29)-VII-3	0.04	0.15	0.03	0.05	40067	120067	0.19	5.00	26
4-12	(28+29)-VI-4	0.04	0.04	0.03	0.16	40068	120068	0.19	5.00	26
4-12	(28+29)-V-3	0.04	0.17	0.03	0.04	40069	120069	0.20	5.00	24
4-12	(28+29)-VII-4	0.03	0.16	0.03	0.04	40070	120070	0.19	5.00	26
4-12	(28+29)-V-4	0.04	0.15	0.03	0.20	40071	120071	0.22	5.00	22
4-12	(28+29)-V-4	0.02	0.18	0.02	0.03	40074	120074	0.20	5.00	25
4-12	(28+29)-V-4	0.02	0.20	0.04	0.01	40075	120075	0.22	5.00	23
4-12	(28+29)-V-4	0.04	0.19	0.04	0.04	40076	120076	0.23	5.00	22
4-12	(28+29)-V-4	0.04	0.18	0.04	0.04	40077	120077	0.21	5.00	23
4-12	(28+29)-V-4	0.04	0.17	0.04	0.07	40078	120078	0.21	5.00	24
4-12	(28+29)-V-4	0.04	0.20	0.04	0.05	40079	120079	0.23	5.00	21
4-12	(28+29)-VI-4	0.03	0.26	0.04	0.13	40080	120080	0.29	5.00	17
4-12	(28+29)-VI-4	0.04	0.25	0.03	0.18	40081	120081	0.29	5.00	17
5-6	(28+29)-IV-4	0.01	0.01	0.01	0.04	50445	60445	0.05	0.70	15
5-6	(28+29)-VIII-3	0.00	0.01	0.01	0.04	50449	60449	0.05	0.70	15
5-6	(28+29)-VI-4	0.00	0.02	0.01	0.04	50453	60453	0.05	0.70	15
5-6	(28+29)-I-4	0.01	0.04	0.01	0.02	50457	60457	0.05	0.70	15
5-6	(28+29)-I-4	0.00	0.00	0.00	0.00	50466	60466	0.00	0.70	>100
5-6	(28+29)-I-4	0.00	0.00	0.00	0.00	50470	60470	0.00	0.70	>100
5-6	(28+29)-V-4	0.00	0.00	0.00	0.00	50486	60486	0.00	0.70	>100
5-6	(28+29)-VI-4	0.00	0.02	0.01	0.04	50490	60490	0.05	0.70	14
5-6	(28+29)-VIII-3	0.00	0.01	0.01	0.04	50499	60499	0.05	0.70	14
5-6	(28+29)-VII-3	0.00	0.00	0.00	0.00	50503	60503	0.00	0.70	>100
5-6	(28+29)-II-3	0.00	0.03	0.01	0.05	50527	60527	0.06	0.70	12
5-6	(28+29)-IV-3	0.00	0.00	0.01	0.04	50540	60540	0.05	0.70	15
5-6	(28+29)-VI-4	0.00	0.00	0.01	0.05	50570	60570	0.06	0.70	12
5-6	(28+29)-VIII-3	0.00	0.00	0.01	0.05	50580	60580	0.06	0.70	12
5-6	(28+29)-VI-4	0.01	0.02	0.01	0.05	50603	60603	0.06	0.70	12
5-6	(28+29)-VIII-3	0.01	0.00	0.01	0.05	50612	60612	0.06	0.70	12
5-6	(28+29)-I-4	0.00	0.03	0.00	0.02	50622	60622	0.03	0.70	21
5-6	(28+29)-VII-3	0.00	0.03	0.00	0.02	50626	60626	0.03	0.70	21
5-6	(28+29)-I-4	0.00	0.03	0.00	0.02	50668	60668	0.04	0.70	19
5-6	(28+29)-III-3	0.00	0.03	0.00	0.02	50672	60672	0.03	0.70	20
5-6	(28+29)-V-3	0.00	0.06	0.01	0.07	50676	60676	0.08	0.70	9.2
5-6	(28+29)-VIII-4	0.01	0.06	0.01	0.07	50682	60682	0.08	0.70	8.9
5-14	(28+29)-VIII-4	0.04	0.57	0.05	0.90	50717	140717	0.95	5.45	5.7
5-13	(28+29)-V-3	0.03	0.81	0.05	0.93	50736	130736	0.98	4.70	4.8
5-13	(28+29)-VIII-4	0.01	0.67	0.03	0.76	50737	130737	0.79	4.70	5.9
6-13	(28+29)-IV-3	0.00	0.01	0.01	0.02	60445	130445	0.04	4.00	>100
6-13	(28+29)-VIII-4	0.00	0.00	0.01	0.02	60449	130449	0.03	4.00	>100
6-13	(28+29)-VI-3	0.00	0.00	0.01	0.02	60453	130453	0.03	4.00	>100
6-13	(28+29)-VI-4	0.00	0.01	0.01	0.02	60457	130457	0.04	4.00	>100
6-13	(28+29)-II-3	0.00	0.01	0.02	0.06	60466	130466	0.07	4.00	55
6-13	(28+29)-IV-4	0.00	0.01	0.02	0.06	60470	130470	0.08	4.00	48
6-13	(28+29)-VI-4	0.00	0.02	0.02	0.06	60486	130486	0.08	4.00	53
6-13	(28+29)-VI-4	0.00	0.01	0.01	0.02	60490	130490	0.03	4.00	>100
6-13	(28+29)-VIII-3	0.00	0.01	0.01	0.02	60499	130499	0.03	4.00	>100
6-13	(28+29)-VII-3	0.00	0.02	0.01	0.06	60503	130503	0.07	4.00	54
6-13	(28+29)-II-3	0.00	0.01	0.01	0.03	60527	130527	0.04	4.00	>100
6-13	(28+29)-VIII-3	0.00	0.00	0.01	0.02	60540	130540	0.03	4.00	>100
6-11	(28+29)-VIII-3	0.00	0.02	0.01	0.07	60554	110554	0.08	3.25	41
6-11	(28+29)-IV-4	0.00	0.01	0.01	0.07	60557	110557	0.08	3.25	41
6-11	(28+29)-VI-3	0.00	0.01	0.01	0.07	60560	110560	0.08	3.25	41
6-11	(28+29)-VI-4	0.00	0.03	0.01	0.07	60563	110563	0.08	3.25	40
6-13	(28+29)-VI-4	0.00	0.00	0.01	0.03	60570	130570	0.04	4.00	>100
6-11	(28+29)-VIII-4	0.00	0.01	0.01	0.10	60576	110576	0.12	3.25	28

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
6-13	(28+29)-IV-3	0.01	0.00	0.01	0.03	60580	130580	0.04	4.00	>100
6-11	(28+29)-VI-3	0.00	0.00	0.01	0.10	60585	110585	0.11	3.25	29
6-13	(28+29)-VI-4	0.01	0.02	0.01	0.03	60603	130603	0.04	4.00	98
6-11	(28+29)-II-4	0.01	0.04	0.01	0.09	60608	110608	0.11	3.25	30
6-13	(28+29)-VIII-3	0.01	0.00	0.01	0.03	60612	130612	0.04	4.00	99
6-11	(28+29)-VIII-3	0.01	0.03	0.01	0.08	60617	110617	0.09	3.25	35
6-13	(28+29)-VI-4	0.01	0.01	0.01	0.06	60622	130622	0.08	4.00	52
6-13	(28+29)-VIII-3	0.01	0.02	0.02	0.06	60626	130626	0.08	4.00	51
6-11	(28+29)-VI-4	0.00	0.03	0.01	0.09	60649	110649	0.10	3.25	32
6-11	(28+29)-VIII-3	0.00	0.04	0.01	0.09	60658	110658	0.10	3.25	32
6-13	(28+29)-VI-3	0.01	0.05	0.02	0.11	60668	130668	0.13	4.00	31
6-13	(28+29)-VIII-4	0.01	0.06	0.03	0.14	60672	130672	0.16	4.00	25
6-13	(28+29)-VI-3	0.00	0.01	0.01	0.07	60676	130676	0.08	4.00	51
6-13	(28+29)-VIII-4	0.00	0.01	0.02	0.07	60682	130682	0.09	4.00	44
6-11	(28+29)-VIII-4	0.01	0.01	0.01	0.10	60683	110683	0.12	3.25	28
6-11	(28+29)-VI-3	0.01	0.00	0.02	0.11	60691	110691	0.12	3.25	26
6-11	(28+29)-V-4	0.00	0.19	0.02	0.22	60734	110734	0.24	3.25	13
6-11	(28+29)-VII-3	0.00	0.16	0.02	0.25	60735	110735	0.27	3.25	12
7-8	(28+29)-I-4	0.01	0.14	0.00	0.01	61498	80360	0.15	1.50	9.8
7-8	(28+29)-I-4	0.00	0.14	0.00	0.01	61499	80357	0.15	1.50	10
7-8	(28+29)-I-4	0.00	0.14	0.00	0.01	61500	80354	0.15	1.50	10
7-8	(28+29)-I-4	0.01	0.14	0.00	0.00	61501	80351	0.15	1.50	9.8
7-8	(28+29)-I-4	0.01	0.13	0.00	0.06	61502	80522	0.14	1.50	10
7-8	(28+29)-V-4	0.01	0.13	0.00	0.06	61503	80481	0.14	1.50	11
7-8	(28+29)-I-4	0.00	0.13	0.00	0.05	61504	80424	0.13	1.50	11
7-8	(28+29)-I-4	0.01	0.14	0.00	0.05	61505	80392	0.14	1.50	11
7-8	(28+29)-I-4	0.00	0.14	0.00	0.05	61506	80437	0.14	1.50	11
7-8	(28+29)-V-4	0.01	0.14	0.00	0.05	61507	80495	0.14	1.50	10
7-8	(28+29)-I-4	0.01	0.13	0.00	0.06	61508	80536	0.14	1.50	10
7-8	(28+29)-I-4	0.00	0.14	0.00	0.05	61509	80401	0.14	1.50	11
7-8	(28+29)-I-4	0.00	0.14	0.00	0.03	61510	80378	0.14	1.50	11
7-8	(28+29)-I-4	0.00	0.14	0.00	0.02	61511	80363	0.14	1.50	11
7-8	(28+29)-I-4	0.00	0.14	0.00	0.01	61512	80367	0.14	1.50	11
7-8	(28+29)-I-4	0.01	0.14	0.00	0.03	61513	80389	0.14	1.50	10
7-8	(28+29)-V-4	0.00	0.13	0.00	0.08	61514	80546	0.13	1.50	11
7-8	(28+29)-V-4	0.01	0.14	0.00	0.04	61515	80597	0.14	1.50	11
7-8	(28+29)-VII-4	0.00	0.15	0.01	0.10	61516	80600	0.16	1.50	9.5
7-8	(28+29)-VII-3	0.00	0.13	0.01	0.08	61517	80550	0.14	1.50	11
7-14	(28+29)-V-3	0.03	0.88	0.06	1.00	61518	140681	1.06	4.60	4.3
7-8	(28+29)-V-3	0.01	0.08	0.00	0.08	61519	80621	0.09	1.50	17
7-14	(28+29)-VIII-4	0.02	0.56	0.06	0.91	61520	140665	0.97	4.60	4.7
7-12	(28+29)-V-4	0.00	0.49	0.10	0.11	70003	120003	0.50	2.85	5.7
7-12	(28+29)-V-4	0.00	0.49	0.07	0.22	70004	120004	0.49	2.85	5.8
7-12	(28+29)-IV-3	0.01	0.04	0.03	0.86	70005	120005	0.89	2.85	3.2
7-12	(28+29)-V-4	0.00	0.47	0.02	0.09	70006	120006	0.47	2.85	6.1
7-12	(28+29)-V-4	0.00	0.47	0.03	0.04	70007	120007	0.47	2.85	6.1
7-12	(28+29)-V-4	0.00	0.47	0.03	0.03	70008	120008	0.47	2.85	6.1
7-12	(28+29)-V-3	0.00	0.49	0.03	0.07	70009	120009	0.50	2.85	5.8
7-12	(28+29)-VI-3	0.00	0.32	0.03	0.67	70010	120010	0.70	2.85	4.1
7-12	(28+29)-V-3	0.01	0.52	0.07	0.05	70011	120011	0.53	2.85	5.4
7-12	(28+29)-VI-3	0.01	0.33	0.14	1.64	70012	120012	1.78	2.85	1.6
7-8	(28+29)-III-3	0.01	0.03	0.00	0.01	70262	80262	0.04	0.65	18
7-8	(28+29)-VIII-3	0.00	0.01	0.01	0.03	70266	80266	0.04	0.65	15
7-8	(28+29)-II-3	0.00	0.01	0.01	0.03	70270	80270	0.04	0.65	16
7-8	(28+29)-III-3	0.01	0.03	0.00	0.01	70274	80274	0.04	0.65	18
7-8	(28+29)-III-3	0.00	0.03	0.00	0.01	70279	80279	0.03	0.65	19
7-8	(28+29)-III-3	0.00	0.03	0.00	0.01	70283	80283	0.03	0.65	20
7-8	(28+29)-III-3	0.00	0.03	0.00	0.00	70290	80290	0.04	0.65	19
7-8	(28+29)-I-4	0.00	0.03	0.00	0.01	70294	80294	0.03	0.65	19
7-8	(28+29)-III-3	0.00	0.03	0.01	0.00	70303	80303	0.03	0.65	19
7-8	(28+29)-I-4	0.00	0.03	0.01	0.01	70312	80312	0.03	0.65	19
7-8	(28+29)-II-4	0.00	0.00	0.01	0.04	70333	80333	0.04	0.65	15
7-8	(28+29)-IV-3	0.00	0.02	0.01	0.03	70346	80346	0.04	0.65	16
7-8	(28+29)-II-4	0.00	0.00	0.01	0.04	70384	80384	0.05	0.65	13
7-8	(28+29)-IV-3	0.00	0.02	0.01	0.04	70396	80396	0.05	0.65	14
7-8	(28+29)-VI-4	0.01	0.02	0.00	0.04	70418	80418	0.04	0.65	16
7-8	(28+29)-III-4	0.01	0.03	0.00	0.00	70429	80429	0.04	0.65	17
7-8	(28+29)-VI-4	0.00	0.02	0.01	0.04	70461	80461	0.05	0.65	14
7-8	(28+29)-VIII-3	0.00	0.00	0.01	0.04	70474	80474	0.04	0.65	16
7-8	(28+29)-VI-3	0.01	0.02	0.00	0.05	70518	80518	0.05	0.65	12
7-8	(28+29)-VIII-4	0.01	0.05	0.01	0.08	70532	80532	0.09	0.65	7.2
7-8	(28+29)-V-3	0.00	0.06	0.00	0.07	70553	80553	0.07	0.65	9.5
7-16	(28+29)-VIII-4	0.01	0.56	0.05	0.89	70592	160592	0.94	4.50	4.8
7-16	(28+29)-V-3	0.04	0.92	0.06	1.05	70630	160630	1.11	4.50	4.0
7-9	(28+29)-IV-3	0.00	0.00	0.01	0.04	70770	90770	0.05	0.75	15
7-9	(28+29)-VIII-3	0.00	0.00	0.00	0.09	70773	90773	0.09	0.75	7.9
7-9	(28+29)-VI-3	0.00	0.00	0.00	0.09	70776	90776	0.09	0.75	8.3
7-9	(28+29)-II-4	0.00	0.00	0.01	0.06	70779	90779	0.06	0.75	12
7-9	(28+29)-VI-3	0.00	0.00	0.01	0.04	70782	90782	0.05	0.75	14

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
7-9	(28+29)-VIII-4	0.00	0.00	0.01	0.03	70790	90790	0.05	0.75	17
7-9	(28+29)-I-3	0.01	0.02	0.02	0.29	70802	90802	0.31	0.75	2.4
7-9	(28+29)-IV-3	0.01	0.03	0.02	0.09	70809	90809	0.11	0.75	6.5
7-9	(28+29)-VI-4	0.01	0.04	0.04	0.12	70821	90821	0.15	0.75	4.9
7-9	(28+29)-IV-3	0.01	0.03	0.02	0.10	70825	90825	0.13	0.75	5.8
7-9	(28+29)-V-3	0.02	0.01	0.05	0.15	70844	90844	0.20	0.75	3.8
7-9	(28+29)-VIII-3	0.01	0.01	0.04	0.07	70847	90847	0.11	0.75	6.9
7-9	(28+29)-II-3	0.01	0.01	0.05	0.05	70850	90850	0.10	0.75	7.7
7-9	(28+29)-III-3	0.01	0.02	0.04	0.15	70851	90851	0.20	0.75	3.8
7-9	(28+29)-V-3	0.02	0.08	0.03	0.08	70894	90894	0.11	0.75	7.0
7-9	(28+29)-VIII-4	0.01	0.08	0.03	0.06	70895	90895	0.09	0.75	8.1
8-17	(28+29)-VII-4	0.03	0.26	0.05	0.20	71498	170510	0.29	4.90	17
8-16	(28+29)-III-3	0.00	0.02	0.01	0.01	80262	160262	0.03	3.85	>100
8-16	(28+29)-IV-4	0.00	0.00	0.01	0.02	80266	160266	0.03	3.85	>100
8-16	(28+29)-II-3	0.00	0.00	0.01	0.03	80270	160270	0.04	3.85	>100
8-16	(28+29)-III-3	0.00	0.02	0.01	0.01	80274	160274	0.03	3.85	>100
8-16	(28+29)-II-3	0.00	0.01	0.01	0.02	80279	160279	0.02	3.85	>100
8-16	(28+29)-IV-3	0.00	0.01	0.01	0.02	80283	160283	0.02	3.85	>100
8-16	(28+29)-VI-4	0.00	0.01	0.01	0.02	80290	160290	0.02	3.85	>100
8-16	(28+29)-VIII-3	0.00	0.01	0.00	0.02	80294	160294	0.02	3.85	>100
8-16	(28+29)-III-3	0.00	0.02	0.01	0.00	80303	160303	0.03	3.85	>100
8-16	(28+29)-IV-4	0.00	0.00	0.01	0.02	80312	160312	0.03	3.85	>100
8-16	(28+29)-II-4	0.00	0.00	0.01	0.03	80333	160333	0.04	3.85	>100
8-16	(28+29)-IV-3	0.00	0.01	0.01	0.02	80346	160346	0.03	3.85	>100
8-14	(28+29)-IV-4	0.01	0.01	0.01	0.04	80351	140351	0.05	3.10	58
8-14	(28+29)-IV-4	0.00	0.01	0.01	0.05	80354	140354	0.06	3.10	49
8-14	(28+29)-II-3	0.00	0.01	0.01	0.05	80357	140357	0.06	3.10	50
8-14	(28+29)-II-3	0.01	0.01	0.01	0.04	80360	140360	0.05	3.10	63
8-14	(28+29)-VI-4	0.00	0.01	0.01	0.04	80363	140363	0.05	3.10	65
8-14	(28+29)-VIII-3	0.00	0.01	0.01	0.04	80367	140367	0.05	3.10	60
8-14	(28+29)-VI-4	0.00	0.01	0.01	0.04	80378	140378	0.05	3.10	67
8-16	(28+29)-II-4	0.00	0.00	0.01	0.03	80384	160384	0.04	3.85	>100
8-14	(28+29)-VI-3	0.00	0.01	0.01	0.05	80389	140389	0.06	3.10	54
8-14	(28+29)-VI-4	0.01	0.01	0.01	0.04	80392	140392	0.05	3.10	61
8-16	(28+29)-IV-3	0.00	0.01	0.01	0.03	80396	160396	0.03	3.85	>100
8-14	(28+29)-VI-3	0.01	0.00	0.01	0.06	80401	140401	0.07	3.10	43
8-16	(28+29)-VI-4	0.00	0.01	0.00	0.03	80418	160418	0.03	3.85	>100
8-14	(28+29)-II-4	0.00	0.02	0.01	0.05	80424	140424	0.06	3.10	48
8-16	(28+29)-VIII-3	0.00	0.00	0.00	0.03	80429	160429	0.03	3.85	>100
8-14	(28+29)-II-3	0.00	0.01	0.01	0.06	80437	140437	0.08	3.10	41
8-16	(28+29)-VI-4	0.00	0.01	0.00	0.03	80461	160461	0.03	3.85	>100
8-16	(28+29)-VIII-3	0.00	0.00	0.00	0.02	80474	160474	0.03	3.85	>100
8-14	(28+29)-II-4	0.00	0.02	0.01	0.06	80481	140481	0.07	3.10	42
8-14	(28+29)-II-3	0.00	0.01	0.01	0.07	80495	140495	0.08	3.10	41
8-16	(28+29)-II-4	0.00	0.00	0.00	0.04	80518	160518	0.04	3.85	98
8-14	(28+29)-VI-4	0.01	0.01	0.01	0.05	80522	140522	0.06	3.10	52
8-16	(28+29)-VIII-4	0.00	0.04	0.01	0.06	80532	160532	0.07	3.85	56
8-14	(28+29)-VI-3	0.01	0.01	0.01	0.06	80536	140536	0.06	3.10	48
8-14	(28+29)-II-4	0.00	0.01	0.01	0.05	80546	140546	0.06	3.10	49
8-14	(28+29)-VIII-3	0.01	0.01	0.02	0.05	80550	140550	0.07	3.10	45
8-16	(28+29)-II-4	0.00	0.01	0.01	0.08	80553	160553	0.10	3.85	40
8-14	(28+29)-VI-3	0.00	0.07	0.01	0.06	80597	140597	0.07	3.10	42
8-14	(28+29)-VIII-4	0.00	0.04	0.02	0.09	80600	140600	0.11	3.10	27
8-14	(28+29)-I-4	0.01	0.09	0.02	0.10	80621	140621	0.12	3.10	25
9-10	(28+29)-IV-3	0.01	0.00	0.01	0.07	90704	100704	0.08	0.75	9.3
9-10	(28+29)-IV-4	0.00	0.01	0.01	0.12	90707	100707	0.12	0.75	6.1
9-10	(28+29)-II-3	0.00	0.00	0.01	0.11	90710	100710	0.12	0.75	6.3
9-10	(28+29)-II-4	0.00	0.01	0.01	0.08	90713	100713	0.09	0.75	8.8
9-10	(28+29)-VI-3	0.01	0.00	0.01	0.09	90722	100722	0.10	0.75	7.8
9-10	(28+29)-IV-4	0.00	0.01	0.01	0.08	90731	100731	0.09	0.75	8.7
9-10	(28+29)-II-3	0.01	0.06	0.02	0.22	90746	100746	0.23	0.75	3.2
9-10	(28+29)-IV-3	0.00	0.03	0.02	0.14	90754	100754	0.16	0.75	4.7
9-10	(28+29)-II-4	0.00	0.04	0.01	0.16	90765	100765	0.17	0.75	4.4
9-10	(28+29)-IV-3	0.00	0.04	0.01	0.16	90786	100786	0.17	0.75	4.5
9-10	(28+29)-VI-3	0.00	0.01	0.01	0.13	90798	100798	0.14	0.75	5.3
9-10	(28+29)-IV-4	0.00	0.03	0.01	0.14	90805	100805	0.16	0.75	4.8
9-10	(28+29)-VI-3	0.01	0.00	0.02	0.01	90816	100816	0.03	0.75	23
9-10	(28+29)-VIII-4	0.00	0.03	0.01	0.16	90817	100817	0.17	0.75	4.3
9-10	(28+29)-V-3	0.01	0.07	0.01	0.06	90852	100852	0.09	0.75	8.5
9-10	(28+29)-VIII-4	0.01	0.07	0.02	0.03	90853	100853	0.08	0.75	9.4
10-11	(28+29)-III-3	0.01	0.14	0.01	0.02	91498	110201	0.15	1.40	9.5
10-11	(28+29)-III-3	0.00	0.14	0.01	0.02	91499	110198	0.14	1.40	9.9
10-11	(28+29)-III-3	0.00	0.14	0.01	0.02	91500	110195	0.14	1.40	9.8
10-11	(28+29)-III-3	0.01	0.14	0.01	0.02	91501	110192	0.15	1.40	9.5
10-11	(28+29)-III-3	0.01	0.12	0.01	0.05	91502	110328	0.12	1.40	11
10-11	(28+29)-III-3	0.00	0.12	0.00	0.03	91503	110299	0.12	1.40	11
10-11	(28+29)-III-3	0.00	0.12	0.00	0.02	91504	110251	0.13	1.40	11
10-11	(28+29)-III-3	0.00	0.13	0.00	0.02	91505	110228	0.13	1.40	11
10-11	(28+29)-III-3	0.00	0.14	0.00	0.06	91506	110258	0.14	1.40	10

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
10-11	(28+29)-III-3	0.00	0.14	0.00	0.06	91507	110308	0.14	1.40	9.7
10-11	(28+29)-III-3	0.00	0.14	0.01	0.07	91508	110339	0.14	1.40	9.8
10-11	(28+29)-III-3	0.00	0.14	0.00	0.06	91509	110234	0.14	1.40	9.8
10-11	(28+29)-III-3	0.00	0.13	0.00	0.01	91510	110217	0.14	1.40	10
10-11	(28+29)-III-3	0.00	0.13	0.01	0.00	91511	110211	0.13	1.40	10
10-11	(28+29)-III-3	0.00	0.14	0.01	0.04	91512	110214	0.14	1.40	9.8
10-11	(28+29)-III-3	0.00	0.14	0.00	0.04	91513	110221	0.14	1.40	9.7
10-11	(28+29)-III-3	0.01	0.11	0.01	0.06	91514	110370	0.12	1.40	12
10-11	(28+29)-V-3	0.00	0.13	0.01	0.05	91515	110433	0.13	1.40	11
10-11	(28+29)-I-4	0.01	0.07	0.01	0.02	91516	110325	0.08	0.85	10
10-11	(28+29)-II-4	0.00	0.01	0.01	0.08	91517	110382	0.09	0.85	9.3
10-11	(28+29)-VII-4	0.01	0.06	0.01	0.05	91518	110373	0.07	1.40	20
10-17	(28+29)-V-3	0.04	0.97	0.07	1.13	91519	170566	1.20	4.40	3.7
10-17	(28+29)-VI-3	0.01	0.16	0.02	0.27	91520	170480	0.30	4.40	15
10-17	(28+29)-VII-4	0.02	0.21	0.04	0.33	91521	170414	0.38	4.40	12
10-17	(28+29)-VIII-4	0.02	0.53	0.06	0.85	91522	170507	0.91	4.40	4.8
10-11	(28+29)-IV-4	0.00	0.00	0.00	0.03	100635	110635	0.03	0.75	25
10-11	(28+29)-I-4	0.00	0.02	0.00	0.00	100638	110638	0.02	0.75	32
10-11	(28+29)-I-4	0.00	0.02	0.00	0.00	100641	110641	0.02	0.75	32
10-11	(28+29)-I-4	0.00	0.02	0.00	0.00	100644	110644	0.03	0.75	29
10-11	(28+29)-I-4	0.00	0.02	0.00	0.05	100653	110653	0.05	0.75	16
10-11	(28+29)-VIII-3	0.00	0.01	0.00	0.03	100662	110662	0.03	0.75	24
10-11	(28+29)-V-4	0.00	0.02	0.00	0.00	100687	110687	0.02	0.75	33
10-11	(28+29)-VII-3	0.00	0.02	0.00	0.01	100695	110695	0.02	0.75	33
10-11	(28+29)-VII-4	0.00	0.02	0.00	0.01	100718	110718	0.02	0.75	34
10-11	(28+29)-VII-3	0.00	0.02	0.00	0.00	100726	110726	0.02	0.75	35
10-11	(28+29)-V-4	0.01	0.02	0.01	0.07	100738	110738	0.08	0.75	10.0
10-11	(28+29)-VII-4	0.01	0.02	0.01	0.00	100750	110750	0.03	0.75	29
10-11	(28+29)-V-3	0.01	0.01	0.00	0.00	100762	110762	0.02	0.75	35
10-11	(28+29)-VIII-4	0.01	0.03	0.01	0.04	100764	110764	0.04	0.75	18
10-11	(28+29)-V-3	0.02	0.07	0.01	0.06	100818	110818	0.09	0.75	8.4
10-11	(28+29)-III-3	0.01	0.00	0.02	0.34	100819	110819	0.35	0.75	2.1
11-18	(28+29)-VIII-3	0.00	0.00	0.01	0.07	101498	180145	0.08	4.30	57
11-18	(28+29)-VIII-3	0.00	0.00	0.01	0.09	101499	180146	0.10	4.30	43
11-18	(28+29)-II-3	0.00	0.01	0.01	0.09	101500	180147	0.10	4.30	43
11-18	(28+29)-II-3	0.00	0.01	0.01	0.07	101501	180150	0.07	4.30	59
11-18	(28+29)-I-4	0.01	0.84	0.00	0.32	101502	180186	0.86	3.95	4.6
11-18	(28+29)-VI-3	0.00	0.04	0.01	0.10	101503	180224	0.11	4.30	40
11-18	(28+29)-I-4	0.00	0.08	0.00	0.01	101504	180248	0.08	4.30	55
11-18	(28+29)-VI-3	0.00	0.04	0.01	0.11	101505	180189	0.11	4.30	37
11-18	(28+29)-II-4	0.00	0.00	0.01	0.09	101506	180173	0.10	4.30	44
11-18	(28+29)-IV-3	0.00	0.04	0.01	0.09	101507	180232	0.10	4.30	43
11-18	(28+29)-VIII-3	0.00	0.00	0.01	0.09	101508	180176	0.10	4.30	44
11-18	(28+29)-VIII-3	0.00	0.05	0.00	0.09	101509	180256	0.09	4.30	49
11-18	(28+29)-VIII-4	0.00	0.00	0.00	0.10	101510	180204	0.11	4.30	40
11-18	(28+29)-II-4	0.00	0.02	0.00	0.07	101511	180154	0.07	4.30	59
11-18	(28+29)-II-3	0.00	0.01	0.00	0.07	101512	180165	0.07	4.30	63
11-18	(28+29)-VIII-3	0.00	0.00	0.00	0.07	101513	180168	0.07	4.30	60
11-18	(28+29)-VIII-3	0.00	0.00	0.00	0.07	101514	180162	0.07	4.30	59
11-18	(28+29)-I-4	0.02	0.71	0.01	0.45	101515	180243	0.73	4.05	5.5
11-18	(28+29)-I-4	0.02	0.69	0.00	0.45	101516	180316	0.71	4.15	5.9
11-18	(28+29)-VIII-4	0.06	0.54	0.08	0.83	101517	180404	0.90	4.30	4.8
11-18	(28+29)-VII-4	0.01	0.14	0.01	0.08	101518	180322	0.15	4.30	28
11-18	(28+29)-V-3	0.01	1.25	0.00	1.06	101519	180465	1.26	4.30	3.4
11-18	(28+29)-I-4	0.01	0.59	0.03	0.60	101520	180376	0.64	4.20	6.6
11-18	(28+29)-VIII-4	0.06	0.53	0.08	0.82	101521	180338	0.89	4.25	4.8
11-18	(28+29)-VIII-4	0.04	0.26	0.07	0.66	101522	180287	0.72	4.20	5.8
11-18	(28+29)-III-3	0.02	0.51	0.03	0.30	101523	180231	0.53	4.15	7.9
11-18	(28+29)-III-3	0.01	0.62	0.04	0.22	101524	180208	0.63	4.10	6.5
11-18	(28+29)-IV-3	0.04	0.59	0.01	0.22	101525	180174	0.63	4.05	6.5
11-18	(28+29)-III-3	0.03	0.84	0.00	0.54	101526	180185	0.87	4.05	4.7
11-19	(28+29)-III-3	0.01	1.46	0.13	0.07	110097	190097	1.47	4.50	3.1
11-19	(28+29)-III-3	0.01	1.45	0.15	0.06	110098	190098	1.46	4.50	3.1
11-19	(28+29)-III-3	0.01	1.45	0.15	0.07	110099	190099	1.46	4.50	3.1
11-19	(28+29)-III-3	0.01	1.46	0.13	0.07	110101	190101	1.47	4.50	3.1
11-19	(28+29)-III-3	0.01	1.40	0.13	0.20	110107	190107	1.41	4.50	3.2
11-19	(28+29)-III-3	0.01	1.38	0.13	0.29	110109	190109	1.39	4.50	3.2
11-19	(28+29)-III-3	0.01	1.40	0.11	0.19	110113	190113	1.41	4.50	3.2
11-19	(28+29)-III-3	0.01	1.37	0.11	0.29	110115	190115	1.38	4.50	3.3
11-19	(28+29)-III-3	0.01	1.32	0.11	0.44	110123	190123	1.33	4.50	3.4
11-19	(28+29)-III-3	0.00	1.30	0.10	0.57	110124	190124	1.30	4.50	3.5
11-19	(28+29)-III-3	0.02	1.32	0.11	0.40	110137	190137	1.33	4.50	3.4
11-19	(28+29)-III-3	0.00	1.30	0.10	0.55	110139	190139	1.30	4.50	3.5
11-18	(28+29)-III-4	0.01	1.05	0.01	0.39	110158	180158	1.06	3.75	3.5
11-18	(28+29)-III-3	0.04	1.02	0.00	0.42	110164	180164	1.05	3.75	3.6
11-17	(28+29)-III-3	0.00	0.05	0.00	0.02	110192	170192	0.05	3.00	60
11-17	(28+29)-IV-3	0.00	0.02	0.00	0.07	110195	170195	0.07	3.00	42
11-17	(28+29)-II-3	0.00	0.01	0.00	0.07	110198	170198	0.07	3.00	42
11-17	(28+29)-II-3	0.00	0.01	0.00	0.04	110201	170201	0.05	3.00	62

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
11-17	(28+29)-II-3	0.00	0.01	0.00	0.05	110211	170211	0.05	3.00	62
11-17	(28+29)-III-3	0.00	0.04	0.00	0.02	110214	170214	0.05	3.00	67
11-17	(28+29)-III-3	0.00	0.04	0.00	0.00	110217	170217	0.04	3.00	70
11-17	(28+29)-III-3	0.00	0.04	0.00	0.02	110221	170221	0.05	3.00	65
11-17	(28+29)-III-3	0.01	0.04	0.00	0.00	110228	170228	0.05	3.00	60
11-17	(28+29)-I-4	0.01	0.04	0.00	0.02	110234	170234	0.05	3.00	65
11-17	(28+29)-II-4	0.00	0.01	0.00	0.06	110251	170251	0.06	3.00	51
11-17	(28+29)-IV-3	0.00	0.02	0.00	0.05	110258	170258	0.06	3.00	53
11-17	(28+29)-II-4	0.00	0.03	0.00	0.06	110299	170299	0.07	3.00	46
11-17	(28+29)-IV-3	0.00	0.01	0.00	0.06	110308	170308	0.06	3.00	50
11-18	(28+29)-II-3	0.00	0.00	0.01	0.04	110325	180325	0.05	3.75	78
11-17	(28+29)-VI-4	0.00	0.02	0.02	0.05	110328	170328	0.07	3.00	43
11-17	(28+29)-VI-3	0.01	0.01	0.02	0.06	110339	170339	0.08	3.00	39
11-17	(28+29)-II-3	0.02	0.00	0.03	0.05	110370	170370	0.08	3.00	39
11-17	(28+29)-III-3	0.02	0.14	0.01	0.08	110373	170373	0.16	3.00	19
11-18	(28+29)-V-3	0.00	0.05	0.00	0.03	110382	180382	0.05	3.75	76
11-17	(28+29)-II-4	0.02	0.00	0.03	0.06	110433	170433	0.09	3.00	35
11-13	(28+29)-IV-4	0.00	0.01	0.00	0.05	110554	130554	0.06	0.75	13
11-13	(28+29)-IV-4	0.00	0.00	0.00	0.05	110557	130557	0.05	0.75	14
11-13	(28+29)-VI-3	0.00	0.00	0.00	0.05	110560	130560	0.05	0.75	14
11-13	(28+29)-II-4	0.00	0.01	0.00	0.05	110563	130563	0.05	0.75	15
11-13	(28+29)-VIII-4	0.00	0.00	0.00	0.09	110576	130576	0.09	0.75	8.0
11-13	(28+29)-VI-3	0.00	0.00	0.00	0.09	110585	130585	0.09	0.75	8.3
11-13	(28+29)-VI-3	0.00	0.01	0.00	0.07	110608	130608	0.07	0.75	10
11-13	(28+29)-VIII-3	0.00	0.01	0.00	0.05	110617	130617	0.06	0.75	13
11-13	(28+29)-VI-4	0.00	0.02	0.00	0.07	110649	130649	0.07	0.75	11
11-13	(28+29)-VIII-3	0.00	0.02	0.00	0.06	110658	130658	0.07	0.75	11
11-13	(28+29)-VIII-4	0.00	0.00	0.00	0.10	110683	130683	0.11	0.75	7.1
11-13	(28+29)-VI-3	0.00	0.00	0.01	0.10	110691	130691	0.11	0.75	6.8
11-13	(28+29)-VIII-3	0.00	0.00	0.02	0.15	110734	130734	0.17	0.75	4.3
11-13	(28+29)-VIII-3	0.01	0.01	0.01	0.04	110735	130735	0.05	0.75	14
11-13	(28+29)-V-3	0.02	0.07	0.02	0.05	110769	130769	0.09	0.75	8.5
11-13	(28+29)-IV-4	0.01	0.04	0.02	0.02	110793	130793	0.05	0.75	15
12-15	(28+29)-VII-4	0.02	0.01	0.00	0.00	120003	150003	0.03	1.55	55
12-15	(28+29)-VIII-4	0.02	0.00	0.01	0.03	120004	150004	0.04	1.55	40
12-15	(28+29)-IV-4	0.01	0.00	0.01	0.02	120005	150005	0.04	1.55	41
12-15	(28+29)-IV-3	0.00	0.00	0.01	0.03	120006	150006	0.05	1.55	32
12-15	(28+29)-IV-4	0.00	0.00	0.01	0.04	120007	150007	0.05	1.55	32
12-15	(28+29)-V-4	0.00	0.00	0.01	0.04	120008	150008	0.06	1.55	27
12-15	(28+29)-II-3	0.00	0.00	0.01	0.04	120009	150009	0.05	1.55	31
12-15	(28+29)-II-4	0.00	0.00	0.01	0.02	120010	150010	0.04	1.55	40
12-15	(28+29)-II-4	0.01	0.00	0.01	0.03	120011	150011	0.04	1.55	37
12-15	(28+29)-VI-3	0.01	0.00	0.01	0.03	120012	150012	0.03	1.55	47
12-15	(28+29)-III-4	0.03	0.01	0.00	0.00	120013	150013	0.04	1.55	43
12-15	(28+29)-III-4	0.02	0.02	0.00	0.00	120014	150014	0.04	1.55	39
12-15	(28+29)-III-3	0.01	0.00	0.00	0.00	120015	150015	0.01	1.55	>100
12-15	(28+29)-III-3	0.01	0.01	0.00	0.00	120016	150016	0.01	1.55	>100
12-15	(28+29)-I-3	0.00	0.02	0.00	0.00	120017	150017	0.02	1.55	77
12-15	(28+29)-III-4	0.00	0.01	0.00	0.00	120018	150018	0.02	1.55	89
12-15	(28+29)-II-4	0.00	0.00	0.00	0.01	120019	150019	0.01	1.55	>100
12-15	(28+29)-II-4	0.00	0.00	0.00	0.01	120020	150020	0.01	1.55	>100
12-15	(28+29)-III-4	0.01	0.02	0.00	0.00	120021	150021	0.02	1.55	65
12-15	(28+29)-IV-4	0.02	0.00	0.00	0.00	120022	150022	0.02	1.55	86
12-15	(28+29)-III-4	0.03	0.01	0.00	0.00	120023	150023	0.04	1.55	43
12-15	(28+29)-III-4	0.02	0.02	0.00	0.00	120024	150024	0.04	1.55	37
12-15	(28+29)-IV-4	0.01	0.00	0.00	0.01	120025	150025	0.01	1.55	>100
12-15	(28+29)-I-3	0.01	0.01	0.00	0.00	120026	150026	0.01	1.55	>100
12-15	(28+29)-III-4	0.00	0.02	0.00	0.00	120027	150027	0.02	1.55	71
12-15	(28+29)-III-4	0.00	0.02	0.00	0.00	120028	150028	0.02	1.55	81
12-15	(28+29)-VI-3	0.00	0.00	0.00	0.01	120029	150029	0.01	1.55	>100
12-15	(28+29)-II-4	0.00	0.00	0.00	0.01	120030	150030	0.01	1.55	>100
12-15	(28+29)-III-4	0.01	0.02	0.00	0.00	120031	150031	0.03	1.55	60
12-15	(28+29)-II-3	0.02	0.00	0.00	0.00	120032	150032	0.02	1.55	85
12-15	(28+29)-I-3	0.02	0.01	0.00	0.00	120033	150033	0.04	1.55	42
12-15	(28+29)-I-3	0.02	0.02	0.00	0.00	120034	150034	0.04	1.55	38
12-15	(28+29)-VIII-3	0.01	0.00	0.00	0.02	120035	150035	0.02	1.55	70
12-15	(28+29)-IV-3	0.01	0.00	0.00	0.02	120036	150036	0.02	1.55	80
12-15	(28+29)-III-4	0.00	0.02	0.00	0.01	120037	150037	0.02	1.55	73
12-15	(28+29)-VI-4	0.00	0.00	0.00	0.02	120038	150038	0.02	1.55	75
12-15	(28+29)-II-3	0.00	0.00	0.00	0.02	120039	150039	0.02	1.55	79
12-15	(28+29)-VI-4	0.00	0.00	0.00	0.02	120040	150040	0.02	1.55	75
12-15	(28+29)-III-4	0.01	0.02	0.00	0.01	120041	150041	0.03	1.55	61
12-15	(28+29)-I-4	0.02	0.00	0.00	0.00	120042	150042	0.02	1.55	83
12-15	(28+29)-VII-4	0.03	0.01	0.00	0.00	120043	150043	0.04	1.55	44
12-15	(28+29)-V-4	0.02	0.02	0.00	0.01	120044	150044	0.04	1.55	40
12-15	(28+29)-VIII-3	0.01	0.00	0.00	0.02	120045	150045	0.02	1.55	81
12-15	(28+29)-IV-3	0.01	0.00	0.00	0.01	120046	150046	0.02	1.55	88
12-15	(28+29)-V-3	0.00	0.02	0.00	0.00	120047	150047	0.02	1.55	79
12-15	(28+29)-VI-4	0.00	0.00	0.00	0.02	120048	150048	0.02	1.55	85

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
12-15	(28+29)-II-3	0.00	0.00	0.00	0.01	120049	150049	0.02	1.55	88
12-15	(28+29)-VI-4	0.00	0.00	0.00	0.01	120050	150050	0.02	1.55	86
12-15	(28+29)-V-3	0.01	0.02	0.00	0.00	120051	150051	0.02	1.55	67
12-15	(28+29)-I-4	0.02	0.00	0.00	0.00	120052	150052	0.02	1.55	86
12-15	(28+29)-VII-3	0.02	0.01	0.00	0.00	120053	150053	0.04	1.55	41
12-15	(28+29)-VII-3	0.02	0.02	0.00	0.00	120054	150054	0.04	1.55	37
12-15	(28+29)-VII-4	0.01	0.00	0.00	0.00	120055	150055	0.01	1.55	>100
12-15	(28+29)-VII-4	0.00	0.01	0.00	0.00	120056	150056	0.01	1.55	>100
12-15	(28+29)-V-4	0.00	0.02	0.00	0.00	120057	150057	0.02	1.55	73
12-15	(28+29)-VII-3	0.00	0.01	0.00	0.00	120058	150058	0.02	1.55	82
12-15	(28+29)-VII-3	0.00	0.00	0.00	0.00	120059	150059	0.01	1.55	>100
12-15	(28+29)-VII-3	0.00	0.01	0.00	0.00	120060	150060	0.01	1.55	>100
12-15	(28+29)-V-4	0.01	0.02	0.00	0.00	120061	150061	0.03	1.55	61
12-15	(28+29)-V-4	0.02	0.00	0.00	0.00	120062	150062	0.02	1.55	85
12-15	(28+29)-V-3	0.02	0.01	0.00	0.15	120063	150063	0.15	1.55	10
12-15	(28+29)-VII-4	0.02	0.02	0.00	0.00	120064	150064	0.04	1.55	37
12-15	(28+29)-VII-3	0.01	0.00	0.00	0.00	120065	150065	0.01	1.55	>100
12-15	(28+29)-VII-3	0.00	0.01	0.00	0.00	120066	150066	0.01	1.55	>100
12-15	(28+29)-V-4	0.00	0.02	0.00	0.00	120067	150067	0.02	1.55	70
12-15	(28+29)-VII-4	0.00	0.02	0.00	0.00	120068	150068	0.02	1.55	80
12-15	(28+29)-VI-4	0.00	0.00	0.00	0.01	120069	150069	0.01	1.55	>100
12-15	(28+29)-VII-4	0.00	0.01	0.00	0.00	120070	150070	0.01	1.55	>100
12-15	(28+29)-V-4	0.01	0.02	0.00	0.00	120071	150071	0.03	1.55	60
12-15	(28+29)-VI-4	0.02	0.00	0.00	0.00	120072	150072	0.02	1.55	85
12-15	(28+29)-V-4	0.02	0.01	0.00	0.00	120073	150073	0.03	1.55	46
12-15	(28+29)-V-4	0.02	0.02	0.01	0.00	120074	150074	0.04	1.55	38
12-15	(28+29)-IV-4	0.01	0.00	0.01	0.02	120075	150075	0.03	1.55	61
12-15	(28+29)-VII-4	0.00	0.00	0.01	0.02	120076	150076	0.02	1.55	63
12-15	(28+29)-VIII-4	0.00	0.01	0.01	0.02	120077	150077	0.03	1.55	59
12-15	(28+29)-VI-3	0.00	0.00	0.01	0.02	120078	150078	0.03	1.55	60
12-15	(28+29)-VI-4	0.00	0.00	0.01	0.02	120079	150079	0.03	1.55	61
12-15	(28+29)-II-4	0.00	0.00	0.01	0.02	120080	150080	0.02	1.55	63
12-15	(28+29)-V-4	0.01	0.02	0.01	0.01	120081	150081	0.03	1.55	62
12-15	(28+29)-IV-4	0.02	0.00	0.00	0.00	120082	150082	0.02	1.55	81
12-15	(28+29)-V-3	0.01	0.01	0.01	0.00	120083	150083	0.02	1.55	89
12-15	(28+29)-V-3	0.01	0.00	0.01	0.00	120084	150084	0.02	1.55	>100
12-15	(28+29)-VII-4	0.00	0.00	0.02	0.00	120085	150085	0.02	1.55	80
12-15	(28+29)-VII-4	0.00	0.00	0.02	0.00	120086	150086	0.02	1.55	76
12-15	(28+29)-IV-3	0.00	0.00	0.02	0.00	120087	150087	0.02	1.55	78
12-15	(28+29)-VII-3	0.00	0.00	0.02	0.00	120088	150088	0.02	1.55	73
12-15	(28+29)-V-4	0.00	0.00	0.02	0.00	120089	150089	0.02	1.55	74
12-15	(28+29)-V-3	0.00	0.00	0.02	0.00	120090	150090	0.02	1.55	79
12-15	(28+29)-VII-3	0.00	0.01	0.02	0.00	120091	150091	0.02	1.55	78
12-15	(28+29)-V-3	0.01	0.01	0.01	0.00	120092	150092	0.01	1.55	>100
13-14	(28+29)-III-4	0.00	0.01	0.01	0.02	130445	140445	0.03	0.75	26
13-14	(28+29)-IV-4	0.00	0.00	0.00	0.03	130449	140449	0.04	0.75	20
13-14	(28+29)-II-4	0.00	0.00	0.00	0.04	130453	140453	0.04	0.75	19
13-14	(28+29)-I-3	0.00	0.01	0.01	0.03	130457	140457	0.03	0.75	24
13-14	(28+29)-II-4	0.00	0.00	0.01	0.02	130466	140466	0.02	0.75	35
13-14	(28+29)-IV-3	0.00	0.00	0.01	0.01	130470	140470	0.03	0.75	27
13-14	(28+29)-I-3	0.00	0.01	0.01	0.03	130486	140486	0.04	0.75	21
13-14	(28+29)-VI-4	0.00	0.00	0.01	0.01	130490	140490	0.02	0.75	40
13-14	(28+29)-VIII-3	0.00	0.00	0.01	0.01	130499	140499	0.02	0.75	39
13-14	(28+29)-IV-4	0.00	0.00	0.01	0.01	130503	140503	0.02	0.75	47
13-14	(28+29)-III-4	0.00	0.01	0.00	0.05	130527	140527	0.05	0.75	15
13-14	(28+29)-II-3	0.00	0.00	0.00	0.02	130540	140540	0.02	0.75	30
13-14	(28+29)-VI-4	0.00	0.01	0.00	0.04	130570	140570	0.04	0.75	19
13-14	(28+29)-VIII-3	0.00	0.00	0.00	0.03	130580	140580	0.03	0.75	26
13-14	(28+29)-II-4	0.01	0.01	0.00	0.02	130603	140603	0.02	0.75	32
13-14	(28+29)-IV-4	0.01	0.01	0.00	0.02	130612	140612	0.02	0.75	33
13-14	(28+29)-II-3	0.00	0.04	0.01	0.02	130622	140622	0.04	0.75	18
13-14	(28+29)-VIII-3	0.00	0.00	0.01	0.02	130626	140626	0.03	0.75	22
13-14	(28+29)-VI-4	0.00	0.01	0.02	0.01	130668	140668	0.03	0.75	26
13-14	(28+29)-VIII-4	0.00	0.04	0.02	0.04	130672	140672	0.06	0.75	12
13-14	(28+29)-I-4	0.01	0.00	0.01	0.07	130676	140676	0.08	0.75	9.5
13-14	(28+29)-III-3	0.02	0.00	0.01	0.09	130682	140682	0.10	0.75	7.9
13-14	(28+29)-V-3	0.01	0.06	0.01	0.05	130736	140736	0.08	0.75	9.5
13-14	(28+29)-IV-4	0.04	0.03	0.02	0.03	130737	140737	0.07	0.75	11
14-16	(28+29)-IV-4	0.00	0.00	0.01	0.03	140351	160351	0.04	0.75	21
14-16	(28+29)-IV-4	0.00	0.00	0.00	0.04	140354	160354	0.04	0.75	20
14-16	(28+29)-II-3	0.00	0.00	0.00	0.03	140357	160357	0.04	0.75	20
14-16	(28+29)-II-3	0.00	0.00	0.01	0.03	140360	160360	0.03	0.75	24
14-16	(28+29)-VI-4	0.00	0.01	0.01	0.03	140363	160363	0.03	0.75	24
14-16	(28+29)-VIII-3	0.00	0.01	0.01	0.03	140367	160367	0.03	0.75	22
14-16	(28+29)-II-3	0.00	0.01	0.01	0.02	140378	160378	0.03	0.75	26
14-16	(28+29)-VI-3	0.00	0.00	0.01	0.04	140389	160389	0.05	0.75	15
14-16	(28+29)-VI-4	0.00	0.00	0.01	0.02	140392	160392	0.03	0.75	24
14-16	(28+29)-VI-3	0.00	0.00	0.01	0.05	140401	160401	0.06	0.75	13
14-16	(28+29)-IV-4	0.00	0.00	0.00	0.03	140424	160424	0.04	0.75	20

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
14-16	(28+29)-II-3	0.00	0.00	0.00	0.03	140437	160437	0.03	0.75	25
14-16	(28+29)-II-4	0.00	0.01	0.00	0.04	140481	160481	0.05	0.75	16
14-16	(28+29)-II-3	0.00	0.00	0.00	0.06	140495	160495	0.06	0.75	12
14-16	(28+29)-II-3	0.00	0.00	0.01	0.03	140522	160522	0.04	0.75	19
14-16	(28+29)-VI-3	0.00	0.01	0.01	0.05	140536	160536	0.06	0.75	12
14-16	(28+29)-II-4	0.00	0.00	0.01	0.03	140546	160546	0.04	0.75	18
14-16	(28+29)-VIII-3	0.00	0.00	0.01	0.04	140550	160550	0.04	0.75	17
14-16	(28+29)-VI-3	0.00	0.01	0.01	0.04	140597	160597	0.05	0.75	16
14-16	(28+29)-VIII-4	0.00	0.02	0.01	0.05	140600	160600	0.06	0.75	13
14-16	(28+29)-VI-3	0.00	0.00	0.01	0.02	140621	160621	0.03	0.75	24
14-16	(28+29)-III-3	0.01	0.27	0.02	0.45	140665	160665	0.47	0.75	1.6
14-16	(28+29)-V-3	0.01	0.06	0.01	0.05	140681	160681	0.07	0.75	11
16-17	(28+29)-VIII-3	0.00	0.01	0.00	0.04	160262	170262	0.04	0.75	20
16-17	(28+29)-IV-3	0.00	0.01	0.00	0.06	160266	170266	0.07	0.75	12
16-17	(28+29)-II-3	0.00	0.00	0.00	0.06	160270	170270	0.06	0.75	12
16-17	(28+29)-II-3	0.00	0.00	0.00	0.04	160274	170274	0.04	0.75	19
16-17	(28+29)-VI-4	0.00	0.00	0.00	0.04	160279	170279	0.04	0.75	21
16-17	(28+29)-VIII-3	0.00	0.01	0.00	0.04	160283	170283	0.04	0.75	21
16-17	(28+29)-II-4	0.00	0.01	0.00	0.03	160290	170290	0.03	0.75	22
16-17	(28+29)-VIII-3	0.00	0.01	0.00	0.03	160294	170294	0.03	0.75	22
16-17	(28+29)-II-4	0.00	0.01	0.00	0.04	160303	170303	0.04	0.75	19
16-17	(28+29)-IV-3	0.00	0.01	0.00	0.04	160312	170312	0.05	0.75	16
16-17	(28+29)-VI-3	0.00	0.02	0.00	0.06	160333	170333	0.06	0.75	12
16-17	(28+29)-VIII-4	0.00	0.04	0.00	0.05	160346	170346	0.06	0.75	13
16-17	(28+29)-VI-4	0.00	0.01	0.00	0.06	160384	170384	0.06	0.75	12
16-17	(28+29)-VIII-3	0.00	0.02	0.00	0.05	160396	170396	0.06	0.75	13
16-17	(28+29)-VI-3	0.00	0.00	0.01	0.05	160418	170418	0.06	0.75	12
16-17	(28+29)-VIII-3	0.00	0.01	0.01	0.04	160429	170429	0.05	0.75	15
16-17	(28+29)-I-3	0.01	0.01	0.02	0.06	160461	170461	0.07	0.75	10
16-17	(28+29)-VIII-3	0.00	0.01	0.00	0.04	160474	170474	0.04	0.75	18
16-17	(28+29)-VI-3	0.00	0.04	0.02	0.05	160518	170518	0.06	0.75	12
16-17	(28+29)-VIII-4	0.04	0.06	0.05	0.08	160532	170532	0.13	0.75	5.8
16-17	(28+29)-II-3	0.01	0.06	0.00	0.12	160553	170553	0.12	0.75	6.2
16-17	(28+29)-I-3	0.04	0.02	0.00	0.02	160592	170592	0.05	0.75	14
16-17	(28+29)-V-3	0.02	0.05	0.00	0.05	160630	170630	0.08	0.75	9.7
17-18	(28+29)-IV-4	0.00	0.00	0.01	0.02	170192	180192	0.03	0.75	26
17-18	(28+29)-IV-3	0.00	0.01	0.01	0.04	170195	180195	0.05	0.75	16
17-18	(28+29)-II-3	0.00	0.00	0.01	0.04	170198	180198	0.05	0.75	15
17-18	(28+29)-VI-4	0.00	0.01	0.01	0.03	170201	180201	0.03	0.75	24
17-18	(28+29)-II-3	0.00	0.00	0.00	0.02	170211	180211	0.03	0.75	26
17-18	(28+29)-VI-3	0.00	0.00	0.00	0.02	170214	180214	0.03	0.75	29
17-18	(28+29)-III-3	0.00	0.02	0.00	0.00	170217	180217	0.02	0.75	33
17-18	(28+29)-III-3	0.00	0.02	0.00	0.00	170221	180221	0.02	0.75	34
17-18	(28+29)-III-3	0.00	0.02	0.00	0.00	170228	180228	0.02	0.75	37
17-18	(28+29)-III-3	0.00	0.02	0.00	0.01	170234	180234	0.02	0.75	37
17-18	(28+29)-IV-4	0.00	0.00	0.00	0.03	170251	180251	0.03	0.75	25
17-18	(28+29)-II-3	0.00	0.00	0.00	0.02	170258	180258	0.03	0.75	28
17-18	(28+29)-II-4	0.00	0.00	0.00	0.04	170299	180299	0.04	0.75	20
17-18	(28+29)-IV-3	0.01	0.01	0.00	0.03	170308	180308	0.03	0.75	22
17-18	(28+29)-VI-4	0.01	0.01	0.01	0.03	170328	180328	0.04	0.75	17
17-18	(28+29)-VIII-4	0.01	0.00	0.01	0.02	170339	180339	0.04	0.75	20
17-18	(28+29)-II-3	0.02	0.00	0.04	0.02	170370	180370	0.05	0.75	14
17-18	(28+29)-VIII-3	0.01	0.01	0.01	0.06	170373	180373	0.08	0.75	9.6
17-18	(28+29)-VIII-4	0.00	0.06	0.00	0.08	170414	180414	0.08	0.75	9.2
17-18	(28+29)-VI-3	0.02	0.00	0.03	0.02	170433	180433	0.05	0.75	16
17-18	(28+29)-VI-3	0.03	0.05	0.05	0.06	170480	180480	0.11	0.75	7.1
17-18	(28+29)-II-4	0.04	0.02	0.02	0.06	170507	180507	0.07	0.75	10
17-18	(28+29)-V-3	0.04	0.05	0.07	0.04	170566	180566	0.11	0.75	6.7
18-19	(28+29)-II-3	0.01	0.01	0.14	0.08	180145	190145	0.22	0.75	3.4
18-19	(28+29)-VIII-3	0.00	0.00	0.16	0.09	180146	190146	0.25	0.75	3.0
18-19	(28+29)-II-3	0.00	0.03	0.16	0.10	180147	190147	0.26	0.75	2.9
18-19	(28+29)-VI-4	0.01	0.01	0.14	0.08	180150	190150	0.22	0.75	3.3
18-19	(28+29)-VI-4	0.02	0.02	0.13	0.10	180154	190154	0.24	0.75	3.2
18-19	(28+29)-IV-3	0.05	0.51	0.04	0.26	180158	190158	0.57	0.75	1.3
18-19	(28+29)-VIII-4	0.02	0.02	0.14	0.11	180162	190162	0.24	0.75	3.1
18-19	(28+29)-III-3	0.06	0.24	0.03	0.13	180164	190164	0.30	0.75	2.5
18-19	(28+29)-II-4	0.02	0.02	0.11	0.13	180165	190165	0.23	0.75	3.2
18-19	(28+29)-VIII-4	0.02	0.03	0.10	0.13	180168	190168	0.24	0.75	3.2
18-19	(28+29)-II-3	0.02	0.04	0.09	0.17	180173	190173	0.26	0.75	2.9
18-19	(28+29)-VIII-3	0.02	0.03	0.08	0.15	180176	190176	0.23	0.75	3.2
18-19	(28+29)-II-4	0.02	0.03	0.09	0.16	180189	190189	0.25	0.75	3.0
18-19	(28+29)-VIII-4	0.02	0.10	0.09	0.17	180204	190204	0.25	0.75	2.9
18-19	(28+29)-V-4	0.00	0.02	0.03	0.08	180224	190224	0.11	0.75	6.7
18-19	(28+29)-IV-3	0.00	0.01	0.03	0.04	180232	190232	0.07	0.75	11
Minimo										
18-19	(28+29)-IV-3	0.05	0.51	0.04	0.26	180158	190158	0.57	0.75	1.3

Periodi di vibrazione e Masse modali

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Posizione masse 1

Numero di Frequenze calcolate =120, filtrate=72

N	T(s)	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(3)	0.1247	32.737	-0.002	10510	0	7.65	0.00
2(4)	0.1190	-7.679	16.612	578	2706	0.42	1.97
3(5)	0.1072	-16.476	-13.803	2662	1868	1.94	1.36
4(6)	0.0922	44.544	-2.060	19458	42	14.16	0.03
5(7)	0.0745	43.330	1.341	18412	18	13.40	0.01
6(8)	0.0743	1.663	-20.321	27	4050	0.02	2.95
7(9)	0.0728	-0.176	69.679	0	47612	0.00	34.65
8(10)	0.0724	0.652	-12.490	4	1530	0.00	1.11
9(11)	0.0722	6.148	26.164	371	6713	0.27	4.89
10(13)	0.0707	15.591	-11.665	2384	1334	1.73	0.97
11(14)	0.0698	-12.392	-3.248	1506	103	1.10	0.08
12(15)	0.0690	13.807	-6.231	1869	381	1.36	0.28
13(16)	0.0682	-5.273	-17.820	273	3114	0.20	2.27
14(19)	0.0663	13.031	-1.241	1665	15	1.21	0.01
15(20)	0.0656	-5.797	-0.542	330	3	0.24	0.00
16(21)	0.0651	-8.377	9.136	688	819	0.50	0.60
17(22)	0.0640	-6.388	-8.367	400	687	0.29	0.50
18(23)	0.0637	37.243	-3.377	13603	112	9.90	0.08
19(24)	0.0630	-28.142	-12.703	7766	1582	5.65	1.15
20(25)	0.0627	18.259	-2.556	3269	64	2.38	0.05
21(26)	0.0624	3.996	-11.617	157	1323	0.11	0.96
22(27)	0.0610	7.331	4.973	527	243	0.38	0.18
23(28)	0.0610	2.347	-7.535	54	557	0.04	0.41
24(29)	0.0604	9.299	0.601	848	4	0.62	0.00
25(31)	0.0593	8.019	-10.009	631	982	0.46	0.72
26(32)	0.0589	9.013	-12.331	797	1491	0.58	1.09
27(34)	0.0583	4.199	0.614	173	4	0.13	0.00
28(35)	0.0578	-7.155	-1.321	502	17	0.37	0.01
29(36)	0.0572	-10.243	-5.306	1029	276	0.75	0.20
30(37)	0.0568	-4.534	9.257	202	840	0.15	0.61
31(39)	0.0557	-6.476	-1.523	411	23	0.30	0.02
32(42)	0.0543	25.819	0.183	6537	0	4.76	0.00
33(43)	0.0542	-46.359	3.348	21076	110	15.34	0.08
34(44)	0.0541	-3.989	-4.209	156	174	0.11	0.13
35(46)	0.0533	-2.487	8.264	61	670	0.04	0.49
36(48)	0.0529	-3.055	-31.509	92	9736	0.07	7.09
37(49)	0.0523	-7.010	-2.537	482	63	0.35	0.05
38(50)	0.0520	2.854	5.486	80	295	0.06	0.21
39(52)	0.0517	0.293	-10.076	1	996	0.00	0.72
40(53)	0.0516	-3.733	6.300	137	389	0.10	0.28
41(54)	0.0514	-5.016	-16.141	247	2555	0.18	1.86
42(55)	0.0512	0.483	-6.017	2	355	0.00	0.26
43(56)	0.0507	0.947	-4.612	9	209	0.01	0.15
44(57)	0.0505	5.733	3.796	322	141	0.23	0.10
45(58)	0.0504	-4.351	3.531	186	122	0.14	0.09
46(60)	0.0499	0.524	4.610	3	208	0.00	0.15
47(61)	0.0494	-2.236	-6.655	49	434	0.04	0.32
48(63)	0.0489	-1.052	-7.183	11	506	0.01	0.37
49(65)	0.0484	0.078	17.243	0	2916	0.00	2.12
50(67)	0.0477	4.536	-2.026	202	40	0.15	0.03
51(68)	0.0476	-4.449	12.828	194	1614	0.14	1.17
52(70)	0.0471	3.171	4.941	99	239	0.07	0.17
53(71)	0.0471	3.824	5.987	143	351	0.10	0.26
54(72)	0.0467	4.460	-3.040	195	91	0.14	0.07
55(73)	0.0465	-3.214	-7.637	101	572	0.07	0.42
56(74)	0.0462	-3.447	-5.254	117	271	0.08	0.20
57(77)	0.0459	-5.055	-14.332	251	2014	0.18	1.47
58(79)	0.0457	1.122	9.080	12	809	0.01	0.59
59(81)	0.0449	-5.008	8.319	246	679	0.18	0.49
60(82)	0.0449	-5.140	7.303	259	523	0.19	0.38
61(84)	0.0445	3.031	6.371	90	398	0.07	0.29
62(88)	0.0438	0.043	-6.333	0	393	0.00	0.29
63(89)	0.0438	-8.131	9.508	648	887	0.47	0.65
64(90)	0.0435	2.236	-4.504	49	199	0.04	0.14
65(92)	0.0433	-2.471	5.643	60	312	0.04	0.23
66(97)	0.0428	-3.504	9.880	120	957	0.09	0.70
67(99)	0.0426	-0.870	9.903	7	962	0.01	0.70
68(101)	0.0423	-4.719	5.897	218	341	0.16	0.25

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
69(108)	0.0417	0.180	-7.486	0	550	0.00	0.40
70(110)	0.0413	4.422	-9.745	192	931	0.14	0.68
71(117)	0.0406	0.391	-5.851	2	336	0.00	0.24
72(119)	0.0405	-2.890	-13.767	82	1859	0.06	1.35
Somma delle Masse Modali [kgm*g]				123842	113720		
Masse strutturali libere [kgm*g]				137398	137398		
Percentuale				90.13	85.77	90.13	85.77

Posizione masse 2

Numero di Frequenze calcolate =120, filtrate=76

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
				kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(2)	0.1370	13.236	-16.168	1718	2563	1.25	1.87
2(3)	0.1242	15.744	18.350	2431	3302	1.77	2.40
3(4)	0.1201	-30.292	-3.552	8999	124	6.55	0.09
4(6)	0.0993	-35.089	13.530	12074	1795	8.79	1.31
5(7)	0.0942	-27.809	-14.563	7584	2080	5.52	1.51
6(8)	0.0787	10.015	-36.840	984	13310	0.72	9.69
7(9)	0.0750	0.154	27.565	0	7451	0.00	5.42
8(10)	0.0738	-7.816	-23.192	599	5275	0.44	3.84
9(11)	0.0718	2.139	37.926	45	14106	0.03	10.27
10(12)	0.0710	-51.923	2.176	26439	46	19.24	0.03
11(13)	0.0704	2.180	4.112	47	166	0.03	0.12
12(14)	0.0689	-1.284	-27.170	16	7239	0.01	5.27
13(15)	0.0685	-5.317	5.175	277	263	0.20	0.19
14(16)	0.0683	-4.016	11.160	158	1221	0.12	0.89
15(17)	0.0668	-12.024	-19.655	1418	3788	1.03	2.76
16(18)	0.0660	2.147	-22.245	45	4853	0.03	3.53
17(19)	0.0659	2.711	4.601	72	208	0.05	0.15
18(20)	0.0657	6.338	9.462	394	878	0.29	0.64
19(21)	0.0654	4.721	-7.712	219	583	0.16	0.42
20(22)	0.0646	-48.206	-8.043	22789	634	16.59	0.46
21(23)	0.0641	-8.674	4.546	738	203	0.54	0.15
22(24)	0.0638	-0.907	8.741	8	749	0.01	0.55
23(25)	0.0634	-5.481	7.914	295	614	0.21	0.45
24(28)	0.0611	-5.436	-3.251	290	104	0.21	0.08
25(29)	0.0596	-3.795	1.327	141	17	0.10	0.01
26(30)	0.0595	-4.835	12.329	229	1491	0.17	1.08
27(31)	0.0589	1.199	-4.790	14	225	0.01	0.16
28(32)	0.0584	0.103	4.775	0	224	0.00	0.16
29(34)	0.0577	-1.323	-3.798	17	141	0.01	0.10
30(35)	0.0575	-4.545	8.262	203	669	0.15	0.49
31(36)	0.0572	-2.286	-11.028	51	1193	0.04	0.87
32(37)	0.0567	4.775	4.045	224	160	0.16	0.12
33(38)	0.0563	-3.711	-11.558	135	1310	0.10	0.95
34(39)	0.0559	6.609	-6.730	428	444	0.31	0.32
35(42)	0.0547	-6.378	-25.774	399	6515	0.29	4.74
36(43)	0.0545	-29.967	-7.599	8807	566	6.41	0.41
37(44)	0.0544	-13.574	10.719	1807	1127	1.32	0.82
38(45)	0.0541	-25.387	1.217	6320	15	4.60	0.01
39(46)	0.0539	-6.458	8.197	409	659	0.30	0.48
40(48)	0.0532	-7.736	9.845	587	951	0.43	0.69
41(49)	0.0531	25.275	-13.784	6265	1863	4.56	1.36
42(50)	0.0527	-13.933	-1.128	1904	12	1.39	0.01
43(51)	0.0526	-9.697	1.812	922	32	0.67	0.02
44(52)	0.0519	19.306	-1.409	3655	19	2.66	0.01
45(54)	0.0513	-1.117	-5.424	12	289	0.01	0.21
46(56)	0.0509	-0.249	9.120	1	816	0.00	0.59
47(58)	0.0505	-5.025	11.771	248	1359	0.18	0.99
48(59)	0.0503	-1.299	-7.859	17	606	0.01	0.44
49(60)	0.0500	-0.865	-4.351	7	186	0.01	0.14
50(61)	0.0495	1.316	-21.735	17	4633	0.01	3.37
51(63)	0.0492	1.104	-4.165	12	170	0.01	0.12
52(64)	0.0489	-2.757	15.745	75	2431	0.05	1.77
53(65)	0.0488	-7.852	11.732	605	1350	0.44	0.98
54(68)	0.0479	-4.574	-3.222	205	102	0.15	0.07
55(69)	0.0478	-5.001	-4.171	245	171	0.18	0.12
56(70)	0.0476	-1.411	-15.317	20	2301	0.01	1.67
57(71)	0.0474	2.362	-6.661	55	435	0.04	0.32
58(74)	0.0469	2.115	4.092	44	164	0.03	0.12
59(76)	0.0467	0.136	-10.458	0	1073	0.00	0.78
60(78)	0.0458	0.114	10.134	0	1007	0.00	0.73
61(80)	0.0455	-4.797	6.837	226	458	0.16	0.33
62(81)	0.0453	5.140	5.325	259	278	0.19	0.20
63(82)	0.0450	-1.473	7.209	21	510	0.02	0.37
64(83)	0.0450	-1.337	3.859	18	146	0.01	0.11

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
65(84)	0.0449	-3.256	-3.993	104	156	0.08	0.11
66(85)	0.0449	2.413	-13.896	57	1894	0.04	1.38
67(87)	0.0445	0.934	-5.116	9	257	0.01	0.19
68(89)	0.0442	-9.209	-14.615	832	2095	0.61	1.52
69(90)	0.0442	-0.105	-9.842	0	950	0.00	0.69
70(94)	0.0437	-1.910	-3.908	36	150	0.03	0.11
71(95)	0.0435	3.925	-4.255	151	178	0.11	0.13
72(98)	0.0431	-2.150	-5.000	45	245	0.03	0.18
73(103)	0.0424	1.086	-4.403	12	190	0.01	0.14
74(111)	0.0414	3.940	-11.327	152	1258	0.11	0.92
75(114)	0.0411	1.587	-4.670	25	214	0.02	0.16
76(117)	0.0406	-1.070	8.022	11	631	0.01	0.46
Somma delle Masse Modali [kgm*g]				123672	115888		
Masse strutturali libere [kgm*g]				137398	137398		
Percentuale				90.01	85.35	90.01	85.35

Posizione masse 3

Numero di Frequenze calcolate =120, filtrate=75

N	T(s)	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.1492	-21.899	2.985	4703	87	3.42	0.06
2(2)	0.1176	-4.735	1.237	220	15	0.16	0.01
3(3)	0.1155	19.152	0.938	3597	9	2.62	0.01
4(4)	0.1143	-5.770	-23.206	326	5281	0.24	3.84
5(6)	0.1069	-34.649	15.449	11773	2341	8.57	1.70
6(7)	0.0993	37.100	17.202	13498	2902	9.82	2.11
7(8)	0.0945	-2.257	18.934	50	3516	0.04	2.56
8(9)	0.0759	3.188	44.500	100	19420	0.07	14.13
9(10)	0.0745	4.595	-30.468	207	9104	0.15	6.62
10(11)	0.0732	46.217	0.663	20947	4	15.24	0.00
11(12)	0.0706	3.124	-44.338	96	19279	0.07	14.03
12(13)	0.0692	-2.813	19.420	78	3698	0.06	2.69
13(14)	0.0687	-15.506	-6.085	2358	363	1.72	0.26
14(15)	0.0682	9.493	-0.478	884	2	0.64	0.00
15(16)	0.0681	3.745	-15.015	138	2211	0.10	1.61
16(17)	0.0671	13.880	-6.344	1889	395	1.37	0.29
17(18)	0.0668	0.586	5.331	3	279	0.00	0.20
18(19)	0.0660	-31.566	-1.255	9771	15	7.11	0.01
19(21)	0.0648	-10.820	-5.713	1148	320	0.84	0.23
20(22)	0.0647	-14.120	1.744	1955	30	1.42	0.02
21(23)	0.0646	-26.936	-3.482	7115	119	5.18	0.09
22(24)	0.0637	14.952	4.644	2192	212	1.60	0.15
23(25)	0.0629	2.372	-12.898	55	1631	0.04	1.19
24(26)	0.0626	7.137	-1.442	499	20	0.36	0.01
25(27)	0.0623	0.231	-3.900	1	149	0.00	0.11
26(28)	0.0620	-0.894	14.707	8	2121	0.01	1.54
27(30)	0.0613	5.389	-1.340	285	18	0.21	0.01
28(32)	0.0605	-9.131	-1.154	818	13	0.59	0.01
29(33)	0.0599	5.481	4.903	295	236	0.21	0.17
30(35)	0.0591	12.710	-2.132	1584	45	1.15	0.03
31(36)	0.0588	-8.290	-3.843	674	145	0.49	0.11
32(38)	0.0578	-1.112	7.461	12	546	0.01	0.40
33(39)	0.0572	-0.324	19.378	1	3683	0.00	2.68
34(40)	0.0568	-1.862	-11.495	34	1296	0.02	0.94
35(41)	0.0566	-2.092	-5.830	43	333	0.03	0.24
36(42)	0.0553	-9.341	-11.994	856	1411	0.62	1.03
37(43)	0.0551	4.940	-0.544	239	3	0.17	0.00
38(45)	0.0550	-7.230	-2.216	513	48	0.37	0.04
39(46)	0.0541	33.963	-17.049	11312	2850	8.23	2.07
40(47)	0.0539	39.257	-1.031	15113	10	11.00	0.01
41(48)	0.0532	-9.876	-10.194	956	1019	0.70	0.74
42(51)	0.0529	-3.452	-8.128	117	648	0.09	0.47
43(52)	0.0527	-3.699	-4.855	134	231	0.10	0.17
44(53)	0.0525	2.401	20.767	57	4229	0.04	3.08
45(54)	0.0521	-10.153	3.637	1011	130	0.74	0.09
46(55)	0.0520	2.291	-13.206	51	1710	0.04	1.24
47(56)	0.0519	3.722	-5.872	136	338	0.10	0.25
48(57)	0.0517	13.046	4.779	1669	224	1.21	0.16
49(59)	0.0510	0.771	-9.374	6	862	0.00	0.63
50(61)	0.0505	4.715	-0.222	218	0	0.16	0.00
51(63)	0.0498	1.376	5.177	19	263	0.01	0.19
52(65)	0.0495	8.984	11.558	791	1310	0.58	0.95
53(66)	0.0494	-7.577	5.210	563	266	0.41	0.19
54(68)	0.0486	2.630	3.979	68	155	0.05	0.11
55(70)	0.0483	-3.899	-5.875	149	338	0.11	0.25
56(72)	0.0479	-0.014	10.046	0	990	0.00	0.72

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
57(73)	0.0477	-8.665	-20.039	736	3938	0.54	2.87
58(76)	0.0468	-5.045	11.125	250	1214	0.18	0.88
59(77)	0.0465	5.703	-17.901	319	3142	0.23	2.29
60(78)	0.0465	-2.805	8.599	77	725	0.06	0.53
61(80)	0.0459	5.163	2.631	261	68	0.19	0.05
62(81)	0.0457	-1.975	14.058	38	1938	0.03	1.41
63(82)	0.0457	-4.861	6.860	232	461	0.17	0.34
64(83)	0.0455	1.974	22.831	38	5112	0.03	3.72
65(87)	0.0445	-5.109	8.311	256	677	0.19	0.49
66(90)	0.0442	-3.390	-6.856	113	461	0.08	0.34
67(92)	0.0440	-1.024	4.210	10	174	0.01	0.13
68(96)	0.0436	3.917	3.621	150	129	0.11	0.09
69(98)	0.0431	1.524	-11.179	23	1225	0.02	0.89
70(101)	0.0427	-1.571	5.959	24	348	0.02	0.25
71(104)	0.0422	0.686	-12.230	5	1467	0.00	1.07
72(112)	0.0412	-1.786	-5.756	31	325	0.02	0.24
73(113)	0.0410	-1.385	-10.697	19	1122	0.01	0.82
74(114)	0.0409	4.551	0.164	203	0	0.15	0.00
75(116)	0.0407	-4.037	-1.855	160	34	0.12	0.02
Somma delle Masse Modali [kgm*g]				124280	119434		
Masse strutturali libere [kgm*g]				137417	137417		
Percentuale				90.44	86.91	90.44	86.91

Posizione masse 4

Numero di Frequenze calcolate =120, filtrate=81

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
				kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(2)	0.1318	-19.453	1.275	3711	16	2.70	0.01
2(3)	0.1203	25.435	-4.922	6345	238	4.62	0.17
3(4)	0.1189	13.747	-2.212	1853	48	1.35	0.03
4(5)	0.0978	33.153	15.076	10779	2229	7.85	1.62
5(6)	0.0954	-32.993	10.146	10675	1010	7.77	0.73
6(7)	0.0913	-1.376	-30.638	19	9206	0.01	6.70
7(8)	0.0806	-8.612	-16.321	727	2612	0.53	1.90
8(9)	0.0798	2.836	42.550	79	17755	0.06	12.92
9(10)	0.0748	-6.572	1.880	424	35	0.31	0.03
10(11)	0.0746	1.260	13.289	16	1732	0.01	1.26
11(12)	0.0720	-1.183	-42.377	14	17611	0.01	12.82
12(13)	0.0713	52.074	-3.589	26592	126	19.35	0.09
13(15)	0.0688	7.268	7.402	518	537	0.38	0.39
14(16)	0.0688	-0.198	-13.842	0	1879	0.00	1.37
15(17)	0.0680	-7.762	29.904	591	8770	0.43	6.38
16(18)	0.0668	-7.559	-16.919	560	2807	0.41	2.04
17(19)	0.0660	-0.776	5.110	6	256	0.00	0.19
18(20)	0.0654	-9.216	-10.310	833	1042	0.61	0.76
19(21)	0.0649	32.560	-16.069	10397	2532	7.57	1.84
20(22)	0.0645	-29.738	-2.202	8673	48	6.31	0.03
21(23)	0.0642	-1.117	10.641	12	1110	0.01	0.81
22(24)	0.0640	-7.004	-2.913	481	83	0.35	0.06
23(25)	0.0636	-13.286	2.102	1731	43	1.26	0.03
24(28)	0.0613	2.696	-4.821	71	228	0.05	0.17
25(29)	0.0604	11.736	1.956	1351	38	0.98	0.03
26(30)	0.0601	-11.676	-13.639	1337	1824	0.97	1.33
27(31)	0.0600	5.933	3.557	345	124	0.25	0.09
28(32)	0.0588	-0.832	-15.313	7	2300	0.00	1.67
29(33)	0.0585	3.060	7.666	92	576	0.07	0.42
30(35)	0.0578	0.362	5.670	1	315	0.00	0.23
31(36)	0.0574	-6.447	1.424	408	20	0.30	0.01
32(37)	0.0574	-8.866	2.013	771	40	0.56	0.03
33(38)	0.0572	1.743	7.964	30	622	0.02	0.45
34(39)	0.0560	-5.480	-5.648	294	313	0.21	0.23
35(41)	0.0554	-2.965	12.529	86	1539	0.06	1.12
36(43)	0.0549	-33.749	16.253	11170	2591	8.13	1.89
37(44)	0.0547	5.395	-0.691	285	5	0.21	0.00
38(45)	0.0544	-23.089	-7.510	5228	553	3.81	0.40
39(46)	0.0542	30.247	2.937	8972	85	6.53	0.06
40(47)	0.0540	-17.045	-4.943	2849	240	2.07	0.17
41(49)	0.0532	0.432	-10.720	2	1127	0.00	0.82
42(50)	0.0526	6.055	3.309	360	107	0.26	0.08
43(51)	0.0524	-2.275	-6.847	51	460	0.04	0.33
44(54)	0.0514	4.472	-1.836	196	33	0.14	0.02
45(56)	0.0508	0.545	-6.074	3	362	0.00	0.26
46(57)	0.0507	-0.935	4.366	9	187	0.01	0.14
47(58)	0.0504	3.081	5.575	93	305	0.07	0.22
48(59)	0.0502	0.564	6.031	3	357	0.00	0.26
49(60)	0.0500	1.710	-11.241	29	1239	0.02	0.90

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
50(61)	0.0496	7.350	31.068	530	9466	0.39	6.89
51(63)	0.0490	0.825	8.372	7	687	0.00	0.50
52(65)	0.0486	-4.278	7.655	179	575	0.13	0.42
53(66)	0.0485	-0.938	4.707	9	217	0.01	0.16
54(67)	0.0482	3.389	-11.337	113	1260	0.08	0.92
55(69)	0.0479	-0.532	5.205	3	266	0.00	0.19
56(71)	0.0473	-10.138	-15.622	1008	2393	0.73	1.74
57(72)	0.0472	5.704	10.202	319	1021	0.23	0.74
58(77)	0.0459	2.256	-9.601	50	904	0.04	0.66
59(78)	0.0458	2.478	-6.372	60	398	0.04	0.29
60(79)	0.0458	6.048	-12.456	359	1522	0.26	1.11
61(80)	0.0453	3.905	-16.881	150	2795	0.11	2.03
62(81)	0.0453	-4.805	1.090	226	12	0.16	0.01
63(82)	0.0450	6.200	-2.276	377	51	0.27	0.04
64(84)	0.0448	1.152	-6.146	13	370	0.01	0.27
65(86)	0.0446	-0.751	6.339	6	394	0.00	0.29
66(87)	0.0445	0.756	-4.125	6	167	0.00	0.12
67(90)	0.0443	0.412	-4.539	2	202	0.00	0.15
68(92)	0.0441	2.466	-4.269	60	179	0.04	0.13
69(93)	0.0437	1.978	8.496	38	708	0.03	0.52
70(96)	0.0432	-2.788	6.091	76	364	0.06	0.26
71(98)	0.0428	-1.318	-6.446	17	407	0.01	0.30
72(100)	0.0425	1.951	10.403	37	1061	0.03	0.77
73(101)	0.0424	4.863	3.760	232	139	0.17	0.10
74(102)	0.0423	-5.053	1.723	250	29	0.18	0.02
75(103)	0.0423	-4.034	8.790	160	758	0.12	0.55
76(107)	0.0418	5.202	8.931	265	782	0.19	0.57
77(108)	0.0417	2.939	6.160	85	372	0.06	0.27
78(109)	0.0416	2.141	-5.148	45	260	0.03	0.19
79(112)	0.0412	3.571	7.574	125	563	0.09	0.41
80(115)	0.0409	-3.419	-9.332	115	854	0.08	0.62
81(116)	0.0408	2.020	-4.571	40	205	0.03	0.15
Somma delle Masse Modali [kgm*g]				124035	116691		
Masse strutturali libere [kgm*g]				137398	137398		
Percentuale				90.27	85.93	90.27	85.93

Risultati Analisi Dinamica - Spostamenti massimi - Nodi

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	mrad	mrad	mrad
1	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
2	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
3	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
4	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
5	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
6	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
7	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
8	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
9	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
10	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
12	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
13	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
14	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
15	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
16	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
17	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
18	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
19	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
20	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
22	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
23	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
24	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
25	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
26	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
27	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
28	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
29	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
30	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
32	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
33	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
34	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
35	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
36	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
37	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
38	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
39	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
40	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
41	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
42	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
43	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
44	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
45	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
46	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
47	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
48	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
49	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
51	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
52	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
53	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
54	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
55	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
56	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
57	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
58	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
59	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
60	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
62	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
63	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
64	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
65	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
66	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
67	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
68	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
69	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
71	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
72	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
73	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
74	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
75	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
76	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
77	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
78	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
79	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
80	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
81	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
82	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
83	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
84	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
85	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
86	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
87	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
88	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
89	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
90	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
92	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
10004	-0.10(12-II-4)	0.09(13-I-4)	-0.01(13-II-4)	0.72(13-II-4)	-0.77(12-II-4)	-0.20(13-I-4)
10005	0.01(12-II-3)	0.10(13-I-4)	-0.01(2)	-0.80(13-I-4)	0.07(12-II-3)	-0.03(12-I-1)
10006	-0.01(12-I-3)	0.09(13-I-1)	-0.01(2)	-0.74(13-I-4)	-0.08(12-I-3)	0.04(12-II-1)
10007	0.10(12-I-4)	0.10(13-I-4)	-0.02(2)	-0.74(13-I-4)	0.73(12-I-4)	0.12(13-I-2)
10008	-0.09(12-II-4)	0.09(13-I-1)	-0.02(2)	-0.72(13-I-1)	-0.70(12-II-4)	-0.12(12-II-4)
10009	0.01(12-II-3)	0.09(13-I-2)	-0.01(2)	-0.77(13-I-2)	0.09(12-II-3)	-0.03(12-I-1)
10010	-0.01(12-I-3)	0.10(13-I-2)	-0.01(2)	-0.78(13-I-2)	-0.08(12-I-3)	0.03(12-II-1)
10011	0.10(12-I-4)	0.08(13-I-2)	-0.01(2)	0.60(13-II-2)	0.75(12-I-4)	0.16(12-I-4)
10014	-0.10(12-II-1)	0.01(13-I-4)	-0.01(13-I-4)	-0.15(13-I-4)	-0.86(12-II-1)	0.05(13-I-4)
10017	0.10(12-I-1)	0.01(13-I-4)	-0.01(2)	-0.15(13-I-4)	-0.84(12-II-1)	-0.03(13-II-4)
10018	0.10(12-I-1)	0.01(13-I-1)	-0.01(2)	-0.14(13-I-1)	0.83(12-I-1)	0.03(13-I-2)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
10021	0.10(12-I-1)	0.01(13-I-2)	-0.01(2)	-0.14(13-I-2)	0.82(12-I-1)	-0.05(13-I-2)
10024	-0.12(12-II-1)	-0.01(13-II-4)	-0.01(12-II-1)	0.12(13-II-4)	-1.00(12-II-1)	-0.03(13-I-4)
10027	0.11(12-I-1)	-0.01(13-II-4)	-0.01(2)	0.13(13-II-4)	0.94(12-I-1)	0.03(13-II-4)
10028	0.11(12-I-1)	-0.01(13-II-2)	-0.01(2)	0.13(13-II-2)	0.92(12-I-1)	-0.03(13-II-2)
10031	0.11(12-I-1)	-0.01(13-II-2)	-0.01(2)	0.11(13-I-2)	0.96(12-I-1)	0.04(13-II-2)
10034	-0.10(12-II-1)	-0.10(13-II-4)	-0.01(12-II-4)	0.84(13-II-4)	-0.85(12-II-1)	0.08(12-II-2)
10035	0.01(12-I-1)	-0.10(13-II-4)	-0.01(12-I-1)	0.88(13-II-4)	0.12(12-I-1)	0.03(12-I-1)
10036	-0.01(12-II-1)	-0.10(13-II-4)	-0.01(2)	0.85(13-II-4)	-0.13(12-II-1)	-0.03(12-II-1)
10037	0.10(12-I-1)	-0.10(13-II-4)	-0.01(2)	0.87(13-II-4)	-0.83(12-I-1)	-0.08(12-I-4)
10038	0.10(12-I-1)	-0.10(13-II-2)	-0.01(2)	0.84(13-II-2)	0.82(12-I-1)	0.07(12-II-2)
10039	0.01(12-I-1)	-0.10(13-II-2)	-0.01(2)	0.89(13-II-2)	0.13(12-I-1)	0.03(12-I-1)
10040	-0.01(12-II-1)	-0.10(13-II-2)	-0.01(2)	0.86(13-II-2)	-0.12(12-II-1)	-0.03(12-II-1)
10041	0.10(12-I-2)	-0.08(13-II-2)	-0.01(2)	0.70(13-II-2)	0.83(12-I-2)	-0.09(12-I-2)
10044	-0.11(12-II-4)	-0.10(13-II-4)	-0.01(12-II-4)	0.80(13-II-4)	-0.89(12-II-4)	-0.09(12-II-4)
10045	0.01(12-I-4)	-0.10(13-II-4)	-0.01(12-I-4)	-0.83(13-I-4)	0.12(12-I-4)	-0.03(12-I-3)
10046	-0.01(12-II-4)	-0.09(13-II-4)	-0.01(2)	-0.81(13-I-4)	-0.13(12-II-4)	0.04(12-II-3)
10047	0.10(12-I-4)	-0.10(13-II-4)	-0.01(2)	-0.82(13-I-4)	-0.83(12-II-4)	-0.08(13-II-4)
10048	0.10(12-I-2)	-0.10(13-II-2)	-0.01(2)	-0.79(13-I-2)	0.82(12-I-2)	0.08(12-I-4)
10049	0.01(12-I-4)	-0.10(13-II-2)	-0.01(2)	0.84(13-II-2)	0.12(12-I-2)	-0.03(12-I-3)
10050	-0.01(12-II-2)	-0.09(13-II-2)	-0.01(2)	-0.81(13-I-2)	-0.12(12-II-2)	0.03(12-II-3)
10051	0.10(12-I-2)	-0.08(13-II-2)	-0.01(2)	0.66(13-II-2)	0.84(12-I-2)	0.08(12-I-2)
10054	-0.11(12-II-3)	0.01(13-I-4)	-0.01(12-II-3)	-0.11(13-I-4)	-0.98(12-II-3)	0.03(13-I-1)
10057	0.11(12-I-3)	0.01(13-I-4)	-0.01(2)	-0.12(13-I-4)	0.97(12-I-3)	-0.03(13-I-4)
10058	0.11(12-I-3)	0.01(13-I-2)	-0.01(2)	-0.12(13-I-2)	0.95(12-I-3)	0.03(13-I-2)
10061	0.11(12-I-3)	0.01(13-I-2)	-0.01(2)	-0.10(13-I-2)	0.94(12-I-3)	-0.04(13-I-2)
10064	-0.12(12-II-3)	-0.01(13-II-4)	-0.01(12-II-3)	0.11(13-II-4)	-1.01(12-II-3)	-0.03(13-I-4)
10067	0.11(12-I-3)	-0.01(13-II-4)	-0.01(2)	0.12(13-II-4)	-0.96(12-II-3)	0.03(13-II-4)
10068	0.11(12-I-3)	-0.01(13-II-2)	-0.01(2)	0.12(13-II-2)	0.95(12-I-3)	-0.03(13-II-2)
10071	0.11(12-I-3)	-0.01(13-II-2)	-0.01(2)	0.10(13-II-2)	0.96(12-I-3)	0.03(13-II-2)
10074	-0.10(12-II-3)	0.10(13-I-4)	-0.01(13-I-4)	-0.80(13-I-4)	-0.83(12-II-3)	0.10(12-II-3)
10075	0.01(12-I-3)	0.10(13-I-4)	-0.01(12-I-3)	-0.82(13-I-4)	0.11(12-I-3)	0.04(12-I-3)
10076	-0.01(12-II-3)	0.10(13-I-4)	-0.01(2)	-0.82(13-I-4)	-0.12(12-II-3)	-0.04(12-II-3)
10077	0.10(12-I-3)	0.10(13-I-4)	-0.01(2)	-0.82(13-I-4)	-0.79(12-II-3)	0.10(12-II-3)
10078	0.09(12-I-3)	0.10(13-I-2)	-0.01(2)	-0.79(13-I-2)	0.79(12-I-3)	-0.09(12-I-3)
10079	0.01(12-I-3)	0.10(13-I-2)	-0.01(2)	-0.85(13-I-2)	0.12(12-I-3)	0.04(12-I-3)
10080	-0.01(12-II-3)	0.09(13-I-2)	-0.01(2)	-0.80(13-I-2)	-0.11(12-II-3)	-0.04(12-II-3)
10081	0.10(12-I-3)	0.08(13-I-2)	-0.01(2)	0.66(13-II-2)	0.80(12-I-3)	-0.11(12-I-3)
11498	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11499	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11500	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11501	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11502	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11503	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11504	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11505	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11506	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11507	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11508	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11509	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11510	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11511	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11512	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11513	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11514	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11515	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11516	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11517	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11518	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11519	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11520	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11521	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11522	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11523	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11524	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11525	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11526	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11527	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11528	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11529	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11530	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11531	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11532	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11533	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11534	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11535	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11536	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11537	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11538	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11539	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
11540	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11541	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11542	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
11543	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
20770	-0.25(12-II-1)	0.25(13-I-1)	-0.01(2)	-0.92(13-I-1)	-0.93(12-II-1)	-0.19(12-I-1)
20773	-0.24(12-II-1)	0.40(13-I-1)	-0.02(2)	1.45(13-II-1)	-0.90(12-II-1)	0.18(12-II-1)
20776	0.24(12-I-1)	0.41(13-I-1)	-0.02(2)	1.51(13-II-1)	0.89(12-I-1)	-0.19(13-I-1)
20779	0.25(12-I-1)	0.29(13-I-1)	-0.01(2)	-1.07(13-I-1)	0.92(12-I-1)	0.20(12-II-1)
20782	-0.22(12-II-1)	-0.10(13-II-1)	-0.01(2)	0.55(13-II-1)	-0.87(12-II-1)	-0.33(13-II-2)
20790	0.23(12-I-1)	-0.09(13-II-1)	-0.01(2)	0.49(13-II-1)	0.89(12-I-1)	0.25(13-II-1)
20802	0.23(12-I-1)	-0.18(13-II-1)	-0.03(2)	1.04(13-II-1)	0.94(12-I-1)	-0.14(13-II-2)
20809	-0.24(12-II-1)	-0.17(13-II-1)	-0.03(2)	0.94(13-II-1)	-0.97(12-II-1)	0.10(13-II-4)
20821	0.24(12-I-1)	0.13(13-I-2)	-0.02(2)	-0.74(13-I-2)	0.93(12-I-1)	0.19(13-II-2)
20825	-0.26(12-II-1)	0.12(13-I-1)	-0.02(2)	-0.68(13-I-4)	-1.00(12-II-1)	-0.13(13-I-4)
20828	-0.63(12-II-1)	0.25(13-I-1)	-0.03(2)	-0.56(13-I-1)	1.18(12-I-1)	0.33(12-II-1)
20830	0.62(12-I-1)	0.41(13-I-1)	-0.04(2)	-0.87(13-I-1)	-1.17(12-II-1)	-0.33(12-I-1)
20832	-0.62(12-II-1)	0.43(13-I-1)	-0.04(2)	-0.91(13-I-1)	1.17(12-I-1)	0.33(12-II-1)
20834	0.63(12-I-1)	0.30(13-I-1)	-0.03(2)	-0.65(13-I-1)	-1.19(12-II-1)	-0.34(12-I-1)
20844	0.24(12-I-1)	0.11(12-I-2)	-0.01(2)	-0.57(13-I-2)	0.92(12-I-1)	0.19(13-II-2)
20847	-0.26(12-II-1)	0.11(13-I-4)	-0.01(2)	-0.63(13-I-4)	-1.00(12-II-1)	-0.19(13-II-4)
20854	-0.75(12-II-1)	-0.25(13-II-4)	-0.03(2)	0.61(13-II-4)	1.13(12-I-1)	-0.39(12-I-4)
20855	-0.75(12-II-1)	-0.40(13-II-4)	-0.04(2)	0.82(13-II-4)	-1.23(12-II-1)	-0.44(13-II-3)
20856	-0.74(12-II-1)	-0.70(13-II-4)	-0.06(2)	1.66(13-II-4)	-1.17(12-II-1)	-0.42(13-II-3)
20857	0.77(12-I-1)	-0.48(2)	-0.06(2)	0.99(13-I-1)	1.24(12-I-1)	-0.27(13-I-3)
20858	0.78(12-I-1)	-0.53(2)	-0.05(2)	1.09(13-II-4)	-1.20(12-II-1)	0.11(13-II-4)
20859	-0.78(12-II-1)	-0.53(2)	-0.05(2)	1.11(13-II-1)	-1.21(12-II-1)	-0.20(13-I-2)
20860	0.78(12-I-1)	-0.48(2)	-0.06(2)	0.89(2)	-1.23(12-II-1)	0.23(13-II-1)
20861	0.77(12-I-1)	-0.59(13-II-2)	-0.06(2)	1.40(13-II-2)	1.26(12-I-1)	-0.15(13-II-4)
20862	0.78(12-I-1)	-0.46(13-II-2)	-0.05(2)	0.97(13-II-2)	1.25(12-I-1)	0.41(13-II-2)
20863	0.78(12-I-1)	-0.21(13-II-3)	-0.04(2)	0.47(13-II-3)	1.23(12-I-1)	0.46(13-II-2)
21498	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21499	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21500	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21501	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21502	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21503	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21504	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21505	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21506	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21507	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21508	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21509	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21510	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21511	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21512	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
21513	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
30635	-0.05(12-II-1)	-0.06(13-II-1)	-0.01(2)	0.50(13-II-1)	-0.40(12-II-1)	-0.08(12-I-2)
30638	0.05(12-I-1)	-0.10(13-II-1)	-0.01(2)	0.74(13-II-1)	0.36(12-I-1)	0.08(13-I-1)
30641	-0.05(12-II-1)	-0.10(13-II-1)	-0.01(2)	0.76(13-II-1)	-0.36(12-II-1)	-0.08(13-I-1)
30644	0.05(12-I-1)	-0.07(13-II-1)	-0.01(2)	0.55(13-II-1)	0.40(12-I-1)	0.08(12-II-1)
30653	-0.05(12-II-1)	-0.07(13-II-1)	-0.01(2)	0.54(13-II-1)	-0.38(12-II-1)	-0.07(13-I-1)
30662	0.05(12-I-1)	-0.06(13-II-1)	-0.01(2)	0.49(13-II-1)	0.39(12-I-1)	0.07(12-II-4)
30687	0.05(12-I-2)	-0.11(13-II-2)	-0.01(2)	0.84(13-II-2)	0.43(12-I-2)	0.10(13-I-2)
30695	-0.06(12-II-4)	0.10(13-I-1)	-0.01(2)	0.75(13-II-1)	-0.44(12-II-4)	-0.09(12-I-4)
30704	-0.20(12-II-1)	0.07(13-I-1)	-0.02(2)	0.37(13-II-1)	-0.65(12-II-1)	0.17(12-II-1)
30707	-0.20(12-II-1)	0.10(13-I-1)	-0.03(2)	0.58(13-II-1)	-0.62(12-II-1)	0.14(12-II-1)
30710	0.19(12-I-1)	0.11(13-I-1)	-0.03(2)	0.59(13-II-1)	0.59(12-I-1)	0.17(12-II-1)
30713	0.20(12-I-1)	0.08(13-I-1)	-0.02(2)	0.41(13-II-1)	0.63(12-I-1)	-0.17(12-I-1)
30718	0.07(12-I-2)	-0.10(13-II-2)	-0.01(2)	0.78(13-II-2)	0.51(12-I-2)	-0.09(13-I-2)
30722	-0.19(12-II-2)	0.08(13-I-1)	-0.02(2)	0.43(13-II-1)	-0.61(12-II-1)	0.19(12-II-2)
30726	-0.06(12-II-4)	-0.10(13-II-4)	-0.01(2)	0.77(13-II-4)	-0.44(12-II-4)	0.08(13-I-1)
30731	0.18(12-I-1)	0.08(13-I-1)	-0.02(2)	0.39(13-II-1)	0.58(12-I-1)	-0.19(12-I-4)
30738	0.05(12-I-2)	0.07(13-I-3)	-0.01(2)	0.50(13-II-3)	0.43(12-I-2)	0.09(12-II-2)
30746	-0.20(12-II-2)	0.14(13-I-1)	-0.03(2)	0.67(13-II-1)	0.63(12-I-2)	0.15(12-II-2)
30750	-0.05(12-II-4)	0.08(13-I-4)	-0.01(2)	0.57(13-II-4)	-0.43(12-II-4)	-0.09(12-I-4)
30754	0.18(12-I-4)	0.12(13-I-1)	-0.03(2)	0.60(13-II-1)	-0.61(12-II-4)	0.17(12-II-4)
30762	-0.06(12-II-2)	0.07(13-I-3)	-0.01(2)	0.52(13-II-3)	0.40(12-I-2)	0.09(12-II-2)
30764	0.05(13-I-4)	-0.06(13-II-4)	-0.01(2)	0.49(13-II-4)	-0.36(12-II-4)	-0.07(12-I-4)
30765	0.20(12-I-2)	0.13(13-I-2)	-0.03(2)	0.63(13-II-2)	0.64(12-I-2)	0.15(12-II-2)
30786	-0.20(12-II-4)	0.12(13-I-1)	-0.03(2)	0.61(13-II-4)	-0.63(12-II-4)	0.14(12-II-4)
30798	0.18(12-I-2)	0.11(12-I-2)	-0.02(2)	-0.37(13-I-3)	0.61(12-I-2)	-0.15(13-I-2)
30805	-0.19(12-II-4)	0.11(13-I-4)	-0.02(2)	-0.47(13-I-4)	-0.62(12-II-4)	0.15(12-II-4)
30816	-0.08(12-II-2)	0.08(13-I-3)	-0.02(2)	0.32(13-II-3)	-0.31(12-II-2)	-0.05(12-I-2)
30817	0.07(12-I-4)	0.08(13-I-4)	-0.02(2)	0.41(13-II-4)	-0.33(12-II-4)	0.04(12-II-1)
31498	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31499	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31500	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31501	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31502	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
31503	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31504	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31505	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31506	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31507	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31508	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31509	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31510	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31511	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31512	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
31513	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
40004	0.27(12-I-4)	0.28(13-I-4)	-0.10(2)	-1.08(13-I-4)	-0.86(12-II-4)	-0.10(12-II-4)
40005	0.25(12-I-4)	0.33(13-I-4)	-0.13(2)	-1.87(13-I-3)	-1.00(12-II-4)	0.15(12-I-4)
40006	-0.27(12-II-4)	0.28(13-I-1)	-0.13(2)	-0.73(13-I-3)	1.01(12-I-4)	-0.16(13-II-4)
40007	-0.28(12-II-4)	0.30(13-I-4)	-0.14(2)	-0.99(13-I-4)	0.80(12-I-3)	0.15(12-I-4)
40008	0.28(12-I-4)	0.30(13-I-1)	-0.14(2)	-0.98(13-I-1)	-0.81(12-II-3)	-0.14(12-II-4)
40009	0.27(12-I-4)	0.28(13-I-2)	-0.14(2)	-0.68(13-I-1)	-1.01(12-II-3)	0.14(13-II-2)
40010	-0.26(12-II-4)	0.31(13-I-2)	-0.13(2)	-1.55(13-I-3)	1.01(12-I-3)	-0.15(12-I-2)
40011	-0.27(12-II-4)	0.25(13-I-2)	-0.13(2)	-1.44(13-I-2)	0.83(12-I-3)	0.13(12-I-4)
40014	0.25(12-I-1)	0.27(13-I-4)	-0.09(13-I-4)	0.25(13-II-4)	0.07(12-I-4)	-0.20(12-II-4)
40015	0.25(12-I-1)	0.30(13-I-4)	-0.11(2)	0.22(13-I-3)	-0.22(12-II-1)	0.11(12-II-4)
40016	-0.27(12-II-1)	0.26(13-I-1)	-0.12(2)	0.26(13-II-4)	0.22(12-I-1)	0.10(12-I-4)
40017	-0.27(12-II-1)	0.29(13-I-4)	-0.12(2)	0.26(13-II-4)	-0.06(12-II-4)	0.21(12-I-4)
40018	0.27(12-I-1)	0.28(13-I-1)	-0.12(2)	0.27(13-II-2)	0.05(12-I-4)	-0.20(12-II-4)
40019	0.27(12-I-1)	0.27(13-I-2)	-0.12(2)	0.28(13-II-2)	-0.22(12-II-1)	-0.10(12-I-4)
40020	-0.25(12-II-1)	0.29(13-I-2)	-0.12(2)	0.20(13-II-2)	0.22(12-I-1)	-0.10(12-II-4)
40021	-0.25(12-II-1)	0.24(13-I-2)	-0.11(2)	0.28(13-II-2)	-0.06(12-II-2)	0.21(12-I-4)
40024	0.29(12-I-1)	-0.27(13-II-4)	-0.09(13-II-4)	-0.23(13-I-4)	0.04(13-I-4)	0.10(12-II-2)
40025	0.28(12-I-1)	-0.28(13-II-4)	-0.11(2)	-0.22(13-I-4)	-0.25(12-II-1)	-0.05(12-II-1)
40026	-0.30(12-II-1)	-0.27(13-II-4)	-0.12(2)	-0.22(13-I-4)	0.24(12-I-1)	0.04(12-I-3)
40027	-0.30(12-II-1)	-0.30(13-II-4)	-0.12(2)	-0.24(13-I-4)	-0.04(13-I-4)	-0.11(12-I-4)
40028	0.30(12-I-1)	-0.29(13-II-2)	-0.12(2)	-0.23(13-I-2)	0.03(13-II-2)	0.10(12-II-2)
40029	0.30(12-I-1)	-0.28(13-II-2)	-0.12(2)	-0.23(13-I-2)	-0.25(12-II-1)	0.04(12-I-3)
40030	-0.28(12-II-1)	-0.27(13-II-2)	-0.12(2)	-0.20(13-I-2)	0.24(12-I-1)	0.07(13-II-2)
40031	-0.28(12-II-1)	-0.24(13-II-2)	-0.11(2)	-0.19(13-I-2)	-0.04(13-II-2)	-0.11(12-I-2)
40034	0.27(12-I-1)	-0.28(13-II-4)	-0.08(2)	0.04(13-I-4)	0.04(2)	-0.05(12-II-2)
40035	0.27(12-I-1)	-0.28(13-II-4)	-0.11(2)	0.04(12-I-1)	-0.24(12-II-1)	-0.09(13-I-4)
40036	-0.29(12-II-1)	-0.28(13-II-4)	-0.12(2)	0.04(12-II-1)	0.24(12-I-1)	0.11(13-I-4)
40037	-0.29(12-II-1)	-0.30(13-II-4)	-0.12(2)	0.03(13-I-1)	-0.04(12-I-4)	-0.05(12-II-4)
40038	0.29(12-I-1)	-0.29(13-II-2)	-0.12(2)	0.03(2)	0.03(1)	0.05(12-I-3)
40039	0.28(12-I-1)	-0.28(13-II-2)	-0.12(2)	0.04(12-I-1)	-0.24(12-II-1)	-0.11(13-I-4)
40040	-0.27(12-II-2)	-0.27(13-II-2)	-0.12(2)	0.04(12-II-1)	0.24(12-I-1)	0.12(13-I-2)
40041	-0.27(12-II-2)	-0.24(13-II-2)	-0.11(2)	0.04(13-I-2)	-0.04(2)	-0.12(13-II-2)
40044	0.28(12-I-4)	0.26(13-I-4)	-0.08(2)	-0.03(13-II-4)	0.04(2)	0.06(12-II-4)
40045	0.28(12-I-4)	0.27(13-I-4)	-0.11(2)	-0.03(12-I-3)	-0.25(12-II-4)	0.09(13-II-4)
40046	-0.29(12-II-4)	0.26(13-I-4)	-0.12(2)	-0.04(12-II-3)	0.24(12-I-4)	-0.11(13-II-4)
40047	-0.29(12-II-4)	0.28(13-I-4)	-0.12(2)	-0.03(1)	-0.03(12-I-4)	0.05(13-I-4)
40048	0.29(12-I-2)	0.28(13-I-2)	-0.12(2)	-0.03(1)	0.03(1)	0.04(12-II-3)
40049	0.29(12-I-2)	0.27(13-I-2)	-0.12(2)	-0.03(12-I-3)	-0.25(12-II-2)	0.10(13-II-4)
40050	-0.28(12-II-2)	0.26(13-I-2)	-0.12(2)	-0.04(12-II-3)	0.24(12-I-2)	-0.12(13-II-2)
40051	-0.28(12-II-2)	0.23(13-I-2)	-0.11(2)	-0.03(13-II-2)	-0.04(13-I-2)	-0.12(13-II-2)
40054	0.29(12-I-3)	0.26(13-I-4)	-0.09(13-I-4)	0.24(13-II-4)	0.04(12-I-4)	-0.11(12-II-4)
40055	0.29(12-I-3)	0.27(13-I-4)	-0.11(2)	0.23(13-II-4)	-0.25(12-II-3)	0.06(12-II-4)
40056	-0.30(12-II-3)	0.26(13-I-4)	-0.12(2)	0.23(13-II-4)	0.24(12-I-3)	-0.05(13-II-4)
40057	-0.30(12-II-3)	0.28(13-I-4)	-0.12(2)	0.25(13-II-4)	-0.04(13-II-4)	0.10(12-I-1)
40058	0.30(12-I-3)	0.28(13-I-2)	-0.12(2)	0.25(13-II-2)	0.03(13-II-2)	-0.10(12-II-1)
40059	0.30(12-I-3)	0.27(13-I-2)	-0.12(2)	0.24(13-II-2)	-0.25(12-II-3)	0.04(12-I-3)
40060	-0.28(12-II-3)	0.26(13-I-2)	-0.12(2)	0.21(13-II-2)	0.24(12-I-3)	-0.07(13-I-2)
40061	-0.28(12-II-3)	0.23(13-I-2)	-0.11(2)	0.20(13-II-2)	-0.05(13-I-2)	0.10(12-I-1)
40064	0.29(12-I-3)	-0.26(13-II-4)	-0.09(13-II-4)	-0.23(13-I-4)	0.04(13-II-1)	0.16(12-II-3)
40065	0.29(12-I-3)	-0.26(13-II-4)	-0.11(2)	-0.21(13-I-4)	-0.24(12-II-3)	-0.08(12-II-3)
40066	-0.30(12-II-3)	-0.26(13-II-4)	-0.12(2)	-0.21(13-I-4)	0.23(12-I-3)	-0.08(12-II-3)
40067	-0.30(12-II-3)	-0.28(13-II-4)	-0.12(2)	-0.23(13-I-4)	-0.04(12-I-3)	-0.13(12-I-3)
40068	0.30(12-I-3)	-0.27(13-II-2)	-0.12(2)	-0.23(13-I-2)	0.03(12-II-3)	0.13(12-II-3)
40069	0.30(12-I-3)	-0.27(13-II-2)	-0.12(2)	-0.22(13-I-2)	-0.24(12-II-3)	0.08(12-I-3)
40070	-0.29(12-II-3)	-0.25(13-II-2)	-0.12(2)	-0.20(13-I-2)	0.23(12-I-3)	-0.08(12-I-3)
40071	-0.29(12-II-3)	-0.23(13-II-2)	-0.11(2)	-0.19(13-I-2)	-0.05(13-II-2)	-0.15(12-I-3)
40074	0.26(12-I-3)	-0.26(13-II-4)	-0.08(2)	0.05(12-I-3)	0.04(2)	-0.14(12-I-3)
40075	0.26(12-I-3)	-0.26(13-II-4)	-0.10(2)	0.05(12-I-3)	-0.23(12-II-3)	-0.10(12-I-3)
40076	-0.27(12-II-3)	-0.26(13-II-4)	-0.11(2)	0.05(12-II-3)	0.23(12-I-3)	0.11(13-I-4)
40077	-0.27(12-II-3)	-0.28(13-II-4)	-0.11(2)	0.03(2)	-0.04(12-I-3)	-0.14(12-I-3)
40078	0.27(12-I-3)	-0.27(13-II-2)	-0.11(2)	0.04(12-I-3)	0.03(12-II-3)	0.14(12-II-3)
40079	0.27(12-I-3)	-0.27(13-II-2)	-0.11(2)	0.05(12-I-3)	-0.23(12-II-3)	-0.10(13-I-4)
40080	-0.26(12-II-3)	-0.25(13-II-2)	-0.11(2)	0.04(12-II-3)	0.22(12-I-3)	0.13(13-I-2)
40081	-0.26(12-II-3)	-0.23(13-II-2)	-0.10(2)	0.03(12-II-3)	-0.04(12-I-3)	-0.16(12-I-3)
50445	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50449	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50453	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50457	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
50466	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50470	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50486	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50490	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50499	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50503	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50527	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50540	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50570	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50580	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50603	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50612	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50622	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50626	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50668	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50672	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50676	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50682	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50717	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50736	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
50737	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
60445	-0.06(12-II-1)	-0.06(13-II-1)	-0.01(2)	0.46(13-II-4)	-0.44(12-II-1)	-0.15(12-I-1)
60449	-0.05(12-II-1)	-0.06(13-II-1)	-0.01(2)	0.46(13-II-1)	-0.38(12-II-1)	0.14(12-II-1)
60453	0.05(12-I-1)	-0.06(13-II-1)	-0.01(2)	0.46(13-II-1)	0.38(12-I-1)	-0.14(12-I-1)
60457	0.06(12-I-1)	-0.06(13-II-1)	-0.01(2)	0.45(13-II-1)	0.43(12-I-1)	0.15(12-II-1)
60466	-0.01(12-II-1)	-0.00(13-II-3)	-0.01(2)	0.05(13-II-3)	-0.07(12-II-1)	0.03(12-II-2)
60470	0.01(12-I-1)	-0.00(13-II-4)	-0.01(2)	0.04(13-II-4)	0.07(12-I-1)	-0.03(2)
60486	0.01(12-I-1)	-0.01(12-II-2)	-0.01(2)	0.07(12-II-2)	0.07(12-I-1)	-0.03(12-I-1)
60490	-0.05(12-II-1)	-0.06(13-II-2)	-0.01(2)	0.44(13-II-2)	-0.37(12-II-1)	-0.16(12-I-2)
60499	0.05(12-I-1)	-0.06(13-II-4)	-0.01(2)	0.43(13-II-4)	0.36(12-I-1)	0.16(12-II-4)
60503	-0.01(12-II-1)	-0.01(12-I-4)	-0.01(2)	0.07(12-I-4)	-0.06(12-II-1)	0.04(12-II-1)
60527	0.05(12-I-1)	-0.06(13-II-2)	-0.01(2)	0.46(13-II-2)	0.42(12-I-1)	0.15(12-II-2)
60540	-0.05(12-II-4)	-0.06(13-II-1)	-0.01(2)	0.42(13-II-1)	-0.42(12-II-4)	-0.15(12-I-4)
60554	-0.32(12-II-1)	-0.06(13-II-1)	-0.03(2)	0.36(13-II-4)	-0.94(12-II-1)	0.26(12-II-1)
60557	0.31(12-I-1)	-0.06(13-II-1)	-0.03(2)	0.37(13-II-1)	0.93(12-I-1)	-0.27(12-I-1)
60560	-0.31(12-II-1)	-0.06(13-II-1)	-0.03(2)	0.37(13-II-1)	-0.93(12-II-1)	0.27(12-II-1)
60563	0.32(12-I-1)	-0.06(13-II-1)	-0.03(2)	0.36(13-II-1)	0.94(12-I-1)	-0.26(12-I-1)
60570	0.05(12-I-2)	-0.07(13-II-2)	-0.01(2)	0.48(13-II-2)	0.40(12-I-2)	-0.14(12-I-1)
60576	0.29(12-I-1)	-0.12(12-II-2)	-0.03(2)	0.45(12-II-2)	0.88(12-I-1)	0.28(12-II-2)
60580	-0.05(12-II-4)	-0.06(13-II-4)	-0.01(2)	0.47(13-II-4)	-0.38(12-II-4)	0.15(12-II-4)
60585	-0.29(12-II-4)	-0.12(12-I-4)	-0.03(2)	0.44(12-I-4)	-0.87(12-II-1)	-0.27(12-I-4)
60603	0.06(12-I-2)	-0.07(13-II-3)	-0.01(2)	0.50(13-II-3)	0.43(12-I-2)	0.14(12-II-1)
60608	0.30(12-I-2)	0.10(12-I-2)	-0.03(2)	0.38(13-II-2)	0.93(12-I-2)	-0.28(12-I-2)
60612	-0.05(12-II-4)	-0.07(13-II-4)	-0.01(2)	0.47(13-II-4)	-0.42(12-II-4)	-0.15(12-I-4)
60617	-0.30(12-II-4)	0.10(12-II-4)	-0.03(2)	0.34(13-II-1)	-0.93(12-II-4)	0.28(12-II-4)
60622	0.04(12-I-2)	0.02(12-I-2)	-0.01(2)	0.17(12-II-2)	0.31(12-I-2)	0.03(13-I-3)
60626	-0.04(12-II-4)	-0.02(12-I-4)	-0.01(2)	0.17(12-I-4)	-0.30(12-II-4)	-0.03(12-I-4)
60649	0.31(12-I-2)	0.11(12-I-2)	-0.03(2)	0.42(13-II-2)	0.93(12-I-2)	0.26(12-II-1)
60658	-0.30(12-II-4)	-0.12(12-I-4)	-0.03(2)	0.43(12-I-4)	-0.91(12-II-4)	-0.27(12-I-4)
60668	0.04(12-I-2)	0.03(12-I-2)	-0.01(2)	-0.22(12-I-2)	0.33(12-I-2)	-0.03(12-I-3)
60672	-0.04(12-II-4)	0.03(12-II-4)	-0.01(2)	-0.23(12-II-4)	-0.31(12-II-4)	0.03(12-I-4)
60676	0.06(13-II-3)	-0.07(13-II-3)	-0.01(2)	0.58(13-II-3)	0.43(13-II-3)	-0.17(12-I-2)
60682	-0.06(13-II-4)	-0.07(13-II-4)	-0.01(2)	0.56(13-II-4)	-0.43(13-II-4)	0.16(12-II-4)
60683	0.31(12-I-2)	-0.13(12-II-2)	-0.03(2)	0.46(12-II-2)	0.92(12-I-2)	-0.26(12-I-1)
60691	-0.31(12-II-4)	-0.13(12-I-4)	-0.03(2)	0.45(12-I-4)	-0.93(12-II-4)	0.27(12-II-4)
60734	0.08(12-I-2)	-0.10(12-II-2)	-0.03(2)	0.47(12-II-2)	0.42(12-I-1)	-0.11(12-I-2)
60735	-0.08(12-II-4)	-0.10(12-I-4)	-0.03(2)	0.50(12-I-4)	-0.44(12-II-4)	0.10(12-II-4)
61498	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61499	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61500	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61501	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61502	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61503	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61504	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61505	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61506	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61507	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61508	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61509	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61510	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61511	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61512	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61513	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61514	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61515	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61516	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61517	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61518	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
61519	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
61520	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70001	0.91(12-I-4)	0.83(13-I-4)	-0.02(2)	1.34(2)	0.62(2)	0.57(13-II-4)
70002	-0.88(12-II-3)	0.64(13-I-3)	-0.02(2)	1.69(2)	-0.90(2)	0.53(12-II-3)
70003	0.79(12-I-4)	0.51(13-I-4)	-0.06(2)	1.61(2)	0.33(12-II-3)	-0.54(12-II-4)
70004	0.78(12-I-4)	0.67(13-I-4)	-0.14(2)	2.18(2)	0.28(12-I-4)	-0.40(13-II-4)
70005	0.77(12-I-4)	1.24(13-I-3)	-0.18(2)	3.11(2)	-0.14(12-II-4)	-0.41(12-II-1)
70006	0.75(12-I-4)	0.51(13-I-1)	-0.19(2)	3.04(2)	0.14(12-I-4)	-0.45(12-II-4)
70007	0.74(12-I-4)	0.63(13-I-4)	-0.19(2)	3.09(2)	0.16(12-I-4)	0.42(12-I-4)
70008	0.74(12-I-4)	0.61(13-I-1)	-0.19(2)	3.08(2)	-0.16(12-II-4)	-0.40(12-II-1)
70009	0.74(12-I-3)	0.44(13-I-1)	-0.19(2)	3.02(2)	-0.14(12-II-3)	0.42(12-I-1)
70010	0.74(12-I-3)	1.05(13-I-2)	-0.18(2)	3.02(2)	0.13(12-I-3)	0.43(12-I-1)
70011	-0.76(12-II-3)	0.76(13-I-2)	-0.18(2)	2.79(2)	-0.20(12-II-3)	0.36(13-II-2)
70012	0.77(12-I-3)	0.41(13-I-2)	-0.08(2)	2.15(2)	-0.54(2)	0.68(12-I-2)
70262	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70266	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70270	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70274	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70279	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70283	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70290	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70294	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70303	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70312	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70333	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70346	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70384	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70396	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70418	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70429	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70461	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70474	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70518	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70532	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70553	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70592	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70630	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
70770	0.27(12-I-1)	0.28(13-I-1)	-0.04(2)	-0.55(13-II-1)	0.17(2)	-0.33(12-I-1)
70773	0.27(12-I-1)	0.45(13-I-1)	-0.08(2)	-1.00(13-II-1)	-0.06(12-I-1)	-0.38(12-I-1)
70776	-0.27(12-II-1)	0.47(13-I-1)	-0.08(2)	-1.01(13-II-1)	0.06(12-II-1)	0.38(12-II-1)
70779	-0.27(12-II-1)	0.33(13-I-1)	-0.04(2)	-0.60(13-II-1)	-0.14(2)	0.32(12-II-1)
70782	-0.27(12-II-1)	0.32(13-I-1)	-0.04(2)	-0.52(13-II-1)	0.15(2)	0.25(13-I-2)
70790	0.28(12-I-1)	0.28(13-I-1)	-0.04(2)	-0.48(13-II-1)	-0.12(13-II-1)	-0.17(13-II-4)
70802	0.28(12-I-1)	0.61(13-I-1)	-0.10(2)	-1.55(2)	-0.67(2)	-0.30(12-I-1)
70809	-0.29(12-II-1)	0.53(13-I-1)	-0.10(2)	-1.60(2)	0.68(2)	0.30(12-II-1)
70812	0.59(12-I-1)	0.29(13-I-1)	-0.33(2)	-0.11(13-I-1)	1.53(2)	0.47(12-II-1)
70813	0.59(12-I-1)	0.46(13-I-1)	-0.64(2)	-0.16(13-I-1)	-0.16(2)	-0.33(12-I-1)
70814	0.59(12-I-1)	0.48(13-I-1)	-0.65(2)	-0.17(13-I-1)	0.16(2)	-0.33(12-I-1)
70815	0.59(12-I-1)	0.34(13-I-1)	-0.33(2)	-0.14(13-I-1)	-1.51(2)	-0.48(12-I-1)
70821	-0.28(12-II-1)	0.56(13-I-2)	-0.08(2)	-0.60(13-II-2)	-0.31(13-II-2)	0.50(12-II-1)
70825	0.29(12-I-1)	0.53(13-I-4)	-0.08(2)	-0.70(13-II-4)	0.35(13-II-4)	-0.51(12-I-1)
70828	-0.67(12-II-1)	0.30(13-I-1)	-0.08(2)	0.35(2)	-0.39(2)	-0.20(12-II-4)
70830	0.67(12-I-1)	0.47(13-I-1)	-0.08(2)	1.01(2)	0.12(2)	0.22(12-I-4)
70832	0.67(12-I-1)	0.49(13-I-1)	-0.08(2)	1.07(2)	-0.07(12-I-1)	-0.23(12-II-2)
70834	0.67(12-I-1)	0.35(13-I-1)	-0.08(2)	0.40(2)	0.51(2)	0.19(12-I-2)
70838	0.66(12-I-1)	0.67(13-I-1)	-1.56(2)	-0.69(2)	0.78(2)	0.32(12-II-1)
70840	-0.66(12-II-1)	0.58(13-I-1)	-1.63(2)	-1.14(2)	-0.96(2)	-0.35(12-I-4)
70842	-0.64(12-II-1)	0.61(13-I-2)	-0.34(2)	0.52(2)	-2.69(2)	-0.83(12-I-1)
70843	0.64(12-I-1)	0.56(13-I-4)	-0.51(2)	-0.16(13-II-4)	2.43(2)	0.80(12-II-1)
70844	-0.28(12-II-1)	0.35(13-I-2)	-0.03(2)	0.36(2)	0.13(12-II-2)	-0.70(12-I-1)
70847	0.31(12-I-1)	0.41(13-I-4)	-0.03(2)	0.33(13-I-4)	-0.15(12-I-1)	0.75(12-II-4)
70850	-0.29(12-II-1)	0.33(13-I-2)	-0.03(2)	0.31(12-II-2)	0.26(12-II-2)	-0.33(12-I-2)
70851	0.32(12-I-1)	0.40(13-I-4)	-0.03(2)	0.32(13-I-4)	-0.25(12-I-1)	0.42(12-II-4)
70854	-0.75(12-II-1)	0.50(13-I-4)	-0.05(2)	-1.23(2)	-0.30(2)	1.04(12-II-4)
70855	-0.76(12-II-1)	0.68(13-I-4)	-0.07(2)	-2.75(2)	0.88(2)	-0.29(12-I-3)
70856	-0.77(12-II-1)	1.25(13-I-3)	-0.14(2)	-4.04(2)	0.15(12-I-1)	-0.42(12-I-4)
70857	-0.79(12-II-1)	0.50(13-I-1)	-0.14(2)	-3.57(2)	-0.45(2)	0.52(13-II-1)
70858	0.80(12-I-1)	0.62(13-I-4)	-0.12(2)	-3.99(2)	0.13(12-II-1)	-0.42(13-I-3)
70859	0.80(12-I-1)	0.61(13-I-1)	-0.12(2)	-3.91(2)	0.09(12-II-1)	0.45(13-II-2)
70860	0.81(12-I-1)	0.44(13-I-1)	-0.13(2)	-3.61(2)	0.29(2)	-0.40(13-I-2)
70861	0.79(12-I-1)	1.06(13-I-2)	-0.14(2)	-3.46(2)	-0.58(2)	0.53(13-I-3)
70862	0.79(12-I-1)	0.76(13-I-2)	-0.11(2)	-3.33(2)	-0.56(2)	0.34(12-II-3)
70863	0.78(12-I-1)	0.40(13-I-2)	-0.08(2)	-1.44(2)	-0.30(2)	-1.11(12-I-1)
70866	-0.77(12-II-1)	0.60(13-I-4)	-0.72(2)	-0.88(2)	-0.56(2)	-1.00(13-II-3)
70868	-0.78(12-II-1)	0.60(13-I-1)	-0.87(2)	0.78(2)	-1.06(2)	0.66(13-II-4)
70870	-0.79(12-II-1)	0.31(13-I-1)	-0.29(2)	-1.30(2)	0.84(2)	0.56(13-II-3)
70872	0.80(12-I-1)	0.48(13-I-1)	-0.30(2)	-1.73(2)	1.00(2)	-0.57(13-I-3)
70874	0.80(12-I-1)	0.50(13-I-1)	-0.24(2)	-1.72(2)	0.86(2)	0.58(13-II-3)
70876	0.81(12-I-1)	0.36(13-I-1)	-0.27(2)	-1.30(2)	1.21(2)	0.51(13-II-3)
70877	0.80(12-I-1)	0.69(13-I-1)	-0.61(2)	1.51(2)	-1.08(2)	-1.04(13-II-3)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
70879	0.79(12-I-1)	0.64(13-I-2)	-0.43(2)	-0.46(13-I-2)	-1.07(2)	-0.36(12-I-4)
70884	0.97(12-I-4)	0.68(13-I-4)	-1.35(2)	-2.12(2)	1.50(2)	-0.43(12-I-3)
70885	0.98(12-I-4)	1.25(13-I-3)	-1.96(2)	-2.96(2)	-0.08(13-II-3)	0.38(12-II-3)
70886	0.98(12-I-4)	0.51(13-I-1)	-1.87(2)	-2.95(2)	-0.11(13-I-4)	-0.40(12-I-3)
70887	0.98(12-I-4)	0.63(13-I-4)	-1.92(2)	-2.97(2)	0.08(13-II-3)	0.36(12-II-3)
70888	0.98(12-I-4)	0.61(13-I-1)	-1.91(2)	-2.97(2)	-0.08(13-II-4)	-0.38(12-I-3)
70889	0.98(12-I-4)	0.44(13-I-1)	-1.86(2)	-2.95(2)	0.10(13-I-3)	0.37(12-II-3)
70890	0.97(12-I-4)	1.06(13-I-2)	-1.85(2)	-2.94(2)	-0.10(13-II-2)	-0.38(12-I-3)
70891	0.96(12-I-4)	0.76(13-I-2)	-1.72(2)	-2.72(2)	-0.55(2)	0.44(12-II-3)
70892	0.96(12-I-4)	0.50(13-I-4)	-0.79(2)	-1.33(2)	0.72(2)	-0.30(13-I-4)
70893	0.95(12-I-4)	0.40(13-I-2)	-1.04(2)	-1.74(2)	-1.29(2)	0.35(12-II-3)
70894	-0.53(12-II-2)	0.55(12-II-3)	-0.04(2)	0.44(12-I-3)	-0.69(12-II-3)	-1.32(12-I-4)
70895	0.54(12-I-4)	0.59(13-I-4)	-0.04(2)	0.43(13-II-3)	0.63(13-I-3)	1.33(12-II-4)
70896	0.93(12-I-2)	0.63(13-I-2)	-0.23(2)	1.08(2)	-1.37(2)	-0.66(12-I-4)
70897	-0.97(12-II-4)	0.79(13-I-4)	-0.19(2)	0.96(2)	1.17(2)	0.71(12-II-2)
70898	1.01(12-I-4)	0.67(13-I-4)	-1.34(2)	2.15(2)	1.39(2)	-0.31(13-II-4)
70899	1.01(12-I-4)	1.25(13-I-3)	-1.90(2)	3.14(2)	-0.09(13-II-3)	-0.35(12-II-1)
70900	1.01(12-I-4)	0.51(13-I-1)	-1.84(2)	3.01(2)	-0.08(13-I-4)	0.39(12-I-1)
70901	1.01(12-I-4)	0.63(13-I-4)	-1.88(2)	3.08(2)	0.07(13-II-3)	-0.37(12-II-1)
70902	1.01(12-I-4)	0.61(13-I-1)	-1.87(2)	3.07(2)	-0.08(13-II-4)	0.37(12-I-1)
70903	1.00(12-I-4)	0.44(13-I-1)	-1.84(2)	3.00(2)	-0.09(13-II-3)	-0.38(12-II-1)
70904	0.99(12-I-4)	1.06(13-I-2)	-1.83(2)	2.98(2)	0.08(13-I-2)	0.38(12-I-1)
70905	0.99(12-I-4)	0.76(13-I-2)	-1.71(2)	2.74(2)	-0.44(2)	0.35(12-I-1)
70906	1.01(12-I-4)	0.51(13-I-4)	-0.77(2)	1.30(2)	0.99(2)	-0.29(13-II-4)
70907	0.99(12-I-4)	0.41(13-I-2)	-1.04(2)	1.66(2)	-1.57(2)	0.27(12-I-1)
70908	0.91(12-I-4)	0.51(13-I-4)	-0.32(2)	1.88(2)	0.60(2)	0.68(12-I-1)
70909	-0.88(12-II-3)	0.41(13-I-2)	-0.43(2)	2.52(2)	-1.01(2)	-0.70(12-II-1)
71498	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
80262	-0.05(12-II-1)	-0.05(13-II-1)	-0.01(2)	0.35(13-II-1)	-0.38(12-II-1)	-0.08(12-I-1)
80266	0.04(12-I-1)	-0.06(13-II-1)	-0.01(2)	0.46(13-II-1)	0.33(12-I-1)	0.07(12-II-1)
80270	0.04(12-I-1)	-0.06(13-II-1)	-0.01(2)	0.45(13-II-1)	-0.33(12-I-1)	-0.07(12-I-1)
80274	0.05(12-I-1)	-0.04(13-II-1)	-0.01(2)	0.34(13-II-1)	0.38(12-I-1)	0.09(12-II-1)
80279	-0.05(12-II-1)	-0.04(13-II-1)	-0.01(2)	0.33(13-II-1)	-0.36(12-II-1)	-0.06(12-I-2)
80283	0.04(12-I-1)	-0.04(13-II-1)	-0.01(2)	0.33(13-II-1)	0.35(12-I-1)	0.06(12-II-4)
80290	0.05(12-I-1)	-0.04(13-II-2)	-0.01(2)	0.29(13-II-2)	0.37(12-I-1)	0.06(12-II-1)
80294	-0.05(12-II-1)	-0.04(13-II-1)	-0.01(2)	0.28(13-II-1)	-0.37(12-II-1)	-0.06(12-I-1)
80303	-0.05(12-II-1)	-0.04(13-II-2)	-0.01(2)	0.32(13-II-2)	-0.35(12-II-1)	-0.08(12-II-2)
80312	0.04(12-I-1)	-0.04(13-II-4)	-0.01(2)	0.30(13-II-4)	0.34(12-I-1)	0.08(12-II-3)
80333	0.05(12-I-2)	-0.05(13-II-2)	-0.01(2)	0.38(13-II-2)	0.40(12-I-2)	0.08(12-II-2)
80346	-0.05(12-II-4)	-0.05(13-II-4)	-0.01(2)	0.36(13-II-4)	-0.39(12-II-4)	-0.08(12-I-4)
80351	-0.20(12-II-1)	0.05(13-I-1)	-0.02(2)	0.26(13-II-1)	-0.65(12-II-1)	0.17(12-II-1)
80354	-0.20(12-II-1)	-0.06(13-II-1)	-0.03(2)	0.37(13-II-1)	-0.61(12-II-1)	-0.17(12-I-1)
80357	0.20(12-I-1)	-0.06(13-II-1)	-0.03(2)	0.36(13-II-1)	0.61(12-I-1)	0.17(12-II-1)
80360	0.20(12-I-1)	0.05(13-I-1)	-0.02(2)	0.25(13-II-1)	0.64(12-I-1)	-0.17(12-I-1)
80363	-0.19(12-II-1)	0.05(13-I-1)	-0.02(2)	0.25(13-II-1)	-0.60(12-II-1)	0.14(12-II-2)
80367	-0.19(12-II-1)	0.05(13-I-1)	-0.02(2)	0.26(13-II-1)	0.59(12-I-1)	-0.14(12-I-4)
80378	0.19(12-I-1)	0.04(13-I-2)	-0.02(2)	0.22(13-II-2)	0.61(12-I-1)	-0.14(12-I-2)
80384	0.05(12-I-2)	-0.06(13-II-2)	-0.01(2)	0.47(13-II-2)	0.40(12-I-2)	-0.06(12-I-1)
80389	-0.19(12-II-1)	0.05(12-II-3)	-0.02(2)	0.21(13-II-1)	-0.61(12-II-1)	0.15(12-II-1)
80392	-0.19(12-II-2)	-0.06(12-II-2)	-0.02(2)	0.25(13-II-2)	-0.59(12-II-2)	0.17(12-II-2)
80396	-0.05(12-II-4)	-0.06(13-II-4)	-0.01(2)	0.42(13-II-4)	-0.40(12-II-4)	0.06(12-II-1)
80401	0.19(12-I-4)	-0.07(12-I-3)	-0.02(2)	0.26(12-I-3)	0.58(12-I-4)	-0.17(12-I-4)
80418	0.05(12-I-2)	-0.05(13-II-3)	-0.01(2)	0.38(13-II-3)	0.43(12-I-2)	0.08(12-I-2)
80424	0.19(12-I-2)	-0.06(13-II-2)	-0.03(2)	0.31(13-II-2)	0.63(12-I-2)	-0.17(12-I-2)
80429	-0.05(12-II-4)	-0.05(13-II-4)	-0.01(2)	0.36(13-II-4)	-0.40(12-II-4)	-0.08(12-I-4)
80437	-0.19(12-II-4)	-0.06(12-I-1)	-0.03(2)	0.30(13-II-1)	-0.63(12-II-4)	0.17(12-II-4)
80461	0.05(12-I-2)	-0.06(13-II-3)	-0.01(2)	0.44(13-II-3)	0.42(12-I-2)	-0.05(12-I-2)
80474	-0.05(12-II-4)	-0.05(13-II-4)	-0.01(2)	0.39(13-II-4)	-0.38(12-II-4)	0.09(12-II-4)
80481	0.20(12-I-2)	-0.07(13-II-2)	-0.03(2)	0.39(13-II-2)	0.64(12-I-2)	0.17(12-II-2)
80495	-0.20(12-II-4)	-0.06(13-II-4)	-0.03(2)	0.35(13-II-4)	-0.65(12-II-4)	-0.16(12-I-4)
80518	0.07(12-I-2)	-0.06(13-II-3)	-0.01(2)	0.45(13-II-2)	0.52(12-I-2)	0.08(12-II-2)
80522	0.20(12-I-2)	0.07(12-I-2)	-0.02(2)	0.30(13-II-2)	0.66(12-I-2)	-0.16(12-I-2)
80532	-0.07(12-II-3)	-0.09(13-II-4)	-0.01(2)	0.66(13-II-4)	-0.57(12-II-3)	-0.10(12-I-3)
80536	-0.20(12-II-4)	0.08(12-II-4)	-0.02(2)	0.29(13-II-4)	-0.65(12-II-4)	0.16(12-II-1)
80546	0.19(12-I-2)	-0.10(12-II-2)	-0.02(2)	0.35(13-II-2)	0.59(12-I-2)	0.17(12-II-2)
80550	0.19(12-I-4)	-0.11(12-I-4)	-0.02(2)	0.37(12-I-4)	-0.58(12-II-4)	-0.19(12-I-3)
80553	0.05(13-I-3)	-0.07(13-II-3)	-0.01(2)	0.51(13-II-3)	0.41(12-I-2)	0.09(12-II-2)
80597	0.20(12-I-2)	-0.10(12-II-1)	-0.02(2)	0.34(13-II-2)	0.67(12-I-2)	-0.16(12-I-2)
80600	-0.20(12-II-4)	-0.11(12-I-4)	-0.03(2)	0.46(13-II-4)	-0.69(12-II-4)	0.19(12-II-4)
80621	-0.09(12-II-2)	-0.08(13-II-3)	-0.02(2)	0.37(13-II-3)	0.38(12-I-2)	-0.05(12-I-1)
90704	-0.23(12-II-1)	0.22(13-I-1)	-0.05(2)	-0.58(13-II-1)	0.26(2)	0.14(12-II-1)
90707	-0.24(12-II-1)	0.33(13-I-1)	-0.08(2)	-1.02(13-II-1)	0.07(12-II-1)	0.12(12-II-1)
90710	-0.24(12-II-1)	0.34(13-I-1)	-0.08(2)	-1.03(13-II-1)	0.07(12-II-1)	-0.12(12-I-1)
90713	-0.24(12-II-1)	0.25(13-I-1)	-0.05(2)	-0.65(13-II-1)	-0.21(2)	-0.15(12-I-1)
90722	-0.24(12-II-1)	0.24(13-I-1)	-0.05(2)	-0.63(2)	0.09(12-II-1)	0.14(12-II-1)
90731	-0.23(12-II-1)	0.21(13-I-1)	-0.05(2)	-0.62(2)	0.09(12-II-1)	-0.16(12-I-1)
90741	-0.31(12-II-1)	0.22(13-I-1)	-0.39(2)	-0.12(13-I-1)	0.59(2)	-0.20(12-I-1)
90742	-0.31(12-II-1)	0.34(13-I-1)	-0.66(2)	-0.17(13-I-1)	0.03(13-I-2)	-0.15(12-I-1)
90743	-0.31(12-II-1)	0.35(13-I-1)	-0.66(2)	-0.17(13-I-1)	-0.03(13-I-1)	-0.15(12-I-1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
90744	-0.31(12-II-1)	0.25(13-I-1)	-0.39(2)	-0.13(13-I-1)	-0.60(2)	-0.19(12-I-1)
90746	-0.25(12-II-2)	0.43(13-I-1)	-0.08(2)	-1.03(13-II-2)	-0.39(13-II-2)	0.13(12-II-2)
90749	-0.31(12-II-1)	0.25(13-I-1)	-0.39(2)	-0.28(2)	0.53(2)	-0.20(12-I-1)
90754	0.25(12-I-4)	0.40(13-I-1)	-0.08(2)	-0.95(13-II-1)	0.36(13-II-1)	-0.12(12-I-1)
90757	-0.31(12-II-1)	0.22(13-I-1)	-0.39(2)	-0.28(2)	-0.52(2)	-0.20(12-I-1)
90765	-0.26(12-II-2)	0.38(13-I-2)	-0.08(2)	-1.03(13-II-2)	-0.37(13-II-2)	-0.11(13-I-1)
90768	-0.31(12-II-2)	0.46(13-I-1)	-0.64(2)	-0.26(13-I-2)	0.09(13-II-2)	-0.16(12-I-1)
90770	-0.28(12-II-1)	0.23(13-I-1)	-0.04(2)	0.72(2)	-0.07(13-I-1)	0.16(12-II-1)
90773	-0.28(12-II-1)	0.35(13-I-1)	-0.09(2)	1.18(2)	0.04(12-I-3)	-0.16(12-I-1)
90776	-0.28(12-II-1)	0.36(13-I-1)	-0.09(2)	1.19(2)	0.03(12-I-3)	0.16(12-II-1)
90779	0.28(12-I-1)	0.26(13-I-1)	-0.04(2)	0.74(2)	-0.07(13-II-2)	-0.15(12-I-1)
90782	0.28(12-I-1)	0.26(13-I-1)	-0.05(2)	0.66(2)	0.27(2)	0.14(12-II-1)
90786	0.23(12-I-4)	0.37(13-I-4)	-0.08(2)	-0.99(13-II-4)	0.39(13-II-4)	0.12(12-II-1)
90789	0.31(12-I-4)	0.42(13-I-1)	-0.64(2)	-0.22(13-I-1)	-0.08(13-II-1)	-0.17(12-I-1)
90790	-0.28(12-II-1)	0.22(13-I-1)	-0.05(2)	0.67(2)	-0.31(2)	0.15(12-II-1)
90798	-0.22(12-II-2)	0.22(13-I-3)	-0.06(2)	-0.50(2)	-0.42(2)	0.15(12-II-1)
90801	-0.32(12-II-2)	0.39(13-I-2)	-0.69(2)	-0.24(13-I-2)	-0.10(13-I-2)	-0.17(12-I-1)
90802	-0.28(12-II-1)	0.47(13-I-1)	-0.11(2)	1.15(13-I-2)	0.42(13-I-2)	-0.17(12-II-1)
90805	-0.22(12-II-4)	0.28(13-I-4)	-0.06(2)	-0.56(13-II-4)	0.46(2)	0.16(12-II-1)
90808	0.30(12-I-1)	0.39(13-I-4)	-0.67(2)	-0.22(13-I-4)	0.09(13-I-4)	0.17(12-II-1)
90809	0.29(12-I-1)	0.43(13-I-1)	-0.11(2)	0.97(13-I-1)	-0.37(13-I-1)	0.18(12-II-1)
90816	-0.21(12-II-2)	0.22(12-I-2)	-0.06(2)	-0.54(2)	-0.23(2)	0.23(12-II-2)
90817	-0.22(12-II-4)	0.27(13-I-4)	-0.06(2)	-0.58(2)	0.28(2)	-0.24(12-I-4)
90820	-0.28(12-II-2)	0.24(13-I-3)	-0.43(2)	0.15(13-II-2)	-0.62(2)	-0.21(12-I-1)
90821	0.27(12-I-1)	0.41(13-I-2)	-0.08(2)	1.35(2)	0.49(2)	-0.20(12-I-1)
90824	0.28(12-I-4)	0.30(13-I-4)	-0.43(2)	0.17(13-II-4)	0.57(2)	-0.22(12-I-1)
90825	0.28(12-I-1)	0.40(13-I-4)	-0.09(2)	1.26(2)	-0.47(2)	-0.21(12-I-1)
90836	-0.26(12-II-2)	0.25(12-I-2)	-0.43(2)	-0.49(2)	0.37(2)	0.25(12-II-2)
90837	-0.28(12-II-4)	0.30(13-I-4)	-0.43(2)	-0.48(2)	-0.37(2)	-0.26(12-I-4)
90844	-0.25(12-II-1)	0.25(13-I-2)	-0.03(2)	1.01(2)	0.35(2)	-0.28(12-II-2)
90847	-0.28(12-II-1)	0.31(13-I-4)	-0.03(2)	0.95(2)	-0.36(2)	0.31(12-II-4)
90850	-0.25(12-II-1)	0.24(13-I-3)	-0.03(2)	0.81(2)	0.62(2)	0.28(12-II-2)
90851	-0.28(12-II-1)	0.31(13-I-4)	-0.03(2)	0.79(2)	-0.59(2)	0.30(12-II-4)
90852	-0.55(12-II-3)	0.65(12-II-3)	-0.04(2)	-0.31(12-II-3)	-0.69(2)	0.33(12-II-2)
90853	0.49(12-I-4)	0.58(13-I-4)	-0.04(2)	-0.25(13-I-3)	0.69(2)	-0.30(12-I-4)
90882	-0.58(12-II-3)	0.63(12-II-3)	-0.31(2)	1.00(2)	-1.12(2)	0.20(12-II-2)
90883	0.55(12-I-4)	0.60(13-I-4)	-0.31(2)	1.00(2)	1.13(2)	-0.20(12-I-4)
90894	-0.60(12-II-2)	0.59(12-II-3)	-0.04(2)	0.83(2)	-0.30(12-II-3)	0.53(12-II-2)
90895	0.58(12-I-4)	0.61(13-I-4)	-0.04(2)	0.85(2)	-0.33(13-II-3)	-0.54(12-I-4)
91498	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91499	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91500	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91501	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91502	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91503	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91504	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91505	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91506	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91507	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91508	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91509	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91510	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91511	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91512	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91513	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91514	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91515	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91516	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91517	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91518	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91519	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91520	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91521	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
91522	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
100635	-0.09(12-II-1)	0.11(13-I-1)	-0.05(2)	-0.81(2)	0.22(2)	0.15(12-II-1)
100638	0.09(12-I-1)	0.15(13-I-1)	-0.07(2)	-1.07(2)	-0.07(12-II-1)	-0.17(12-I-1)
100641	-0.09(12-II-1)	0.16(13-I-1)	-0.07(2)	-1.06(2)	0.07(12-I-1)	0.17(12-II-1)
100644	0.09(12-I-1)	0.12(13-I-1)	-0.05(2)	-0.80(2)	-0.21(2)	-0.15(12-I-1)
100653	-0.09(12-II-1)	0.12(13-I-1)	-0.05(2)	-0.83(2)	-0.10(13-I-1)	0.16(12-II-1)
100662	0.09(12-I-1)	0.11(13-I-1)	-0.05(2)	-0.82(2)	0.10(13-I-1)	-0.16(12-I-4)
100677	0.24(12-I-1)	0.12(13-I-1)	-0.48(2)	-0.15(13-I-1)	0.74(2)	-0.09(12-I-1)
100678	0.24(12-I-1)	0.16(13-I-1)	-0.66(2)	-0.22(13-I-1)	-0.08(13-II-1)	-0.13(12-I-1)
100679	0.24(12-I-1)	0.17(13-I-1)	-0.66(2)	-0.23(13-I-1)	0.08(13-II-1)	0.12(12-II-1)
100680	0.24(12-I-1)	0.13(13-I-1)	-0.48(2)	-0.16(13-I-1)	-0.73(2)	-0.09(12-I-1)
100687	-0.10(12-II-2)	0.19(13-I-2)	-0.07(2)	-0.98(2)	-0.41(2)	-0.17(12-I-2)
100690	0.23(12-I-1)	0.13(13-I-1)	-0.48(2)	-0.33(2)	0.67(2)	-0.09(12-I-1)
100695	0.10(12-I-4)	0.17(13-I-1)	-0.07(2)	-0.98(2)	0.41(2)	0.16(12-II-4)
100698	0.23(12-I-1)	0.12(13-I-1)	-0.48(2)	-0.32(2)	-0.66(2)	0.09(12-II-1)
100704	0.22(12-I-1)	0.12(13-I-1)	-0.06(2)	0.91(2)	0.18(2)	-0.09(12-I-1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
100707	0.22(12-I-1)	0.17(13-I-1)	-0.08(2)	1.31(13-I-1)	0.04(12-II-1)	0.08(13-II-1)
100710	-0.22(12-II-1)	0.17(13-I-1)	-0.08(2)	1.34(13-I-1)	0.05(12-II-1)	-0.08(13-I-1)
100713	0.22(12-I-1)	0.13(13-I-1)	-0.05(2)	0.95(13-I-1)	-0.15(2)	0.09(12-II-1)
100718	-0.11(12-II-2)	0.17(13-I-2)	-0.07(2)	-0.99(2)	-0.36(2)	0.15(12-II-2)
100721	-0.23(12-II-2)	0.21(13-I-1)	-0.67(2)	-0.28(13-I-2)	-0.11(13-I-1)	-0.13(12-I-2)
100722	0.22(12-I-1)	0.13(13-I-1)	-0.06(2)	0.88(13-I-1)	0.48(2)	0.09(12-II-1)
100726	0.10(12-I-4)	0.17(13-I-4)	-0.07(2)	-1.00(2)	0.37(2)	-0.15(12-I-4)
100729	0.24(12-I-4)	0.19(13-I-1)	-0.67(2)	-0.25(13-I-1)	0.11(13-I-1)	0.12(12-II-1)
100731	-0.21(12-I-1)	0.12(13-I-1)	-0.05(2)	0.81(13-I-1)	-0.45(2)	0.10(12-II-1)
100738	0.09(12-I-2)	0.13(13-I-3)	-0.06(2)	-0.70(2)	-0.49(2)	-0.13(12-I-2)
100745	0.24(12-I-2)	0.19(13-I-2)	-0.66(2)	-0.24(13-I-2)	0.15(13-II-2)	-0.12(12-I-2)
100746	0.22(12-I-2)	0.22(13-I-1)	-0.09(2)	1.48(13-I-2)	0.57(13-I-2)	0.11(13-I-2)
100750	-0.09(12-II-4)	0.14(13-I-4)	-0.06(2)	-0.67(2)	0.50(2)	0.13(12-II-4)
100753	0.23(12-I-4)	0.19(13-I-4)	-0.67(2)	-0.25(13-I-4)	-0.12(13-II-1)	0.12(12-II-1)
100754	0.22(12-I-4)	0.20(13-I-1)	-0.09(2)	1.37(13-I-1)	-0.51(13-I-1)	-0.09(13-I-4)
100762	0.11(12-I-2)	0.16(12-II-2)	-0.06(2)	-0.77(2)	-0.50(2)	0.25(12-II-3)
100763	0.22(12-I-2)	0.15(12-I-2)	-0.51(2)	0.16(2)	-0.65(2)	-0.09(12-I-1)
100764	-0.11(12-II-4)	0.16(13-I-4)	-0.06(2)	-0.71(2)	0.45(2)	-0.22(12-I-4)
100765	-0.23(12-II-2)	0.20(13-I-2)	-0.08(2)	1.36(13-I-2)	0.48(13-I-2)	-0.12(13-I-2)
100785	0.21(12-I-4)	0.15(13-I-4)	-0.50(2)	0.23(13-II-4)	0.70(2)	-0.09(12-I-1)
100786	0.21(12-I-4)	0.19(13-I-4)	-0.09(2)	1.35(13-I-4)	-0.50(13-I-4)	0.10(12-I-4)
100794	0.20(12-I-2)	0.21(12-I-2)	-0.54(2)	-0.55(2)	0.48(2)	0.16(12-II-3)
100795	0.19(12-I-4)	0.19(12-II-4)	-0.50(2)	-0.54(2)	-0.48(2)	-0.15(12-I-4)
100798	0.21(12-I-2)	0.15(12-I-2)	-0.06(2)	0.97(2)	0.24(13-I-3)	0.13(12-I-2)
100805	0.21(12-I-4)	0.16(13-I-4)	-0.06(2)	0.99(13-I-4)	-0.33(13-I-4)	0.11(12-II-4)
100816	0.20(12-I-2)	0.20(12-I-2)	-0.07(2)	0.68(2)	0.77(2)	0.24(12-II-3)
100817	0.19(12-I-4)	0.18(13-I-4)	-0.06(2)	0.67(13-I-4)	-0.69(2)	-0.19(12-I-4)
100818	-0.58(12-II-3)	0.70(12-II-3)	-0.04(2)	-0.34(12-II-3)	-0.72(2)	0.34(12-II-3)
100819	0.47(12-I-4)	0.59(13-I-4)	-0.04(2)	-0.27(13-I-4)	0.67(2)	-0.30(12-I-4)
100839	-0.61(12-II-3)	0.69(12-II-3)	-0.31(2)	1.10(2)	-1.21(2)	0.20(12-II-2)
100841	0.52(12-I-4)	0.59(13-I-4)	-0.30(2)	1.09(2)	1.20(2)	-0.19(12-I-4)
100852	-0.62(12-II-3)	0.68(12-II-3)	-0.04(2)	0.79(2)	-0.25(12-II-3)	0.31(12-II-3)
100853	0.53(12-I-4)	0.60(13-I-4)	-0.04(2)	0.79(2)	0.24(13-I-3)	-0.26(12-I-4)
101498	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101499	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101500	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101501	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101502	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101503	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101504	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101505	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101506	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101507	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101508	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101509	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101510	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101511	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101512	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101513	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101514	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101515	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101516	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101517	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101518	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101519	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101520	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101521	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101522	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101523	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101524	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101525	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
101526	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110097	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110098	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110099	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110101	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110107	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110109	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110113	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110115	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110123	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110124	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110137	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110139	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110145	-0.03(12-II-1)	0.05(13-I-1)	-0.01(2)	-0.39(13-I-1)	-0.29(12-II-1)	-0.08(12-I-1)
110146	0.03(12-I-1)	0.07(13-I-1)	-0.01(2)	-0.53(13-I-1)	0.28(12-I-1)	0.08(12-II-1)
110147	-0.03(12-II-1)	0.07(13-I-1)	-0.01(2)	-0.52(13-I-1)	-0.27(12-II-1)	-0.08(12-I-1)
110150	0.03(12-I-1)	0.05(13-I-1)	-0.01(2)	-0.37(13-I-1)	0.28(12-I-1)	0.08(12-II-1)
110154	-0.03(12-II-1)	0.04(13-I-1)	-0.01(2)	-0.32(13-I-1)	-0.29(12-II-1)	-0.07(12-I-1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
110158	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110162	0.03(12-I-1)	-0.05(13-II-1)	-0.01(2)	0.34(13-II-1)	0.30(12-I-1)	0.08(12-II-1)
110164	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
110165	0.03(12-I-1)	-0.04(13-II-2)	-0.01(2)	0.32(13-II-2)	0.28(12-I-1)	-0.08(12-I-1)
110168	-0.03(12-II-4)	-0.04(13-II-4)	-0.01(2)	0.31(13-II-4)	-0.30(12-II-4)	0.08(12-II-4)
110173	-0.03(12-II-1)	-0.05(13-II-2)	-0.01(2)	0.42(13-II-2)	-0.28(12-II-1)	-0.07(12-I-1)
110176	0.04(12-I-4)	-0.05(13-II-4)	-0.01(2)	0.42(13-II-4)	0.33(12-I-4)	0.08(12-II-1)
110189	0.03(12-I-2)	-0.07(13-II-2)	-0.01(2)	0.55(13-II-2)	0.30(12-I-2)	0.09(12-II-2)
110192	-0.20(12-II-1)	0.07(13-I-1)	-0.02(2)	0.32(13-II-1)	-0.67(12-II-1)	0.17(12-II-1)
110195	0.19(12-I-1)	0.09(13-I-1)	-0.03(2)	0.48(13-II-1)	0.64(12-I-1)	-0.17(12-I-1)
110198	0.19(12-I-1)	0.09(13-I-1)	-0.03(2)	0.47(13-II-1)	0.63(12-I-1)	0.17(12-II-1)
110201	0.20(12-I-1)	0.06(13-I-1)	-0.02(2)	0.30(13-II-1)	0.66(12-I-1)	-0.18(12-I-1)
110204	-0.04(12-II-4)	-0.07(13-II-4)	-0.01(2)	0.52(13-II-4)	-0.37(12-II-4)	-0.10(12-I-4)
110211	-0.18(12-II-1)	0.06(13-I-1)	-0.02(2)	0.30(13-II-1)	-0.61(12-II-1)	0.15(12-II-1)
110214	0.19(12-I-1)	0.06(13-I-1)	-0.02(2)	0.31(13-II-1)	0.64(12-I-1)	-0.16(12-I-4)
110217	0.18(12-I-1)	0.06(13-I-2)	-0.02(2)	0.27(13-II-2)	0.63(12-I-1)	-0.16(12-I-1)
110221	-0.19(12-II-1)	0.06(13-I-4)	-0.02(2)	0.27(13-II-4)	-0.66(12-II-1)	0.16(12-II-1)
110224	-0.04(12-II-2)	-0.08(13-II-2)	-0.01(2)	0.62(13-II-2)	-0.32(12-II-2)	0.08(12-II-1)
110228	-0.17(12-II-1)	-0.07(13-II-2)	-0.02(2)	0.33(13-II-2)	-0.57(12-II-1)	0.16(12-II-2)
110232	0.06(12-I-4)	-0.07(13-II-4)	-0.01(2)	0.55(13-II-4)	0.48(12-I-4)	-0.09(12-I-1)
110234	0.20(12-I-4)	-0.07(12-I-3)	-0.02(2)	0.34(13-II-4)	0.64(12-I-4)	-0.18(12-I-4)
110248	0.03(12-I-2)	0.05(13-II-2)	-0.01(2)	-0.45(13-I-2)	0.30(12-I-2)	0.08(12-I-2)
110251	0.17(12-I-2)	-0.09(13-II-2)	-0.03(2)	0.42(13-II-2)	0.61(12-I-2)	-0.17(12-I-2)
110256	-0.04(12-II-4)	0.06(13-I-4)	-0.01(2)	-0.58(13-I-4)	-0.37(12-I-4)	-0.06(12-I-1)
110258	-0.19(12-II-4)	-0.09(13-II-4)	-0.03(2)	0.43(13-II-4)	-0.69(12-II-4)	0.18(12-II-4)
110299	0.17(12-I-2)	-0.09(13-II-2)	-0.03(2)	0.48(13-II-2)	0.60(12-I-2)	0.13(12-II-1)
110308	-0.21(12-I-4)	-0.09(13-II-4)	-0.03(2)	0.45(13-II-3)	-0.71(12-II-4)	0.14(12-II-1)
110322	0.04(12-I-3)	0.05(13-I-4)	-0.01(2)	-0.46(13-I-4)	0.43(12-I-4)	0.09(12-II-4)
110325	-0.11(12-II-2)	0.10(13-II-2)	-0.01(2)	-0.60(13-II-2)	-0.66(12-II-2)	0.08(13-II-3)
110328	0.17(12-I-2)	0.08(13-I-2)	-0.02(2)	0.35(13-II-2)	0.62(12-I-2)	-0.15(12-I-1)
110339	-0.19(12-II-4)	0.11(12-II-4)	-0.02(2)	0.37(13-II-4)	-0.69(12-II-4)	0.14(12-II-1)
110370	-0.18(12-II-2)	0.12(13-II-2)	-0.02(2)	0.45(13-I-2)	0.58(12-I-2)	-0.17(12-I-2)
110373	0.08(12-I-4)	0.07(13-I-4)	-0.02(2)	0.31(13-II-4)	0.38(12-I-4)	0.12(12-II-1)
110382	-0.11(12-II-2)	0.10(13-I-3)	-0.01(2)	-0.65(13-I-3)	-0.69(12-II-2)	-0.13(12-II-2)
110433	-0.18(12-II-2)	0.12(13-I-2)	-0.02(2)	0.44(13-II-2)	0.67(12-I-2)	-0.16(12-I-2)
110554	-0.39(12-II-1)	0.16(13-I-4)	-0.07(2)	-0.92(2)	0.17(12-II-1)	-0.04(13-II-4)
110557	-0.39(12-II-1)	0.17(13-I-1)	-0.08(2)	-1.02(2)	-0.12(12-I-1)	0.06(12-II-2)
110560	0.39(12-I-1)	0.17(13-I-1)	-0.08(2)	-1.02(2)	0.12(12-II-1)	-0.07(12-I-4)
110563	0.39(12-I-1)	0.16(13-I-1)	-0.07(2)	-0.91(2)	-0.17(12-I-1)	0.04(13-II-2)
110576	0.37(12-I-1)	0.17(12-I-2)	-0.07(2)	-0.89(2)	-0.23(2)	-0.05(13-I-2)
110585	-0.37(12-II-1)	0.16(12-II-4)	-0.07(2)	-0.89(2)	0.25(2)	0.05(13-I-1)
110593	-0.39(12-II-1)	0.16(13-I-4)	-0.56(2)	-0.07(13-II-4)	0.47(2)	-0.27(12-II-1)
110594	-0.39(12-II-1)	0.17(13-I-1)	-0.65(2)	-0.07(13-II-1)	-0.09(13-II-1)	-0.24(12-II-1)
110595	0.39(12-I-1)	0.17(13-I-1)	-0.65(2)	-0.07(13-II-1)	0.09(13-II-1)	0.24(12-I-1)
110596	0.39(12-I-1)	0.16(13-I-1)	-0.56(2)	-0.07(13-II-2)	-0.48(2)	0.26(12-I-1)
110608	0.38(12-I-2)	0.19(13-I-2)	-0.08(2)	-0.93(2)	-0.36(2)	0.09(12-II-2)
110611	0.37(12-I-1)	0.17(12-I-2)	-0.56(2)	-0.22(2)	0.44(2)	0.26(12-I-1)
110617	-0.38(12-II-4)	0.17(13-I-1)	-0.08(2)	-0.93(2)	0.37(2)	-0.08(12-I-4)
110620	-0.37(12-II-4)	0.16(12-II-4)	-0.56(2)	-0.22(2)	-0.42(2)	-0.27(12-II-1)
110635	0.11(12-I-1)	0.16(13-I-4)	-0.06(2)	1.00(2)	0.15(2)	0.27(12-I-4)
110638	0.11(12-I-1)	0.17(13-I-1)	-0.07(2)	1.16(2)	-0.10(12-II-1)	-0.30(12-II-4)
110641	-0.11(12-II-1)	0.17(13-I-1)	-0.07(2)	1.17(2)	0.10(12-I-1)	0.30(12-I-2)
110644	-0.11(12-II-1)	0.16(13-I-1)	-0.06(2)	0.99(2)	-0.16(2)	-0.27(12-II-2)
110649	0.39(12-I-2)	0.20(13-I-2)	-0.08(2)	-0.94(2)	-0.36(2)	-0.05(12-I-2)
110652	-0.39(12-II-2)	0.20(13-I-2)	-0.65(2)	-0.07(13-I-2)	-0.11(13-II-2)	0.24(12-I-1)
110653	0.11(12-I-1)	0.15(13-I-1)	-0.06(2)	0.88(2)	0.48(2)	0.26(12-I-1)
110658	-0.38(12-II-4)	0.19(13-I-4)	-0.08(2)	-0.93(2)	0.37(2)	0.05(12-II-4)
110661	0.39(12-I-4)	0.18(13-I-1)	-0.65(2)	-0.06(13-I-4)	0.12(13-II-4)	-0.25(12-II-1)
110662	-0.11(12-II-1)	0.15(13-I-4)	-0.06(2)	0.88(2)	-0.50(2)	-0.26(12-II-1)
110683	0.37(12-I-2)	0.21(12-I-2)	-0.07(2)	-0.85(2)	-0.39(2)	0.06(13-I-2)
110686	-0.40(12-II-2)	0.20(13-I-2)	-0.65(2)	-0.09(13-I-2)	0.05(13-I-1)	0.25(12-I-2)
110687	-0.13(12-II-2)	0.19(13-I-2)	-0.07(2)	1.12(2)	0.39(2)	-0.29(12-II-1)
110691	-0.37(12-II-4)	0.20(12-II-4)	-0.07(2)	-0.83(2)	0.41(2)	-0.06(13-II-1)
110694	0.38(12-I-4)	0.19(13-I-4)	-0.65(2)	-0.09(13-I-4)	-0.05(13-II-1)	-0.25(12-II-4)
110695	0.13(12-I-4)	0.17(13-I-1)	-0.07(2)	1.12(2)	-0.40(2)	0.30(12-I-4)
110716	0.37(12-I-2)	0.21(12-I-2)	-0.58(2)	0.08(13-II-2)	-0.37(2)	0.28(12-I-2)
110718	-0.14(12-II-2)	0.19(13-I-2)	-0.07(2)	1.10(2)	0.42(2)	0.32(12-I-2)
110725	-0.37(12-II-4)	0.20(12-II-4)	-0.58(2)	0.10(13-I-4)	0.40(2)	-0.28(12-II-4)
110726	0.13(12-I-4)	0.19(13-I-4)	-0.07(2)	1.10(2)	-0.43(2)	-0.33(12-II-4)
110734	0.30(12-I-2)	0.34(12-I-2)	-0.09(2)	-0.61(2)	-0.56(2)	0.24(12-II-3)
110735	-0.30(12-II-4)	0.34(12-II-4)	-0.08(2)	-0.71(2)	0.62(2)	-0.21(13-I-3)
110738	-0.12(12-II-2)	0.17(13-I-3)	-0.06(2)	1.05(2)	0.25(13-II-3)	0.30(12-I-2)
110750	0.12(12-I-4)	0.16(13-I-4)	-0.06(2)	1.04(2)	-0.27(13-II-4)	-0.30(12-II-4)
110758	-0.31(12-II-2)	0.34(12-I-2)	-0.58(2)	-0.29(2)	0.21(2)	0.30(12-I-2)
110759	0.31(12-I-4)	0.34(12-II-4)	-0.60(2)	-0.34(2)	-0.26(2)	-0.28(12-II-4)
110762	-0.12(12-II-2)	0.17(12-I-2)	-0.07(2)	0.66(2)	0.69(2)	0.36(12-II-3)
110764	0.13(12-I-4)	0.20(13-I-4)	-0.07(2)	0.70(2)	-0.76(2)	-0.32(12-I-4)
110769	-0.68(12-II-3)	0.80(12-II-3)	-0.04(2)	-0.34(12-II-3)	-0.69(2)	0.34(12-II-3)
110793	0.58(12-I-4)	0.64(13-I-4)	-0.04(2)	-0.22(13-I-3)	0.66(2)	-0.28(13-I-3)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
110796	-0.69(12-II-3)	0.80(12-II-3)	-0.29(2)	1.06(2)	-1.14(2)	0.31(12-I-2)
110797	0.59(12-I-4)	0.64(13-I-4)	-0.30(2)	1.09(2)	1.19(2)	-0.31(12-II-4)
110818	-0.65(12-II-3)	0.73(12-II-3)	-0.04(2)	0.73(2)	-0.28(12-II-3)	0.51(12-II-3)
110819	0.53(13-I-4)	0.62(13-I-4)	-0.04(2)	0.79(2)	-0.19(13-II-3)	-0.45(12-II-4)
120003	0.34(12-I-1)	-0.58(13-II-4)	-0.07(2)	-0.34(13-I-4)	0.31(12-II-3)	0.24(13-II-4)
120004	0.33(12-I-1)	-0.40(13-II-4)	-0.16(2)	-0.42(13-II-3)	0.31(12-II-3)	0.13(12-II-4)
120005	0.35(12-I-1)	-0.41(13-II-4)	-0.22(2)	-1.13(13-II-3)	0.41(12-II-3)	-0.17(12-I-1)
120006	0.34(12-I-1)	-0.38(13-II-4)	-0.22(2)	-0.46(2)	0.39(12-II-3)	-0.16(12-I-1)
120007	0.33(12-I-1)	-0.43(13-II-4)	-0.23(2)	-0.43(13-II-4)	0.38(12-II-3)	-0.18(12-I-1)
120008	0.33(12-I-1)	-0.42(13-II-1)	-0.23(2)	-0.45(13-II-1)	0.39(12-II-3)	0.14(12-II-1)
120009	0.34(12-I-1)	-0.39(13-II-2)	-0.22(2)	-0.46(13-I-2)	0.39(12-II-3)	-0.18(12-I-1)
120010	0.34(12-I-1)	-0.39(13-II-2)	-0.22(2)	-0.92(13-II-3)	0.39(12-II-3)	-0.16(12-I-1)
120011	0.34(12-I-1)	-0.34(13-II-2)	-0.21(2)	-0.63(13-II-2)	-0.40(12-I-3)	-0.62(13-II-2)
120012	0.35(12-I-1)	-1.63(13-II-2)	-0.10(2)	-1.32(13-I-2)	0.43(12-II-3)	-0.65(13-II-2)
120013	-0.39(12-II-1)	-0.58(13-II-4)	-0.07(2)	-0.03(13-I-1)	0.15(2)	0.17(13-II-4)
120014	0.38(12-I-1)	-0.43(13-II-4)	-0.16(2)	-0.11(13-I-4)	0.14(12-I-1)	0.13(12-II-4)
120015	0.41(12-I-1)	-0.42(13-II-4)	-0.22(2)	-0.12(13-I-1)	0.12(12-I-1)	0.16(12-II-4)
120016	0.40(12-I-1)	-0.41(13-II-4)	-0.23(2)	-0.12(13-I-1)	0.13(12-I-1)	0.15(12-II-4)
120017	0.38(12-I-1)	-0.45(13-II-4)	-0.23(2)	-0.13(13-I-1)	0.18(12-I-1)	0.15(12-II-1)
120018	0.37(12-I-1)	-0.44(13-II-1)	-0.23(2)	-0.13(13-I-1)	-0.14(12-II-1)	0.13(12-II-1)
120019	0.39(12-I-1)	-0.42(13-II-2)	-0.23(2)	-0.12(13-I-1)	0.09(12-I-1)	0.14(12-II-1)
120020	0.38(12-I-1)	-0.41(13-II-2)	-0.23(2)	-0.10(13-I-1)	0.12(12-I-1)	0.14(12-II-2)
120021	0.38(12-I-1)	-0.36(13-II-2)	-0.21(2)	0.11(13-II-2)	0.14(12-I-1)	-0.56(13-II-2)
120022	0.39(12-I-1)	-1.64(13-II-2)	-0.10(2)	-0.16(13-I-2)	-0.08(12-II-1)	-0.38(13-II-2)
120023	-0.45(12-II-1)	-0.58(13-II-4)	-0.06(2)	-0.03(13-I-1)	0.15(2)	0.19(13-II-4)
120024	0.44(12-I-1)	-0.42(13-II-4)	-0.16(2)	-0.11(13-I-4)	0.14(12-I-4)	0.10(12-II-3)
120025	0.46(12-I-1)	-0.41(13-II-4)	-0.22(2)	-0.13(13-I-1)	0.13(12-I-4)	-0.12(13-II-4)
120026	0.45(12-I-1)	-0.40(13-II-4)	-0.23(2)	-0.13(13-I-1)	0.14(12-I-1)	0.12(13-I-4)
120027	0.44(12-I-1)	-0.44(13-II-4)	-0.23(2)	-0.14(13-I-1)	0.19(12-I-1)	0.11(12-I-4)
120028	0.43(12-I-1)	-0.43(13-II-2)	-0.23(2)	-0.14(13-I-1)	-0.16(12-II-1)	-0.09(12-II-3)
120029	0.45(12-I-1)	-0.41(13-II-2)	-0.23(2)	-0.12(13-I-1)	0.09(12-I-1)	-0.10(12-II-1)
120030	0.44(12-I-1)	-0.40(13-II-2)	-0.23(2)	-0.11(13-I-1)	0.13(12-I-1)	0.10(12-II-2)
120031	0.43(12-I-1)	-0.35(13-II-2)	-0.21(2)	-0.12(13-I-2)	0.16(12-I-1)	-0.55(13-II-2)
120032	0.45(12-I-1)	-1.64(13-II-2)	-0.10(2)	0.15(13-II-2)	-0.09(12-II-2)	-0.41(13-II-2)
120033	-0.43(12-II-4)	-0.58(13-II-4)	-0.06(2)	-0.03(13-I-1)	0.15(2)	0.20(13-II-4)
120034	0.42(12-I-4)	-0.41(13-II-4)	-0.16(2)	-0.16(13-I-4)	0.16(12-I-4)	0.10(13-II-4)
120035	0.45(12-I-1)	-0.40(13-II-4)	-0.22(2)	-0.17(13-I-1)	0.14(12-I-4)	0.10(12-I-1)
120036	0.43(12-I-1)	-0.39(13-II-4)	-0.23(2)	-0.17(13-I-1)	0.15(12-I-4)	-0.11(13-II-4)
120037	0.42(12-I-1)	-0.43(13-II-4)	-0.23(2)	-0.18(13-I-1)	0.20(12-I-4)	0.10(12-II-3)
120038	0.41(12-I-1)	-0.42(13-II-2)	-0.23(2)	-0.19(13-I-1)	-0.16(12-II-4)	-0.09(12-I-3)
120039	0.43(12-I-1)	-0.40(13-II-2)	-0.23(2)	-0.17(13-I-2)	-0.10(12-II-2)	0.11(12-I-3)
120040	0.42(12-I-2)	-0.38(13-II-2)	-0.22(2)	-0.15(13-I-2)	0.13(12-I-2)	-0.09(12-I-3)
120041	0.42(12-I-2)	-0.34(13-II-2)	-0.21(2)	-0.16(13-I-2)	0.17(12-I-2)	-0.53(13-II-2)
120042	0.43(12-I-2)	-1.64(13-II-2)	-0.10(2)	-0.15(13-I-2)	-0.10(12-II-2)	-0.41(13-II-2)
120043	-0.44(12-II-4)	-0.58(13-II-4)	-0.06(2)	-0.03(12-II-3)	0.15(2)	0.21(13-II-4)
120044	0.43(12-I-4)	-0.40(13-II-4)	-0.16(2)	0.14(13-II-4)	0.16(12-I-4)	0.10(13-II-4)
120045	0.46(12-I-4)	-0.39(13-II-4)	-0.22(2)	0.14(13-II-1)	0.14(12-I-4)	-0.11(12-II-3)
120046	0.44(12-I-4)	-0.38(13-II-4)	-0.23(2)	0.14(13-II-4)	0.16(12-I-4)	0.12(12-II-3)
120047	0.42(12-I-4)	-0.42(13-II-4)	-0.23(2)	0.15(13-II-4)	0.20(12-I-4)	0.11(12-II-3)
120048	0.41(12-I-2)	-0.41(13-II-2)	-0.23(2)	0.15(13-II-2)	-0.16(12-II-4)	0.11(12-II-3)
120049	0.44(12-I-2)	-0.39(13-II-2)	-0.23(2)	0.14(13-II-2)	-0.10(12-II-2)	-0.12(12-II-3)
120050	0.43(12-I-2)	-0.37(13-II-2)	-0.22(2)	0.13(13-II-2)	0.13(12-I-2)	0.12(12-II-3)
120051	0.43(12-I-2)	-0.34(13-II-2)	-0.21(2)	0.14(13-II-2)	0.18(12-I-2)	-0.52(13-II-2)
120052	0.44(12-I-2)	-1.64(13-II-2)	-0.10(2)	-0.16(13-I-2)	-0.10(12-II-2)	-0.42(13-II-2)
120053	-0.45(12-II-3)	-0.58(13-II-4)	-0.06(2)	-0.03(12-II-3)	0.15(2)	0.18(13-II-4)
120054	0.44(12-I-3)	-0.42(13-II-4)	-0.16(2)	0.09(13-II-4)	0.15(12-I-3)	0.13(12-II-4)
120055	0.47(12-I-3)	-0.40(13-II-4)	-0.22(2)	0.08(13-II-4)	0.13(12-I-4)	0.10(12-II-4)
120056	0.46(12-I-3)	-0.40(13-II-4)	-0.23(2)	0.08(13-II-4)	0.14(12-I-3)	0.12(13-I-4)
120057	0.44(12-I-3)	-0.44(13-II-4)	-0.23(2)	0.09(13-II-4)	0.20(12-I-3)	-0.10(13-II-4)
120058	0.43(12-I-3)	-0.43(13-II-2)	-0.23(2)	0.09(13-II-2)	-0.16(12-II-3)	0.10(12-II-3)
120059	0.45(12-I-3)	-0.42(13-II-2)	-0.23(2)	0.08(13-II-2)	0.10(12-I-3)	0.09(13-II-2)
120060	0.44(12-I-3)	-0.39(13-II-2)	-0.22(2)	0.07(13-I-2)	0.13(12-I-3)	0.10(12-II-3)
120061	0.44(12-I-3)	-0.36(13-II-2)	-0.21(2)	0.10(13-II-2)	0.16(12-I-3)	-0.56(13-II-2)
120062	0.45(12-I-3)	-1.64(13-II-2)	-0.10(2)	-0.16(13-I-2)	-0.10(12-II-3)	-0.41(13-II-2)
120063	-0.45(12-II-3)	-0.57(13-II-4)	-0.07(2)	-0.03(12-II-3)	0.15(2)	0.21(12-II-3)
120064	0.44(12-I-3)	-0.41(13-II-4)	-0.16(2)	-0.11(13-I-4)	0.14(12-I-3)	0.16(12-II-3)
120065	0.47(12-I-3)	-0.39(13-II-4)	-0.22(2)	-0.10(13-I-4)	0.12(12-I-3)	-0.11(12-I-4)
120066	0.46(12-I-3)	-0.39(13-II-4)	-0.23(2)	-0.11(13-I-4)	0.13(12-I-3)	0.12(13-I-4)
120067	0.44(12-I-3)	-0.43(13-II-4)	-0.23(2)	-0.12(13-I-3)	0.19(12-I-3)	0.10(13-I-2)
120068	0.43(12-I-3)	-0.42(13-II-2)	-0.23(2)	-0.12(13-I-2)	-0.15(12-II-3)	-0.09(12-I-3)
120069	0.45(12-I-3)	-0.41(13-II-2)	-0.23(2)	-0.11(13-I-2)	0.09(12-I-3)	-0.09(13-I-2)
120070	0.44(12-I-3)	-0.38(13-II-2)	-0.23(2)	-0.10(13-I-2)	0.12(12-I-3)	0.09(12-II-3)
120071	0.44(12-I-3)	-0.35(13-II-2)	-0.21(2)	-0.11(13-I-2)	0.15(12-I-3)	-0.55(13-II-2)
120072	0.45(12-I-3)	-1.64(13-II-2)	-0.10(2)	0.16(13-II-2)	-0.09(12-II-3)	-0.41(13-II-2)
120073	-0.41(12-II-3)	-0.57(13-II-4)	-0.06(2)	0.10(12-II-3)	0.14(2)	0.79(12-II-3)
120074	0.40(12-I-3)	-0.40(13-II-4)	-0.14(2)	-0.14(13-I-4)	0.15(12-I-3)	0.58(12-II-3)
120075	0.43(12-I-3)	0.38(13-I-4)	-0.20(2)	0.14(13-I-4)	0.13(12-I-3)	0.67(12-II-3)
120076	0.41(12-I-3)	0.38(13-I-4)	-0.21(2)	0.14(13-II-4)	0.15(12-I-3)	-0.66(12-I-3)
120077	0.40(12-I-3)	0.42(13-I-4)	-0.21(2)	-0.16(13-I-3)	0.19(12-I-3)	-0.62(12-I-3)

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
120078	0.39(12-I-3)	0.40(13-I-3)	-0.21(2)	-0.16(13-I-3)	-0.17(12-II-3)	-0.62(12-I-3)
120079	0.41(12-I-3)	0.39(13-I-2)	-0.21(2)	0.14(13-II-2)	-0.11(12-II-3)	-0.67(12-I-3)
120080	0.40(12-I-3)	0.37(13-I-2)	-0.21(2)	0.13(13-II-2)	0.13(12-I-3)	-0.67(12-I-3)
120081	0.40(12-I-3)	-0.34(13-II-2)	-0.19(2)	0.15(13-II-2)	0.16(12-I-3)	-0.71(12-I-3)
120082	0.41(12-I-3)	-1.64(13-II-2)	-0.09(2)	0.18(13-II-2)	-0.12(12-II-3)	-1.02(12-I-3)
120083	2.04(12-I-3)	-0.57(13-II-4)	-0.03(2)	0.12(12-II-3)	0.14(12-I-3)	0.74(12-II-3)
120084	2.04(12-I-3)	0.41(13-I-4)	-0.07(2)	0.09(13-II-4)	0.14(12-I-3)	0.48(12-II-3)
120085	2.04(12-I-3)	0.39(13-I-4)	-0.10(2)	0.09(13-II-4)	0.20(12-I-3)	-0.49(12-I-3)
120086	2.05(12-I-3)	0.39(13-I-4)	-0.10(2)	0.10(13-II-3)	0.20(12-I-3)	-0.48(12-I-3)
120087	2.05(12-I-3)	0.43(13-I-4)	-0.10(2)	0.11(13-II-3)	0.20(12-I-3)	-0.49(12-I-3)
120088	2.05(12-I-3)	0.42(13-I-3)	-0.10(2)	0.10(13-II-3)	0.20(12-I-3)	-0.49(12-I-3)
120089	2.05(12-I-3)	0.41(13-I-2)	-0.10(2)	0.10(13-II-2)	0.20(12-I-3)	-0.48(12-I-3)
120090	2.05(12-I-3)	0.38(13-I-2)	-0.10(2)	0.09(13-II-2)	0.20(12-I-3)	-0.49(12-I-3)
120091	2.05(12-I-3)	0.34(13-I-2)	-0.09(2)	0.11(13-II-2)	-0.20(12-II-3)	-0.83(13-II-2)
120092	2.05(12-I-3)	-1.63(13-II-2)	-0.04(2)	0.18(13-II-2)	-0.21(12-II-3)	-1.12(12-I-3)
120938	0.34(12-I-1)	-0.41(13-II-4)	-0.23(2)	-0.37(13-II-3)	0.10(13-II-1)	-0.14(13-II-2)
120940	0.35(12-I-1)	-0.42(13-II-1)	-0.25(2)	-0.42(13-II-3)	0.07(13-II-1)	-0.25(13-II-4)
120942	0.34(12-I-1)	-0.42(13-II-4)	-0.26(2)	-0.29(2)	0.06(13-II-1)	-0.17(13-II-4)
120944	0.34(12-I-1)	-0.45(13-II-1)	-0.26(2)	-0.30(2)	0.06(13-II-1)	-0.17(13-I-4)
120946	0.33(12-I-1)	-0.42(13-II-2)	-0.25(2)	-0.30(13-I-2)	0.05(13-II-1)	-0.17(13-I-4)
120948	0.34(12-I-1)	-0.41(13-II-2)	-0.25(2)	-0.31(13-I-2)	0.06(12-II-4)	-0.19(13-I-2)
120950	0.33(12-I-1)	-0.34(13-II-2)	-0.25(2)	-0.41(13-II-3)	0.04(13-II-2)	-0.29(13-I-2)
120952	0.35(12-I-1)	-0.95(13-II-2)	-0.17(2)	-0.48(13-I-2)	-0.13(13-II-2)	-1.70(13-II-2)
120972	-0.34(12-II-1)	-0.58(13-II-4)	-0.09(2)	0.02(13-II-4)	0.17(2)	0.35(12-II-4)
120973	0.34(12-I-1)	-0.41(13-II-4)	-0.21(2)	0.07(13-II-4)	0.19(12-I-1)	-0.36(12-II-4)
120974	0.38(12-I-1)	-0.41(13-II-4)	-0.29(2)	-0.07(13-I-4)	0.19(12-I-1)	0.34(12-I-4)
120975	0.37(12-I-1)	-0.39(13-II-4)	-0.30(2)	-0.08(13-I-4)	0.17(12-I-1)	-0.34(12-II-4)
120976	0.37(12-I-1)	-0.44(13-II-4)	-0.30(2)	0.09(13-II-1)	0.22(12-I-1)	0.34(12-I-4)
120977	0.35(12-I-1)	-0.43(13-II-1)	-0.30(2)	0.09(13-II-1)	0.20(12-I-1)	-0.34(12-II-4)
120978	0.37(12-I-1)	-0.40(13-II-2)	-0.30(2)	-0.08(13-I-2)	0.16(12-I-1)	-0.33(12-II-4)
120979	0.36(12-I-1)	-0.40(13-II-2)	-0.30(2)	-0.07(13-I-2)	0.16(12-I-1)	-0.33(12-II-4)
120980	0.36(12-I-1)	-0.35(13-II-2)	-0.27(2)	0.07(13-I-2)	-0.22(12-II-1)	0.36(12-I-2)
120981	0.35(12-I-1)	-1.63(13-II-2)	-0.13(2)	-0.01(13-I-2)	-0.12(12-I-3)	-0.35(12-II-2)
121006	0.40(12-I-1)	-0.43(13-II-4)	-0.27(2)	0.12(13-II-1)	0.09(13-II-1)	0.13(13-I-2)
121008	0.41(12-I-1)	-0.42(13-II-1)	-0.29(2)	-0.13(13-I-1)	0.08(13-II-1)	0.27(13-I-4)
121010	0.39(12-I-1)	-0.45(13-II-4)	-0.29(2)	-0.13(13-I-1)	0.07(13-II-1)	0.18(13-I-4)
121012	0.39(12-I-1)	-0.46(13-II-1)	-0.29(2)	-0.14(13-I-1)	0.08(13-II-1)	0.18(13-II-4)
121014	0.39(12-I-1)	-0.44(13-II-2)	-0.29(2)	-0.13(13-I-1)	0.09(13-II-1)	0.18(13-II-4)
121016	0.40(12-I-1)	-0.43(13-II-2)	-0.29(2)	-0.12(13-I-1)	0.08(13-II-1)	0.20(13-II-2)
121018	0.38(12-I-1)	-0.35(13-II-2)	-0.29(2)	-0.11(13-I-1)	-0.08(13-I-1)	-0.31(13-I-2)
121020	0.39(12-I-1)	-1.00(13-II-2)	-0.20(2)	0.12(13-II-2)	-0.11(2)	-1.78(13-II-2)
121040	-0.44(12-II-1)	-0.58(13-II-4)	-0.08(2)	0.01(13-I-4)	0.20(2)	-0.19(12-I-4)
121041	0.43(12-I-1)	-0.43(13-II-4)	-0.20(2)	0.07(13-I-4)	0.26(12-I-1)	-0.19(12-I-4)
121042	0.48(12-I-1)	-0.42(13-II-4)	-0.28(2)	0.06(13-I-4)	0.26(12-I-4)	-0.17(12-I-2)
121043	0.46(12-I-1)	-0.40(13-II-4)	-0.29(2)	0.06(13-I-4)	0.26(12-I-1)	-0.17(12-II-1)
121044	0.45(12-I-1)	-0.45(13-II-4)	-0.29(2)	0.08(13-I-4)	0.30(12-I-1)	-0.17(12-II-3)
121045	0.44(12-I-1)	-0.44(13-II-1)	-0.29(2)	0.08(13-I-1)	0.28(12-I-1)	-0.17(12-II-1)
121046	0.46(12-I-1)	-0.42(13-II-2)	-0.29(2)	0.06(13-I-2)	0.24(12-I-1)	-0.17(12-I-3)
121047	0.45(12-I-1)	-0.40(13-II-2)	-0.29(2)	0.06(13-I-2)	0.25(12-I-1)	0.16(12-I-1)
121048	0.44(12-I-1)	-0.36(13-II-2)	-0.26(2)	0.06(13-I-2)	-0.28(12-II-1)	0.24(13-II-2)
121049	0.45(12-I-1)	-1.64(13-II-2)	-0.13(2)	0.01(12-II-2)	-0.15(12-II-2)	0.19(12-II-2)
121074	0.45(12-I-1)	-0.42(13-II-4)	-0.27(2)	-0.13(13-I-1)	0.10(13-II-1)	0.13(13-II-2)
121076	0.47(12-I-1)	-0.41(13-II-1)	-0.29(2)	-0.13(13-I-1)	0.08(13-II-1)	0.26(13-I-4)
121078	0.45(12-I-1)	-0.43(13-II-4)	-0.29(2)	-0.13(13-I-1)	0.08(13-II-1)	-0.18(13-II-4)
121080	0.45(12-I-1)	-0.45(13-II-1)	-0.29(2)	-0.14(13-I-1)	0.08(13-II-1)	0.17(13-II-4)
121082	0.44(12-I-1)	-0.44(13-II-2)	-0.29(2)	-0.13(13-I-1)	0.06(13-II-1)	0.17(13-II-4)
121084	0.45(12-I-1)	-0.42(13-II-2)	-0.29(2)	-0.12(13-I-1)	0.07(13-II-1)	0.19(13-II-2)
121086	0.44(12-I-1)	-0.34(13-II-2)	-0.29(2)	-0.10(13-II-2)	-0.08(12-II-1)	-0.32(13-I-2)
121088	0.45(12-I-1)	-1.00(13-II-2)	-0.19(2)	-0.12(13-I-2)	-0.11(2)	-1.78(13-II-2)
121108	-0.46(12-II-1)	-0.58(13-II-4)	-0.08(2)	0.01(12-I-3)	0.20(2)	-0.18(12-II-3)
121109	0.46(12-I-1)	-0.41(13-II-4)	-0.20(2)	0.05(13-II-4)	0.29(12-I-4)	-0.18(12-II-3)
121110	0.50(12-I-1)	-0.40(13-II-4)	-0.28(2)	0.06(13-II-4)	0.29(12-I-4)	-0.16(12-II-3)
121111	0.48(12-I-1)	-0.39(13-II-4)	-0.29(2)	0.06(13-II-4)	0.27(12-I-4)	-0.15(12-II-3)
121112	0.47(12-I-1)	-0.43(13-II-4)	-0.29(2)	0.06(13-II-4)	0.30(12-I-1)	-0.16(12-II-1)
121113	0.46(12-I-1)	-0.42(13-II-2)	-0.29(2)	0.06(13-II-2)	0.27(12-I-1)	-0.15(12-II-1)
121114	0.48(12-I-1)	-0.40(13-II-2)	-0.29(2)	0.06(13-II-2)	0.24(12-I-1)	-0.16(12-II-3)
121115	0.47(12-I-1)	-0.39(13-II-2)	-0.29(2)	0.05(13-II-2)	0.26(12-I-2)	-0.15(12-II-3)
121116	0.46(12-I-1)	-0.34(13-II-2)	-0.26(2)	0.05(13-II-2)	-0.31(12-II-2)	0.26(13-II-2)
121117	0.46(12-I-1)	-1.64(13-II-2)	-0.13(2)	0.01(12-I-3)	-0.16(12-II-2)	0.21(13-II-2)
121146	0.44(12-I-1)	-0.41(13-II-4)	-0.26(2)	-0.15(13-I-4)	0.10(12-I-4)	0.13(13-II-2)
121148	0.45(12-I-1)	-0.39(13-II-4)	-0.29(2)	-0.16(13-I-1)	0.07(13-I-4)	0.24(13-I-4)
121150	0.43(12-I-1)	-0.42(13-II-4)	-0.29(2)	-0.17(13-I-1)	0.07(12-I-4)	0.17(13-I-4)
121152	0.43(12-I-1)	-0.43(13-II-1)	-0.29(2)	-0.17(13-I-1)	0.07(13-II-4)	0.17(13-II-4)
121154	0.42(12-I-1)	-0.43(13-II-2)	-0.29(2)	-0.17(13-I-1)	0.07(13-II-1)	0.17(13-II-4)
121156	0.44(12-I-1)	-0.41(13-II-2)	-0.29(2)	-0.15(13-I-2)	0.07(13-II-2)	0.18(13-II-2)
121158	0.42(12-I-2)	-0.33(13-I-2)	-0.28(2)	-0.14(13-II-2)	-0.08(12-I-1)	-0.31(13-I-2)
121160	0.43(12-I-2)	-0.99(13-II-2)	-0.19(2)	-0.13(13-I-2)	-0.11(2)	-1.79(13-II-2)
121190	-0.46(12-II-4)	-0.58(13-II-4)	-0.08(2)	-0.01(12-II-3)	0.20(2)	-0.26(12-I-3)
121191	0.47(12-I-4)	-0.41(13-II-4)	-0.20(2)	-0.05(13-II-4)	0.31(12-I-4)	-0.26(12-I-3)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
121192	0.50(12-I-4)	-0.39(13-II-4)	-0.28(2)	-0.06(13-II-4)	0.30(12-I-4)	-0.24(12-II-3)
121193	0.48(12-I-4)	-0.39(13-II-4)	-0.29(2)	-0.05(13-II-4)	0.28(12-I-4)	-0.24(12-II-1)
121194	0.46(12-I-4)	-0.43(13-II-4)	-0.29(2)	-0.06(13-II-4)	0.30(12-I-4)	-0.24(12-II-1)
121195	0.45(12-I-2)	-0.42(13-II-2)	-0.29(2)	-0.05(13-II-2)	0.26(12-I-2)	-0.23(12-II-1)
121196	0.48(12-I-2)	-0.40(13-II-2)	-0.29(2)	-0.06(13-II-2)	0.24(12-I-2)	-0.24(12-II-1)
121197	0.47(12-I-2)	-0.38(13-II-2)	-0.28(2)	-0.05(13-II-2)	0.27(12-I-2)	-0.23(12-II-3)
121198	0.47(12-I-2)	-0.34(13-II-2)	-0.26(2)	-0.04(13-I-2)	-0.33(12-II-2)	0.25(12-I-3)
121199	0.47(12-I-2)	-1.64(13-II-2)	-0.12(2)	-0.01(12-I-3)	-0.17(12-II-2)	0.23(12-I-3)
121218	0.45(12-I-4)	-0.39(13-II-4)	-0.26(2)	0.14(13-II-4)	0.10(12-I-4)	0.12(13-I-2)
121220	0.46(12-I-4)	-0.38(13-II-4)	-0.29(2)	0.13(13-II-1)	0.06(13-II-4)	0.24(13-I-4)
121222	0.43(12-I-4)	-0.41(13-II-4)	-0.29(2)	0.14(13-II-4)	0.07(12-I-4)	0.17(13-I-4)
121224	0.43(12-I-2)	-0.41(13-II-3)	-0.29(2)	0.14(13-II-1)	0.06(13-II-3)	0.17(13-II-4)
121226	0.43(12-I-2)	-0.41(13-II-2)	-0.29(2)	0.14(13-II-2)	0.07(13-II-2)	0.17(13-II-4)
121228	0.45(12-I-2)	-0.40(13-II-2)	-0.29(2)	0.13(13-II-2)	0.06(13-II-2)	0.18(13-II-2)
121230	0.43(12-I-2)	-0.32(13-I-2)	-0.29(2)	0.11(13-I-2)	-0.07(12-II-2)	-0.30(13-I-2)
121232	0.44(12-I-2)	-0.99(13-II-2)	-0.19(2)	0.13(13-II-2)	-0.11(2)	-1.80(13-II-2)
121252	-0.45(12-I-4)	-0.58(13-II-4)	-0.08(2)	0.01(12-II-1)	0.20(2)	0.18(12-II-3)
121253	0.45(12-I-4)	-0.41(13-II-4)	-0.20(2)	0.06(13-II-4)	0.30(12-I-4)	-0.18(12-II-1)
121254	0.48(12-I-4)	-0.39(13-II-4)	-0.28(2)	0.06(13-II-4)	0.29(12-I-4)	-0.17(12-II-1)
121255	0.46(12-I-4)	-0.39(13-II-4)	-0.29(2)	0.06(13-II-4)	0.27(12-I-4)	-0.18(12-II-1)
121256	0.44(12-I-3)	-0.43(13-II-4)	-0.29(2)	0.07(13-II-4)	0.29(12-I-4)	-0.17(12-II-1)
121257	0.43(12-I-3)	-0.41(13-II-2)	-0.29(2)	0.07(13-II-2)	0.26(12-I-3)	-0.17(12-II-1)
121258	0.46(12-I-2)	-0.40(13-II-2)	-0.29(2)	0.06(13-II-2)	0.23(12-I-2)	-0.18(12-II-1)
121259	0.45(12-I-2)	-0.38(13-II-2)	-0.29(2)	0.05(13-II-2)	0.26(12-I-2)	-0.17(12-II-1)
121260	0.45(12-I-2)	-0.34(13-II-2)	-0.26(2)	0.05(13-II-2)	-0.32(12-II-2)	0.26(13-II-2)
121261	0.45(12-I-2)	-1.64(13-II-2)	-0.13(2)	-0.01(12-II-1)	-0.16(12-II-2)	0.22(13-II-2)
121286	0.46(12-I-3)	-0.41(13-II-4)	-0.26(2)	0.09(13-II-4)	0.09(12-I-3)	0.12(13-I-2)
121288	0.47(12-I-3)	-0.40(13-II-4)	-0.29(2)	0.08(13-II-4)	0.07(13-I-4)	0.25(13-I-4)
121290	0.45(12-I-3)	-0.43(13-II-4)	-0.29(2)	0.09(13-II-4)	0.06(12-I-3)	0.17(13-I-4)
121292	0.45(12-I-3)	-0.45(13-II-3)	-0.29(2)	0.09(13-II-3)	0.07(13-II-4)	0.18(13-II-4)
121294	0.44(12-I-3)	-0.44(13-II-2)	-0.29(2)	0.09(13-II-2)	0.07(13-I-3)	0.17(13-II-4)
121296	0.46(12-I-3)	-0.42(13-II-2)	-0.29(2)	-0.08(13-I-2)	0.07(13-II-2)	0.19(13-II-2)
121298	0.44(12-I-3)	-0.33(13-I-2)	-0.28(2)	-0.08(13-II-2)	-0.08(12-II-3)	-0.31(13-I-2)
121300	0.45(12-I-3)	-1.00(13-II-2)	-0.19(2)	0.11(13-II-2)	-0.11(2)	-1.77(13-II-2)
121300	-0.48(12-II-3)	-0.58(13-II-4)	-0.08(2)	-0.01(13-II-4)	0.20(2)	0.19(12-II-1)
121331	0.47(12-I-3)	-0.42(13-II-4)	-0.20(2)	-0.06(13-II-4)	0.28(12-I-4)	-0.19(12-I-1)
121332	0.52(12-I-3)	-0.40(13-II-4)	-0.28(2)	-0.06(13-II-4)	0.28(12-I-4)	-0.20(12-I-1)
121333	0.50(12-I-3)	-0.40(13-II-4)	-0.29(2)	-0.06(13-II-4)	0.27(12-I-3)	-0.20(12-I-1)
121334	0.49(12-I-3)	-0.44(13-II-4)	-0.29(2)	-0.07(13-II-4)	0.31(12-I-3)	-0.19(12-I-1)
121335	0.48(12-I-3)	-0.43(13-II-2)	-0.29(2)	-0.07(13-II-2)	0.29(12-I-3)	-0.18(12-I-1)
121336	0.50(12-I-3)	-0.41(13-II-2)	-0.29(2)	-0.06(13-II-2)	0.25(12-I-3)	-0.20(12-I-1)
121337	0.49(12-I-3)	-0.39(13-II-2)	-0.29(2)	-0.05(13-II-2)	0.26(12-I-3)	-0.19(12-I-1)
121338	0.48(12-I-3)	-0.35(13-II-2)	-0.26(2)	-0.06(13-I-2)	-0.30(12-II-2)	0.23(13-II-2)
121339	0.48(12-I-3)	-1.64(13-II-2)	-0.13(2)	-0.01(12-I-2)	-0.15(12-II-2)	0.18(13-II-2)
121354	0.46(12-I-3)	-0.41(13-II-4)	-0.26(2)	-0.10(13-I-4)	0.09(13-II-3)	0.12(13-II-4)
121356	0.47(12-I-3)	-0.39(13-II-4)	-0.29(2)	-0.10(13-I-4)	0.07(13-II-3)	0.24(13-I-4)
121358	0.45(12-I-3)	-0.43(13-II-4)	-0.29(2)	-0.11(13-I-3)	0.08(13-II-3)	-0.17(13-II-4)
121360	0.45(12-I-3)	-0.44(13-II-3)	-0.29(2)	-0.12(13-I-3)	0.08(13-II-3)	0.17(13-II-4)
121362	0.45(12-I-3)	-0.43(13-II-2)	-0.29(2)	-0.11(13-I-3)	0.07(13-II-3)	0.17(13-II-4)
121364	0.46(12-I-3)	-0.41(13-II-2)	-0.29(2)	-0.10(13-I-2)	0.06(13-II-2)	0.18(13-II-2)
121366	0.44(12-I-3)	-0.33(13-I-2)	-0.29(2)	-0.09(13-II-2)	-0.07(12-II-3)	-0.31(13-I-2)
121368	0.45(12-I-3)	-1.00(13-II-2)	-0.19(2)	-0.12(13-I-2)	-0.11(2)	-1.77(13-II-2)
121398	-0.39(12-II-3)	-0.57(13-II-4)	-0.08(2)	0.02(12-II-3)	0.19(2)	-0.31(12-II-3)
121399	0.39(12-I-3)	-0.40(13-II-4)	-0.20(2)	0.06(13-II-4)	0.25(12-I-3)	-0.35(12-II-3)
121400	0.43(12-I-3)	0.38(13-I-4)	-0.28(2)	0.07(13-II-4)	0.24(12-I-3)	-0.37(12-II-3)
121401	0.42(12-I-3)	0.38(13-I-4)	-0.29(2)	0.07(13-II-4)	0.25(12-I-3)	-0.37(12-II-3)
121402	0.41(12-I-3)	0.42(13-I-4)	-0.29(2)	0.08(13-II-4)	0.28(12-I-3)	-0.37(12-II-3)
121403	0.40(12-I-3)	0.41(13-I-2)	-0.29(2)	0.08(13-II-3)	0.26(12-I-3)	-0.35(12-II-3)
121404	0.42(12-I-3)	0.40(13-I-2)	-0.29(2)	0.07(13-II-2)	0.22(12-I-3)	-0.37(12-II-3)
121405	0.41(12-I-3)	0.37(13-I-2)	-0.29(2)	0.06(13-II-2)	0.23(12-I-3)	0.36(12-I-3)
121406	0.40(12-I-3)	-0.34(13-II-2)	-0.26(2)	0.06(13-II-2)	-0.26(12-II-3)	0.34(12-I-3)
121407	0.40(12-I-3)	-1.64(13-II-2)	-0.13(2)	0.01(12-I-3)	-0.16(12-II-3)	0.28(12-I-3)
121426	0.42(12-I-3)	-0.39(13-II-4)	-0.24(2)	0.15(13-II-4)	0.10(12-I-3)	0.27(12-I-3)
121428	0.43(12-I-3)	0.38(13-I-4)	-0.27(2)	0.15(13-II-4)	0.07(13-I-4)	0.27(12-I-3)
121430	0.41(12-I-3)	0.41(13-I-4)	-0.27(2)	0.17(13-II-3)	0.08(12-I-3)	0.29(12-I-3)
121432	0.41(12-I-3)	0.43(13-I-3)	-0.27(2)	0.18(13-II-3)	0.08(13-II-3)	0.26(12-I-3)
121434	0.40(12-I-3)	0.41(13-I-2)	-0.27(2)	0.16(13-II-3)	0.08(13-II-3)	0.29(12-I-3)
121436	0.42(12-I-3)	0.39(13-I-2)	-0.27(2)	0.15(13-II-2)	0.07(13-II-3)	0.27(12-I-3)
121438	0.40(12-I-3)	0.32(13-II-2)	-0.26(2)	0.14(13-II-2)	-0.08(13-II-2)	-0.33(13-II-2)
121440	0.41(12-I-3)	-0.99(13-II-2)	-0.18(2)	0.14(13-II-2)	-0.10(2)	-1.80(13-II-2)
121470	1.35(12-I-3)	-0.57(13-II-4)	-0.05(2)	0.04(2)	0.12(12-II-3)	-2.02(12-I-3)
121471	1.38(12-I-3)	0.41(13-I-4)	-0.13(2)	0.10(2)	0.09(2)	-2.10(12-I-3)
121472	1.40(12-I-3)	0.39(13-I-4)	-0.19(2)	0.13(2)	0.06(12-I-4)	-2.05(12-I-3)
121473	1.40(12-I-3)	0.39(13-I-4)	-0.19(2)	0.13(2)	0.06(12-I-4)	-2.07(12-I-3)
121474	1.39(12-I-3)	0.43(13-I-4)	-0.19(2)	0.14(2)	0.07(12-I-3)	-2.09(12-I-3)
121475	1.38(12-I-3)	0.42(13-I-3)	-0.19(2)	0.13(2)	0.06(12-I-3)	-2.10(12-I-3)
121476	1.40(12-I-3)	0.41(13-I-2)	-0.19(2)	0.14(2)	0.05(12-I-3)	-2.07(12-I-3)
121477	1.39(12-I-3)	0.38(13-I-2)	-0.19(2)	0.13(2)	0.05(12-I-2)	-2.07(12-I-3)
121478	1.38(12-I-3)	0.34(13-I-2)	-0.17(2)	0.12(2)	-0.07(12-II-3)	2.06(12-II-3)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
121479	1.34(12-I-3)	-1.63(13-II-2)	-0.08(2)	0.06(2)	-0.07(13-I-2)	1.93(12-II-3)
121482	2.04(12-I-3)	0.40(13-I-4)	-0.12(2)	0.13(13-II-3)	0.03(2)	0.25(12-I-3)
121484	2.05(12-I-3)	0.40(13-I-4)	-0.13(2)	0.14(13-II-3)	0.01(13-I-4)	0.23(13-I-4)
121486	2.05(12-I-3)	0.43(13-I-4)	-0.13(2)	0.16(13-II-3)	-0.01(13-II-4)	0.26(12-I-3)
121488	2.05(12-I-3)	0.45(13-I-3)	-0.13(2)	0.17(13-II-3)	-0.01(13-II-2)	0.23(12-I-3)
121490	2.05(12-I-3)	0.44(13-I-2)	-0.13(2)	0.16(13-II-3)	0.01(13-II-4)	0.26(12-I-3)
121492	2.05(12-I-3)	0.42(13-I-2)	-0.13(2)	0.14(13-II-3)	0.01(13-II-2)	0.22(12-I-3)
121494	2.05(12-I-3)	0.33(13-II-2)	-0.13(2)	0.15(13-I-2)	-0.01(13-I-2)	0.29(13-I-2)
121496	2.05(12-I-3)	-0.96(13-II-2)	-0.08(2)	0.08(12-I-3)	-0.05(2)	-1.66(13-II-2)
130445	-0.08(12-II-1)	0.09(13-I-1)	-0.04(2)	-0.87(2)	0.30(2)	-0.36(12-I-1)
130449	0.08(12-I-1)	0.09(13-I-1)	-0.07(2)	-1.06(2)	-0.05(12-II-1)	-0.34(12-I-1)
130453	-0.08(12-II-1)	0.09(13-I-1)	-0.07(2)	-1.06(2)	0.05(12-I-1)	0.34(12-II-1)
130457	0.08(12-I-1)	0.09(13-I-1)	-0.04(2)	-0.86(2)	-0.25(2)	0.35(12-II-1)
130466	-0.09(12-II-1)	0.10(13-I-1)	-0.04(2)	-0.33(13-I-1)	0.05(12-I-1)	0.20(12-II-2)
130470	0.09(12-I-1)	0.11(13-I-1)	-0.04(2)	-0.27(13-I-1)	-0.05(12-II-1)	-0.21(2)
130486	-0.08(12-II-1)	0.09(13-I-2)	-0.04(2)	-0.30(2)	-0.11(2)	-0.22(12-I-1)
130490	-0.08(12-II-1)	0.08(13-I-2)	-0.04(2)	-0.87(2)	-0.07(12-II-1)	-0.36(12-I-1)
130499	0.08(12-I-1)	0.08(13-I-4)	-0.04(2)	-0.83(2)	0.05(12-I-1)	0.36(12-II-1)
130503	0.08(12-I-1)	0.09(13-I-4)	-0.04(2)	-0.31(2)	0.10(2)	0.25(12-II-1)
130513	-0.36(12-II-1)	0.09(13-I-1)	-0.61(2)	-0.17(2)	0.03(13-I-1)	0.25(12-II-1)
130514	0.36(12-I-1)	0.09(13-I-1)	-0.64(2)	-0.10(13-I-1)	0.05(13-I-1)	-0.25(12-I-1)
130515	0.36(12-I-1)	0.09(13-I-1)	-0.64(2)	-0.10(13-I-1)	-0.04(13-I-1)	0.25(12-II-1)
130516	0.36(12-I-1)	0.09(13-I-1)	-0.60(2)	-0.17(2)	-0.04(13-I-1)	-0.25(12-I-1)
130527	0.08(12-I-2)	0.09(13-I-2)	-0.07(2)	-0.97(2)	-0.39(2)	-0.34(12-I-2)
130531	0.34(12-I-1)	0.13(12-I-2)	-0.60(2)	-0.18(2)	-0.08(13-I-1)	0.25(12-II-2)
130540	0.08(12-I-4)	0.08(13-I-1)	-0.07(2)	-0.97(2)	0.40(2)	0.33(12-II-4)
130544	-0.34(12-II-1)	0.13(12-II-4)	-0.59(2)	-0.18(2)	0.08(13-I-4)	-0.25(12-I-4)
130554	-0.36(12-II-1)	0.09(13-I-1)	-0.08(2)	1.07(2)	-0.09(12-I-1)	-0.08(12-II-1)
130557	0.36(12-I-1)	0.09(13-I-1)	-0.08(2)	1.14(2)	0.09(12-II-1)	0.07(12-I-1)
130560	-0.36(12-II-1)	0.10(13-I-1)	-0.08(2)	1.14(2)	-0.09(12-I-1)	-0.06(12-II-1)
130563	0.36(12-I-1)	0.09(13-I-1)	-0.08(2)	1.06(2)	-0.09(12-I-1)	0.08(12-I-1)
130570	-0.08(12-II-2)	0.10(13-I-2)	-0.07(2)	-0.96(2)	-0.35(2)	0.32(12-II-1)
130574	0.34(12-I-1)	0.12(12-I-2)	-0.65(2)	-0.12(13-I-2)	0.05(13-II-2)	-0.26(12-I-2)
130576	0.34(12-I-1)	0.14(12-I-2)	-0.07(2)	0.98(2)	0.37(2)	-0.08(12-II-1)
130580	0.08(12-I-4)	0.09(13-I-4)	-0.07(2)	-0.97(2)	0.36(2)	-0.32(12-I-4)
130584	-0.33(12-II-4)	0.12(12-II-4)	-0.65(2)	-0.11(13-I-1)	-0.06(13-II-4)	0.26(12-II-4)
130585	-0.34(12-II-1)	0.14(12-II-4)	-0.07(2)	0.97(2)	-0.37(2)	0.08(12-I-1)
130603	0.07(12-I-2)	0.10(13-I-3)	-0.04(2)	-0.62(2)	-0.44(2)	0.27(12-II-2)
130607	0.34(12-I-2)	0.12(12-I-1)	-0.64(2)	-0.08(13-I-2)	-0.10(13-I-1)	0.26(12-II-2)
130608	0.34(12-I-2)	0.13(12-I-2)	-0.08(2)	1.08(2)	0.42(2)	0.06(12-II-2)
130612	-0.07(12-II-4)	0.09(13-I-4)	-0.04(2)	-0.79(2)	0.53(2)	-0.35(12-I-4)
130616	-0.33(12-II-4)	0.13(12-II-4)	-0.64(2)	-0.09(13-I-4)	0.08(13-I-1)	-0.26(12-I-4)
130617	-0.34(12-II-4)	0.13(12-II-4)	-0.08(2)	1.07(2)	-0.43(2)	-0.06(12-II-1)
130622	-0.08(12-II-2)	0.12(13-I-3)	-0.04(2)	-0.28(13-II-2)	-0.09(13-II-2)	0.15(12-II-2)
130626	0.08(12-I-4)	0.12(13-I-4)	-0.04(2)	-0.31(13-I-4)	0.10(13-I-4)	-0.19(2)
130648	0.32(12-I-2)	0.16(12-I-2)	-0.62(2)	-0.29(2)	0.16(2)	-0.28(12-I-2)
130649	0.35(12-I-2)	0.12(12-I-1)	-0.08(2)	1.07(2)	0.36(2)	-0.07(13-I-2)
130657	-0.32(12-II-4)	0.16(12-II-4)	-0.64(2)	-0.22(2)	-0.08(2)	0.28(12-II-4)
130658	-0.35(12-II-4)	0.14(12-II-4)	-0.08(2)	1.09(2)	-0.38(2)	0.07(12-I-4)
130668	-0.09(12-II-2)	0.15(13-I-3)	-0.04(2)	-0.18(13-I-3)	-0.19(13-I-3)	-0.28(12-I-3)
130672	0.09(12-I-3)	0.17(13-I-3)	-0.05(2)	-0.33(13-I-3)	0.37(13-I-3)	0.27(12-I-3)
130676	0.09(12-I-2)	0.14(13-I-3)	-0.05(2)	-0.93(2)	-0.46(2)	-0.40(12-I-2)
130682	-0.08(12-II-4)	0.14(13-I-3)	-0.03(2)	-0.83(2)	0.56(2)	0.38(12-II-4)
130683	0.35(12-I-2)	0.18(12-I-2)	-0.08(2)	1.04(2)	0.42(2)	0.08(12-I-1)
130691	-0.35(12-II-4)	0.17(12-II-4)	-0.08(2)	1.06(2)	-0.41(2)	-0.08(12-II-4)
130701	0.27(12-I-2)	0.29(12-I-2)	-0.69(2)	-0.03(2)	-0.32(2)	0.35(12-II-2)
130702	-0.26(12-II-4)	0.28(12-II-4)	-0.64(2)	-0.05(12-I-4)	0.26(2)	-0.34(12-I-4)
130734	0.29(12-I-2)	0.32(12-I-2)	-0.09(2)	1.04(2)	0.78(2)	0.27(12-II-3)
130735	0.29(12-I-4)	0.31(12-II-4)	-0.08(2)	0.90(2)	-0.71(2)	0.19(13-II-3)
130736	-0.68(12-II-3)	0.79(12-II-3)	-0.04(2)	-0.38(12-II-3)	-0.68(2)	0.57(12-II-2)
130737	0.55(13-I-4)	0.65(13-I-4)	-0.02(2)	-0.34(13-I-4)	0.81(2)	-0.56(12-I-4)
130760	-0.73(12-II-3)	0.81(12-II-3)	-0.29(2)	1.00(2)	-1.09(2)	0.38(12-II-2)
130761	0.58(12-I-4)	0.65(13-I-4)	-0.30(2)	0.96(2)	1.06(2)	-0.38(12-I-4)
130769	-0.76(12-II-3)	0.82(12-II-3)	-0.04(2)	0.75(2)	-0.27(12-II-3)	0.36(12-II-3)
130793	0.61(12-I-4)	0.64(13-I-4)	-0.04(2)	0.79(2)	-0.17(13-I-3)	-0.28(13-I-3)
140351	-0.25(12-II-1)	0.12(13-I-1)	-0.05(2)	-0.58(2)	0.24(2)	-0.06(12-II-1)
140354	-0.25(12-II-1)	0.16(13-I-1)	-0.08(2)	-0.99(2)	-0.09(12-I-1)	0.05(12-II-1)
140357	-0.25(12-II-1)	0.15(13-I-1)	-0.08(2)	-0.98(2)	0.08(12-II-1)	-0.05(12-I-1)
140360	0.25(12-I-1)	0.12(13-I-1)	-0.05(2)	-0.57(2)	-0.22(2)	0.06(12-I-1)
140363	-0.24(12-II-1)	0.12(13-I-1)	-0.05(2)	-0.58(2)	0.12(12-II-1)	-0.06(12-II-1)
140367	-0.24(12-II-1)	0.12(13-I-1)	-0.05(2)	-0.60(2)	-0.11(12-I-1)	0.05(12-II-2)
140378	0.24(12-I-1)	0.10(13-I-2)	-0.05(2)	-0.52(2)	-0.26(2)	0.06(12-II-2)
140389	-0.24(12-II-1)	0.10(13-I-1)	-0.05(2)	-0.51(2)	0.26(2)	-0.06(12-II-4)
140392	-0.23(12-II-1)	0.11(13-I-2)	-0.04(2)	-0.60(2)	0.09(12-II-1)	0.06(12-II-2)
140401	-0.23(12-II-1)	0.10(13-I-1)	-0.04(2)	-0.59(2)	-0.09(12-I-1)	-0.06(12-II-4)
140405	-0.26(12-II-1)	0.13(13-I-1)	-0.38(2)	-0.07(2)	0.58(2)	-0.18(12-II-1)
140406	-0.26(12-II-1)	0.16(13-I-1)	-0.64(2)	-0.07(13-II-1)	0.05(13-II-1)	-0.15(12-II-1)
140407	-0.26(12-II-1)	0.15(13-I-1)	-0.64(2)	-0.07(13-II-1)	-0.06(13-II-1)	0.15(12-I-1)
140408	-0.26(12-II-1)	0.12(13-I-1)	-0.37(2)	-0.06(2)	-0.51(2)	-0.19(12-II-1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
140409	-0.25(12-II-1)	0.12(13-I-1)	-0.37(2)	-0.12(2)	0.46(2)	-0.19(12-II-1)
140412	-0.25(12-II-1)	0.13(13-I-1)	-0.38(2)	-0.13(2)	-0.53(2)	0.18(12-I-1)
140423	-0.24(12-II-1)	0.10(13-I-2)	-0.37(2)	0.05(2)	-0.46(2)	0.20(12-I-2)
140424	0.25(12-I-2)	0.13(13-I-1)	-0.07(2)	-0.91(2)	-0.35(2)	0.05(12-II-2)
140427	-0.24(12-II-1)	0.11(13-I-2)	-0.37(2)	-0.23(2)	0.44(2)	0.19(12-I-2)
140428	-0.24(12-II-1)	0.10(13-I-1)	-0.36(2)	0.07(2)	0.46(2)	-0.20(12-II-4)
140437	-0.25(12-II-4)	0.13(13-I-1)	-0.08(2)	-0.90(2)	0.36(2)	-0.06(12-I-4)
140440	-0.24(12-II-1)	0.11(13-I-1)	-0.36(2)	-0.23(2)	-0.40(2)	-0.20(12-II-4)
140445	0.10(12-I-1)	0.13(13-I-1)	-0.05(2)	0.64(2)	0.08(12-I-1)	0.17(12-I-1)
140449	0.10(12-I-1)	0.16(13-I-1)	-0.07(2)	1.12(2)	0.06(12-I-1)	-0.21(12-II-1)
140453	-0.10(12-II-1)	0.15(13-I-1)	-0.07(2)	1.11(2)	-0.05(12-II-1)	0.20(12-I-1)
140457	-0.10(12-II-1)	0.12(13-I-1)	-0.05(2)	0.63(2)	-0.08(12-II-1)	-0.17(12-II-1)
140466	-0.09(12-II-1)	0.12(13-I-1)	-0.04(2)	0.64(2)	0.27(2)	-0.17(12-II-1)
140470	0.09(12-I-1)	0.12(13-I-1)	-0.04(2)	0.69(2)	-0.35(2)	-0.16(12-II-1)
140481	0.25(12-I-2)	0.16(13-I-2)	-0.07(2)	-0.92(2)	-0.35(2)	-0.03(13-I-1)
140485	0.25(12-I-2)	0.14(13-I-1)	-0.64(2)	-0.07(13-II-1)	0.06(13-I-2)	0.15(12-I-2)
140486	-0.09(12-II-1)	0.10(13-I-1)	-0.04(2)	0.69(2)	-0.07(12-II-1)	0.17(12-I-2)
140490	-0.09(12-II-1)	0.10(13-I-2)	-0.05(2)	0.57(2)	0.24(2)	0.17(12-I-1)
140495	-0.26(12-II-4)	0.15(13-I-4)	-0.07(2)	-0.92(2)	0.36(2)	0.04(12-II-4)
140498	-0.26(12-II-4)	0.13(13-I-1)	-0.63(2)	-0.07(13-I-1)	-0.05(13-II-4)	-0.15(12-II-4)
140499	0.09(12-I-1)	0.10(13-I-1)	-0.05(2)	0.56(2)	-0.20(2)	-0.18(12-II-4)
140503	0.09(12-I-1)	0.10(13-I-1)	-0.04(2)	0.68(2)	0.08(12-I-1)	-0.18(12-II-4)
140522	0.25(12-I-2)	0.15(13-I-3)	-0.05(2)	-0.45(2)	-0.41(2)	0.06(12-I-1)
140526	0.25(12-I-2)	0.17(13-I-2)	-0.64(2)	-0.06(13-II-2)	-0.08(13-I-1)	0.16(12-I-2)
140527	-0.10(12-II-2)	0.13(13-I-1)	-0.07(2)	1.05(2)	0.40(2)	-0.20(12-II-2)
140536	-0.25(12-II-4)	0.14(13-I-4)	-0.05(2)	-0.46(2)	0.42(2)	-0.07(12-II-4)
140539	-0.26(12-II-4)	0.15(13-I-4)	-0.64(2)	-0.05(13-II-4)	0.07(13-I-1)	-0.17(12-II-4)
140540	0.10(12-I-4)	0.12(13-I-1)	-0.07(2)	1.04(2)	-0.41(2)	-0.20(12-II-1)
140546	0.24(12-I-2)	0.15(13-I-2)	-0.04(2)	-0.56(2)	-0.16(12-I-2)	0.06(12-I-1)
140550	-0.23(12-II-4)	0.15(13-I-4)	-0.04(2)	-0.59(2)	0.18(12-II-4)	-0.06(12-II-1)
140568	0.25(12-I-2)	0.15(13-I-3)	-0.37(2)	0.17(2)	-0.59(2)	0.19(12-I-2)
140570	-0.10(12-II-2)	0.15(13-I-2)	-0.07(2)	1.06(2)	0.41(2)	0.21(12-I-2)
140579	-0.25(12-II-4)	0.14(13-I-4)	-0.38(2)	0.16(2)	0.56(2)	-0.20(12-II-4)
140580	0.10(12-I-4)	0.14(13-I-4)	-0.07(2)	1.06(2)	-0.41(2)	-0.22(12-II-4)
140588	0.23(12-I-2)	0.16(13-I-2)	-0.36(2)	-0.30(2)	0.47(2)	0.19(12-I-2)
140589	-0.23(12-II-4)	0.15(13-I-4)	-0.38(2)	-0.33(2)	-0.45(2)	-0.19(12-II-4)
140597	0.26(12-I-2)	0.17(13-I-2)	-0.05(2)	-0.39(2)	-0.45(2)	0.09(12-II-2)
140600	-0.26(12-II-4)	0.21(13-I-4)	-0.08(2)	-0.83(2)	0.53(2)	-0.21(13-I-4)
140603	-0.09(12-II-2)	0.13(13-I-3)	-0.05(2)	0.62(2)	0.11(12-I-2)	0.16(12-I-2)
140612	0.09(12-I-4)	0.13(13-I-4)	-0.05(2)	0.70(2)	-0.14(13-II-4)	0.17(12-I-4)
140621	0.23(12-I-2)	0.19(13-I-2)	-0.05(2)	-0.57(2)	-0.21(2)	0.29(12-II-3)
140622	-0.09(12-II-2)	0.14(13-I-3)	-0.04(2)	0.40(2)	0.34(2)	0.14(12-I-2)
140626	0.09(12-I-4)	0.13(13-I-4)	-0.04(2)	0.57(2)	-0.48(2)	-0.16(12-II-4)
140633	0.25(12-I-2)	0.17(13-I-2)	-0.39(2)	0.28(2)	-0.53(2)	0.22(12-I-2)
140634	0.26(12-I-4)	0.22(13-I-3)	-0.62(2)	-0.34(2)	0.09(13-II-4)	-0.18(12-I-4)
140647	-0.23(12-II-2)	0.19(13-I-2)	-0.38(2)	-0.44(2)	0.39(2)	0.29(12-II-2)
140665	0.47(13-I-4)	0.81(13-I-4)	-0.04(2)	-0.18(12-I-3)	0.61(2)	-0.21(12-I-3)
140666	0.16(12-I-3)	0.20(13-I-3)	-0.20(2)	0.98(2)	-1.23(2)	-0.40(12-II-4)
140667	0.48(13-I-4)	0.82(13-I-4)	0.04(2)	0.14(12-II-3)	0.62(2)	-0.18(12-II-3)
140668	-0.11(12-II-2)	0.15(13-I-3)	-0.05(2)	0.77(2)	0.16(13-II-3)	0.25(12-II-2)
140672	0.13(12-I-3)	0.19(13-I-3)	-0.06(2)	1.00(2)	-0.38(13-II-3)	-0.31(12-II-4)
140676	-0.12(12-II-2)	0.17(13-I-3)	-0.05(2)	0.41(2)	0.42(2)	0.37(12-II-3)
140681	-0.74(12-II-3)	0.87(12-II-3)	-0.04(2)	-0.35(12-II-3)	-0.66(2)	0.38(12-II-3)
140682	0.13(12-I-3)	0.20(13-I-4)	-0.03(2)	0.44(13-II-3)	-0.26(13-II-3)	-0.34(12-I-3)
140699	0.49(13-I-4)	0.80(13-I-4)	-0.21(2)	0.83(2)	1.35(2)	-0.25(12-II-3)
140700	0.50(13-I-4)	0.81(13-I-4)	-0.03(12-I-3)	0.87(2)	1.17(2)	-0.23(12-II-4)
140703	-0.75(12-II-3)	0.86(12-II-3)	-0.29(2)	0.97(2)	-1.06(2)	0.26(12-II-2)
140717	0.50(13-I-4)	0.79(13-I-4)	-0.04(2)	0.98(2)	0.65(2)	-0.32(12-I-3)
140730	0.51(13-I-4)	0.80(13-I-4)	0.06(2)	0.71(2)	0.71(2)	-0.34(12-I-3)
140736	-0.75(12-II-3)	0.83(12-II-3)	-0.04(2)	0.67(2)	-0.23(12-II-3)	0.48(12-II-3)
140737	0.61(13-I-4)	0.69(13-I-4)	-0.02(2)	-0.16(12-I-3)	0.47(2)	-0.63(13-I-3)
150003	0.36(12-I-1)	-0.58(13-II-4)	-0.07(2)	-0.08(2)	0.25(2)	0.23(13-II-4)
150004	0.36(12-I-1)	0.43(13-I-4)	-0.16(2)	-0.21(2)	0.16(2)	0.17(13-II-4)
150005	0.35(12-I-1)	0.44(13-I-4)	-0.23(2)	-0.32(13-I-4)	0.05(12-I-3)	-0.17(12-I-1)
150006	0.34(12-I-1)	0.42(13-I-4)	-0.23(2)	-0.29(2)	0.04(12-I-3)	-0.18(13-II-4)
150007	0.34(12-I-1)	0.46(13-I-4)	-0.24(2)	-0.29(13-I-1)	0.07(12-I-4)	-0.17(12-I-1)
150008	0.34(12-I-1)	0.46(13-I-1)	-0.24(2)	-0.29(13-I-1)	-0.06(12-II-4)	0.15(12-II-1)
150009	0.34(12-I-1)	0.44(13-I-2)	-0.23(2)	-0.29(2)	-0.03(12-II-3)	-0.15(12-II-1)
150010	0.33(12-I-1)	0.42(13-I-2)	-0.23(2)	-0.31(13-I-2)	-0.04(12-II-3)	-0.14(12-I-1)
150011	-0.34(12-II-1)	0.36(13-I-2)	-0.21(2)	-0.27(2)	-0.11(12-II-4)	-0.66(13-II-2)
150012	-0.34(12-II-1)	-1.64(13-II-2)	-0.10(2)	-0.19(13-II-2)	-0.24(2)	-0.95(13-II-2)
150013	0.42(12-I-1)	-0.58(13-II-4)	-0.07(2)	0.01(12-I-4)	0.32(2)	0.18(12-II-4)
150014	0.42(12-I-1)	-0.43(13-II-4)	-0.17(2)	-0.02(13-II-4)	0.20(2)	0.16(12-II-4)
150015	0.42(12-I-1)	0.43(13-I-4)	-0.25(2)	-0.03(12-I-4)	0.03(2)	0.17(12-II-4)
150016	0.41(12-I-1)	0.41(13-I-4)	-0.26(2)	-0.02(13-I-1)	0.02(13-I-4)	-0.19(12-I-4)
150017	0.41(12-I-1)	-0.45(13-II-4)	-0.26(2)	-0.02(12-I-1)	0.04(12-I-1)	0.19(12-II-1)
150018	0.39(12-I-1)	-0.45(13-II-1)	-0.26(2)	-0.01(13-I-1)	0.03(12-I-1)	-0.16(12-I-1)
150019	0.40(12-I-1)	0.42(13-I-2)	-0.26(2)	-0.02(12-I-2)	0.02(13-II-2)	0.15(12-I-1)
150020	0.39(12-I-1)	0.41(13-I-2)	-0.25(2)	-0.02(13-I-1)	-0.02(13-I-2)	-0.16(12-I-2)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
150021	0.39(12-I-1)	-0.36(13-II-2)	-0.23(2)	-0.02(12-I-2)	-0.13(2)	-0.48(13-II-2)
150022	-0.38(12-II-1)	-1.64(13-II-2)	-0.11(2)	-0.01(12-I-2)	-0.29(2)	-0.48(13-II-2)
150023	0.48(12-I-1)	-0.58(13-II-4)	-0.07(2)	0.01(12-II-3)	0.32(2)	0.16(13-II-4)
150024	0.48(12-I-1)	-0.42(13-II-4)	-0.17(2)	-0.03(13-II-4)	0.20(2)	0.13(12-II-3)
150025	0.48(12-I-1)	0.42(13-I-4)	-0.25(2)	-0.02(12-I-4)	0.03(2)	-0.14(13-II-4)
150026	0.47(12-I-1)	-0.40(13-II-4)	-0.25(2)	-0.01(12-II-4)	0.01(13-II-4)	-0.15(13-I-4)
150027	0.46(12-I-1)	-0.45(13-II-4)	-0.25(2)	-0.01(12-II-3)	0.04(12-I-1)	-0.13(13-II-1)
150028	0.45(12-I-1)	-0.43(13-II-1)	-0.25(2)	-0.01(13-II-3)	0.03(12-I-1)	0.13(13-II-4)
150029	0.46(12-I-1)	0.42(13-I-2)	-0.25(2)	-0.02(12-I-3)	0.02(13-I-2)	0.12(12-I-1)
150030	0.45(12-I-1)	0.40(13-I-2)	-0.25(2)	-0.01(12-II-2)	0.01(13-I-2)	0.12(12-II-2)
150031	0.45(12-I-1)	-0.35(13-II-2)	-0.23(2)	-0.02(12-II-3)	-0.13(2)	-0.49(13-II-2)
150032	-0.44(12-II-1)	-1.64(13-II-2)	-0.11(2)	-0.01(13-I-2)	-0.30(2)	-0.54(13-II-2)
150033	0.47(12-I-4)	-0.58(13-II-4)	-0.07(2)	-0.01(12-II-3)	0.32(2)	0.16(13-II-4)
150034	0.47(12-I-4)	-0.42(13-II-4)	-0.17(2)	-0.01(13-I-1)	0.20(2)	0.13(13-II-4)
150035	0.46(12-I-4)	0.41(13-I-4)	-0.24(2)	-0.04(13-I-1)	0.03(2)	0.13(12-I-1)
150036	0.45(12-I-1)	-0.40(13-II-4)	-0.25(2)	-0.04(13-I-1)	0.02(13-I-4)	-0.14(13-I-1)
150037	0.45(12-I-1)	-0.45(13-II-4)	-0.25(2)	-0.04(13-I-1)	0.05(12-I-4)	-0.11(13-II-4)
150038	0.43(12-I-1)	-0.43(13-II-2)	-0.25(2)	-0.04(13-I-1)	0.03(12-I-4)	0.14(13-II-4)
150039	0.44(12-I-1)	-0.42(13-II-2)	-0.25(2)	-0.04(13-I-1)	0.02(13-II-2)	0.14(12-I-1)
150040	0.43(12-I-2)	-0.40(13-II-2)	-0.25(2)	-0.04(13-I-2)	-0.01(13-I-2)	-0.12(12-II-1)
150041	0.43(12-I-2)	-0.35(13-II-2)	-0.23(2)	-0.03(13-I-2)	-0.13(2)	-0.48(13-II-2)
150042	-0.42(12-II-2)	-1.64(13-II-2)	-0.11(2)	-0.02(13-I-2)	-0.30(2)	-0.53(13-II-2)
150043	0.48(12-I-4)	-0.58(13-II-4)	-0.07(2)	-0.01(12-I-1)	0.32(2)	0.17(13-II-4)
150044	0.48(12-I-4)	-0.41(13-II-4)	-0.17(2)	-0.01(12-II-3)	0.20(2)	0.13(12-II-3)
150045	0.47(12-I-4)	0.40(13-I-4)	-0.25(2)	-0.03(13-I-4)	0.03(2)	-0.15(12-II-1)
150046	0.46(12-I-4)	-0.39(13-II-4)	-0.25(2)	-0.03(13-I-1)	0.02(13-II-4)	0.15(13-I-4)
150047	0.45(12-I-4)	-0.43(13-II-4)	-0.25(2)	-0.03(13-I-1)	0.05(12-I-4)	-0.13(12-I-3)
150048	0.43(12-I-2)	-0.42(13-II-2)	-0.25(2)	-0.03(13-I-1)	0.03(12-I-4)	0.14(12-II-3)
150049	0.44(12-I-2)	-0.41(13-II-2)	-0.25(2)	-0.03(13-I-2)	0.02(13-I-2)	0.13(12-I-3)
150050	0.44(12-I-2)	-0.39(13-II-2)	-0.25(2)	-0.03(13-I-2)	-0.02(13-II-2)	0.14(13-II-2)
150051	0.44(12-I-2)	-0.35(13-II-2)	-0.23(2)	-0.02(12-I-1)	-0.13(2)	-0.48(13-II-2)
150052	-0.43(12-II-2)	-1.64(13-II-2)	-0.11(2)	-0.02(13-I-2)	-0.30(2)	-0.54(13-II-2)
150053	0.49(12-I-3)	-0.58(13-II-4)	-0.07(2)	-0.01(12-I-1)	0.32(2)	0.15(12-II-4)
150054	0.48(12-I-3)	-0.42(13-II-4)	-0.17(2)	-0.03(13-II-4)	0.20(2)	0.16(12-II-4)
150055	0.48(12-I-3)	-0.40(13-II-4)	-0.25(2)	-0.02(12-II-1)	0.03(2)	0.15(12-II-4)
150056	0.47(12-I-3)	-0.40(13-II-4)	-0.25(2)	-0.02(12-I-1)	0.02(13-I-4)	-0.15(13-II-4)
150057	0.47(12-I-3)	-0.44(13-II-4)	-0.25(2)	-0.02(12-II-1)	0.04(12-I-3)	-0.13(13-II-4)
150058	0.45(12-I-3)	-0.43(13-II-2)	-0.25(2)	-0.01(2)	0.03(12-I-3)	0.14(13-II-4)
150059	0.46(12-I-3)	-0.41(13-II-2)	-0.25(2)	-0.02(12-II-1)	0.02(13-II-2)	0.12(13-II-2)
150060	0.45(12-I-3)	-0.39(13-II-2)	-0.25(2)	-0.01(12-II-1)	-0.02(13-I-2)	-0.11(12-II-2)
150061	0.45(12-I-3)	-0.35(13-II-2)	-0.23(2)	-0.02(12-II-1)	-0.13(2)	-0.49(13-II-2)
150062	-0.44(12-II-3)	-1.64(13-II-2)	-0.11(2)	-0.02(13-I-2)	-0.30(2)	-0.53(13-II-2)
150063	0.49(12-I-3)	-0.58(13-II-4)	-0.07(2)	0.01(12-I-3)	0.32(2)	0.19(12-II-3)
150064	0.49(12-I-3)	-0.42(13-II-4)	-0.17(2)	-0.02(13-II-4)	0.20(2)	0.20(12-II-3)
150065	0.48(12-I-3)	-0.40(13-II-4)	-0.25(2)	-0.02(12-II-4)	0.03(2)	0.16(12-I-4)
150066	0.47(12-I-3)	-0.40(13-II-4)	-0.25(2)	-0.01(12-II-3)	0.01(13-I-4)	-0.14(13-II-4)
150067	0.47(12-I-3)	-0.44(13-II-4)	-0.25(2)	-0.02(12-I-3)	0.04(12-I-3)	0.12(12-I-1)
150068	0.45(12-I-3)	-0.42(13-II-2)	-0.25(2)	-0.01(12-II-3)	0.03(12-I-3)	-0.13(12-I-3)
150069	0.46(12-I-3)	-0.41(13-II-2)	-0.25(2)	-0.02(12-I-3)	0.02(13-I-3)	0.12(12-II-3)
150070	0.45(12-I-3)	-0.39(13-II-2)	-0.25(2)	-0.01(13-I-2)	0.01(13-I-2)	-0.13(12-I-3)
150071	0.45(12-I-3)	-0.35(13-II-2)	-0.23(2)	-0.02(12-I-3)	-0.13(2)	-0.49(13-II-2)
150072	-0.44(12-II-3)	-1.64(13-II-2)	-0.11(2)	-0.02(13-I-2)	-0.30(2)	-0.53(13-II-2)
150073	0.44(12-I-3)	-0.58(13-II-4)	-0.06(2)	0.03(12-II-3)	0.29(2)	0.71(12-II-3)
150074	0.44(12-I-3)	-0.42(13-II-4)	-0.16(2)	0.06(12-II-3)	0.19(2)	0.52(12-II-3)
150075	0.43(12-I-3)	-0.40(13-II-4)	-0.23(2)	0.08(13-II-4)	0.03(12-II-3)	0.59(12-II-3)
150076	0.42(12-I-3)	-0.40(13-II-4)	-0.23(2)	0.08(13-II-4)	0.02(12-II-3)	-0.57(12-I-3)
150077	0.42(12-I-3)	-0.44(13-II-4)	-0.23(2)	0.09(13-II-3)	0.03(12-I-3)	-0.55(12-I-3)
150078	0.41(12-I-3)	-0.43(13-II-3)	-0.23(2)	0.09(13-II-3)	0.02(12-I-3)	-0.56(12-I-3)
150079	0.41(12-I-3)	-0.42(13-II-2)	-0.23(2)	0.08(13-II-2)	0.02(12-II-3)	-0.57(12-I-3)
150080	0.41(12-I-3)	-0.39(13-II-2)	-0.23(2)	0.08(13-II-2)	-0.02(12-I-3)	-0.58(12-I-3)
150081	0.41(12-I-3)	-0.36(13-II-2)	-0.21(2)	0.06(2)	-0.12(2)	-0.62(12-I-3)
150082	-0.40(12-II-3)	-1.64(13-II-2)	-0.10(2)	0.04(12-I-3)	-0.27(2)	-0.83(12-I-3)
150083	2.05(12-I-3)	-0.58(13-II-4)	-0.03(2)	0.08(2)	0.15(2)	0.98(12-II-3)
150084	2.05(12-I-3)	-0.42(13-II-4)	-0.08(2)	0.18(2)	0.09(2)	0.58(12-II-3)
150085	2.05(12-I-3)	-0.40(13-II-4)	-0.11(2)	0.25(2)	0.02(12-I-3)	0.59(12-II-3)
150086	2.05(12-I-3)	-0.39(13-II-4)	-0.12(2)	0.26(2)	0.02(12-I-3)	0.59(12-II-3)
150087	2.05(12-I-3)	-0.43(13-II-4)	-0.11(2)	0.26(2)	0.02(12-I-3)	0.60(12-II-3)
150088	2.05(12-I-3)	-0.42(13-II-3)	-0.11(2)	0.26(2)	0.02(12-I-3)	0.60(12-II-3)
150089	2.05(12-I-3)	-0.41(13-II-2)	-0.11(2)	0.26(2)	0.02(12-I-3)	0.59(12-II-3)
150090	2.05(12-I-3)	-0.38(13-II-2)	-0.12(2)	0.25(2)	0.02(12-I-3)	0.60(12-II-3)
150091	2.05(12-I-3)	-0.35(13-II-2)	-0.10(2)	0.23(2)	-0.06(2)	-0.70(12-I-3)
150092	2.04(12-I-3)	-1.64(13-II-2)	-0.05(2)	0.11(2)	-0.14(2)	-1.13(12-I-3)
150964	0.36(12-I-1)	0.47(13-I-4)	-0.23(2)	-0.27(13-I-1)	0.07(12-I-1)	-0.14(13-II-2)
150965	0.35(12-I-1)	0.49(13-I-1)	-0.25(2)	-0.29(13-I-1)	0.09(12-II-4)	-0.23(13-II-4)
150966	0.35(12-I-1)	0.51(13-I-1)	-0.26(2)	-0.33(13-I-1)	0.05(12-I-1)	-0.19(13-II-4)
150967	0.34(12-I-1)	0.54(13-I-1)	-0.26(2)	-0.34(13-I-1)	0.05(12-II-1)	-0.18(13-II-2)
150968	0.34(12-I-1)	0.51(13-I-1)	-0.26(2)	-0.32(13-I-1)	0.05(12-I-1)	-0.17(13-I-4)
150969	0.34(12-I-1)	0.49(13-I-2)	-0.25(2)	-0.33(13-I-1)	0.08(12-II-1)	-0.20(13-I-2)
150970	0.34(12-I-1)	0.40(13-II-2)	-0.25(2)	-0.25(2)	0.05(12-I-1)	-0.26(13-I-2)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
150971	-0.34(12-II-1)	-0.93(13-II-2)	-0.18(2)	-0.17(2)	-0.09(13-II-2)	-1.68(13-II-2)
150982	0.37(12-I-1)	-0.58(13-II-4)	-0.09(2)	0.03(13-II-4)	0.20(2)	-0.34(12-I-4)
150983	0.41(12-I-1)	0.43(13-I-4)	-0.21(2)	0.10(13-II-4)	0.20(12-I-1)	-0.36(12-I-4)
150984	0.45(12-I-1)	0.43(13-I-4)	-0.30(2)	0.09(13-II-4)	0.20(12-I-1)	-0.33(12-I-4)
150985	0.42(12-I-1)	0.42(13-I-4)	-0.30(2)	0.11(13-II-4)	0.17(12-I-1)	-0.34(12-I-4)
150986	0.44(12-I-1)	0.46(13-I-4)	-0.31(2)	0.12(13-II-4)	0.24(12-I-1)	0.34(12-II-4)
150987	0.42(12-I-1)	0.45(13-I-1)	-0.31(2)	0.12(13-II-2)	0.22(12-I-1)	-0.34(12-I-4)
150988	0.43(12-I-1)	0.43(13-I-2)	-0.31(2)	0.11(13-II-2)	0.18(12-I-1)	-0.33(12-I-4)
150989	0.42(12-I-1)	0.42(13-I-2)	-0.30(2)	0.09(13-II-2)	0.18(12-I-1)	-0.33(12-I-1)
150990	0.41(12-I-1)	0.36(13-I-2)	-0.28(2)	0.09(13-II-2)	-0.24(12-II-1)	0.36(12-II-2)
150991	-0.35(12-II-1)	-1.64(13-II-2)	-0.14(2)	0.06(13-II-2)	-0.15(2)	0.35(12-II-2)
151032	0.42(12-I-1)	0.55(13-I-4)	-0.27(2)	0.19(13-II-1)	0.09(12-I-1)	0.15(13-I-2)
151033	0.41(12-I-1)	0.57(13-I-1)	-0.30(2)	0.21(13-II-1)	0.07(12-I-1)	0.27(13-I-4)
151034	0.41(12-I-1)	-0.58(13-II-1)	-0.30(2)	-0.21(13-I-1)	0.06(12-I-1)	-0.20(13-II-4)
151035	0.40(12-I-1)	-0.62(13-II-1)	-0.30(2)	0.22(13-II-1)	-0.07(12-I-1)	0.18(13-I-2)
151036	0.40(12-I-1)	-0.58(13-II-1)	-0.29(2)	-0.21(13-I-1)	0.06(12-I-1)	0.16(13-II-4)
151037	0.40(12-I-1)	0.54(13-I-2)	-0.30(2)	-0.21(13-I-1)	-0.07(12-I-1)	0.20(13-I-2)
151038	0.40(12-I-1)	-0.46(13-I-2)	-0.29(2)	-0.18(13-I-1)	0.07(12-I-1)	-0.28(13-I-2)
151039	0.38(12-I-1)	-0.99(13-II-2)	-0.20(2)	-0.09(13-I-2)	-0.08(2)	-1.80(13-II-2)
151050	0.48(12-I-1)	-0.58(13-II-4)	-0.08(2)	0.02(13-I-4)	0.24(2)	-0.20(12-I-4)
151051	0.53(12-I-1)	-0.42(13-II-4)	-0.20(2)	0.08(13-I-4)	0.28(12-I-1)	-0.22(12-I-4)
151052	0.57(12-I-1)	0.42(13-I-4)	-0.29(2)	0.09(13-I-4)	0.28(12-I-4)	-0.20(12-I-4)
151053	0.56(12-I-1)	0.40(13-I-4)	-0.29(2)	0.09(13-I-1)	0.27(12-I-1)	0.19(12-II-4)
151054	0.56(12-I-1)	0.45(13-I-4)	-0.30(2)	0.11(13-I-1)	0.30(12-I-1)	0.19(12-II-4)
151055	0.54(12-I-1)	0.43(13-I-1)	-0.29(2)	0.12(13-I-1)	0.28(12-I-1)	-0.19(12-I-2)
151056	0.55(12-I-1)	0.42(13-I-2)	-0.30(2)	0.09(13-I-2)	0.25(12-I-1)	-0.20(12-I-2)
151057	0.54(12-I-1)	0.41(13-I-2)	-0.29(2)	0.09(13-I-2)	0.26(12-I-1)	0.20(12-II-2)
151058	0.53(12-I-1)	-0.35(13-II-2)	-0.27(2)	0.08(13-I-2)	-0.30(12-II-1)	0.23(12-II-2)
151059	-0.46(12-II-1)	-1.64(13-II-2)	-0.13(2)	0.02(13-I-2)	-0.19(2)	0.22(13-II-2)
151100	0.48(12-I-1)	0.52(13-I-4)	-0.27(2)	0.19(13-II-1)	0.10(12-I-1)	0.14(13-I-2)
151101	0.47(12-I-1)	0.54(13-I-1)	-0.29(2)	0.19(13-II-1)	0.09(12-II-1)	0.26(13-I-4)
151102	0.47(12-I-1)	0.55(13-I-4)	-0.29(2)	-0.18(13-I-1)	0.07(12-I-1)	-0.20(13-II-4)
151103	0.45(12-I-1)	-0.59(13-II-1)	-0.29(2)	-0.20(13-I-1)	-0.07(12-I-1)	0.18(13-I-2)
151104	0.46(12-I-1)	-0.56(13-II-2)	-0.29(2)	-0.18(13-I-1)	0.08(12-I-1)	0.15(13-II-4)
151105	0.45(12-I-1)	0.53(13-I-2)	-0.29(2)	-0.18(13-I-1)	-0.08(12-I-1)	0.19(13-II-2)
151106	0.45(12-I-1)	-0.44(13-I-2)	-0.29(2)	-0.15(13-II-2)	0.08(12-I-1)	-0.28(13-I-2)
151107	0.44(12-I-1)	-0.98(13-II-2)	-0.20(2)	-0.10(13-I-2)	-0.08(2)	-1.79(13-II-2)
151118	0.50(12-I-1)	-0.58(13-II-4)	-0.08(2)	0.01(13-II-4)	0.24(2)	-0.19(12-II-3)
151119	0.55(12-I-1)	-0.42(13-II-4)	-0.20(2)	0.08(13-II-4)	0.31(12-I-4)	-0.20(12-II-3)
151120	0.59(12-I-1)	0.42(13-I-4)	-0.28(2)	0.07(13-II-4)	0.30(12-I-4)	-0.18(12-II-3)
151121	0.58(12-I-1)	0.41(13-I-4)	-0.29(2)	0.07(13-II-4)	0.27(12-I-4)	0.17(12-I-3)
151122	0.58(12-I-1)	0.45(13-I-4)	-0.29(2)	0.08(13-II-4)	0.30(12-I-1)	0.17(12-I-3)
151123	0.56(12-I-1)	0.43(13-I-2)	-0.29(2)	0.08(13-II-2)	0.28(12-I-1)	-0.17(12-II-3)
151124	0.57(12-I-1)	0.42(13-I-2)	-0.29(2)	0.07(13-II-2)	0.25(12-I-1)	-0.17(12-II-3)
151125	0.56(12-I-1)	0.40(13-I-2)	-0.29(2)	0.06(13-II-2)	0.27(12-I-2)	0.17(12-I-3)
151126	0.55(12-I-1)	-0.35(13-II-2)	-0.26(2)	0.06(13-II-2)	-0.34(12-II-2)	0.24(13-II-2)
151127	-0.48(12-II-1)	-1.64(13-II-2)	-0.13(2)	0.01(12-I-2)	-0.19(2)	0.24(13-II-2)
151172	0.47(12-I-4)	0.53(13-I-4)	-0.27(2)	0.19(13-II-4)	0.10(12-I-4)	0.14(13-I-2)
151173	0.45(12-I-1)	0.52(13-I-1)	-0.29(2)	-0.20(13-I-1)	0.10(12-II-1)	0.25(13-I-4)
151174	0.45(12-I-1)	0.56(13-I-4)	-0.29(2)	-0.21(13-I-1)	0.08(12-I-1)	-0.20(13-II-4)
151175	0.44(12-I-1)	-0.56(13-II-1)	-0.29(2)	-0.21(13-I-1)	-0.07(12-I-1)	-0.18(13-II-2)
151176	0.44(12-I-1)	-0.56(13-II-2)	-0.29(2)	-0.21(13-I-1)	0.08(12-I-1)	0.15(13-II-4)
151177	0.43(12-I-1)	0.53(13-I-2)	-0.29(2)	-0.20(13-I-2)	-0.09(12-I-1)	0.18(13-II-2)
151178	0.44(12-I-2)	-0.44(13-I-2)	-0.29(2)	-0.18(13-II-2)	0.08(12-I-1)	-0.28(13-I-2)
151179	0.43(12-I-2)	-0.98(13-II-2)	-0.20(2)	-0.12(13-I-2)	-0.08(2)	-1.80(13-II-2)
151180	0.51(12-I-4)	-0.58(13-II-4)	-0.08(2)	0.01(12-II-3)	0.24(2)	-0.26(12-I-3)
151181	0.58(12-I-4)	-0.41(13-II-4)	-0.20(2)	0.06(13-I-4)	0.33(12-I-4)	-0.27(12-I-3)
151182	0.61(12-I-4)	0.40(13-I-4)	-0.28(2)	0.09(13-I-4)	0.31(12-I-4)	-0.24(12-I-3)
151183	0.58(12-I-4)	0.39(13-I-4)	-0.29(2)	0.09(13-I-4)	0.28(12-I-4)	0.23(12-II-3)
151184	0.57(12-I-4)	0.43(13-I-4)	-0.29(2)	0.09(13-I-4)	0.30(12-I-4)	0.23(12-I-3)
151185	0.54(12-I-2)	0.42(13-I-2)	-0.29(2)	0.09(13-I-2)	0.26(12-I-2)	-0.23(12-I-3)
151186	0.57(12-I-2)	0.41(13-I-2)	-0.29(2)	0.09(13-I-2)	0.25(12-I-2)	-0.23(12-I-3)
151187	0.58(12-I-2)	0.39(13-I-2)	-0.29(2)	0.08(13-I-2)	0.28(12-I-2)	0.23(12-II-3)
151188	0.58(12-I-2)	-0.34(13-II-2)	-0.26(2)	0.07(13-II-2)	-0.36(12-II-2)	0.26(12-I-3)
151189	-0.49(12-II-2)	-1.64(13-II-2)	-0.13(2)	0.01(13-I-2)	-0.19(2)	0.24(12-I-3)
151244	0.48(12-I-4)	0.50(13-I-4)	-0.27(2)	0.17(13-II-4)	0.10(12-I-4)	0.14(13-I-2)
151245	0.46(12-I-4)	-0.50(13-II-4)	-0.29(2)	-0.17(13-I-4)	0.10(12-II-4)	0.24(13-I-4)
151246	0.46(12-I-4)	-0.54(13-II-4)	-0.29(2)	-0.19(13-I-4)	0.08(12-I-4)	0.19(13-I-4)
151247	0.44(12-I-4)	-0.54(13-II-3)	-0.29(2)	-0.19(13-I-1)	-0.07(12-I-2)	0.18(13-I-2)
151248	0.44(12-I-2)	-0.54(13-II-2)	-0.29(2)	-0.19(13-I-2)	0.08(12-I-4)	0.15(13-II-4)
151249	0.44(12-I-2)	-0.52(13-II-2)	-0.29(2)	-0.18(13-I-2)	-0.10(12-I-2)	0.18(13-II-2)
151250	0.45(12-I-2)	-0.43(13-I-2)	-0.29(2)	-0.17(13-II-2)	0.08(12-I-2)	-0.27(13-I-2)
151251	0.44(12-I-2)	-0.98(13-II-2)	-0.20(2)	-0.11(13-I-2)	-0.08(2)	-1.80(13-II-2)
151262	0.49(12-I-4)	-0.58(13-II-4)	-0.08(2)	0.01(13-II-4)	0.24(2)	-0.19(12-I-3)
151263	0.56(12-I-4)	-0.42(13-II-4)	-0.20(2)	0.09(13-II-4)	0.33(12-I-4)	-0.20(12-I-3)
151264	0.59(12-I-4)	0.40(13-I-4)	-0.28(2)	0.08(13-II-4)	0.30(12-I-4)	-0.18(12-I-3)
151265	0.56(12-I-4)	0.40(13-I-4)	-0.29(2)	0.08(13-II-4)	0.28(12-I-4)	0.17(12-II-3)
151266	0.54(12-I-4)	0.44(13-I-4)	-0.29(2)	0.09(13-II-4)	0.29(12-I-4)	0.17(12-II-3)
151267	0.53(12-I-3)	0.42(13-I-2)	-0.29(2)	0.09(13-II-2)	0.26(12-I-3)	-0.17(12-I-3)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
151268	0.54(12-I-2)	0.41(13-I-2)	-0.29(2)	0.08(13-II-2)	0.24(12-I-2)	-0.17(12-I-3)
151269	0.55(12-I-2)	0.39(13-I-2)	-0.29(2)	0.07(13-II-2)	0.27(12-I-2)	0.17(12-II-3)
151270	0.55(12-I-2)	-0.35(13-II-2)	-0.26(2)	0.07(13-II-2)	-0.34(12-II-2)	0.25(13-II-2)
151271	-0.47(12-II-2)	-1.64(13-II-2)	-0.13(2)	0.01(12-II-1)	-0.19(2)	0.24(13-II-2)
151312	0.49(12-I-3)	-0.52(13-II-4)	-0.27(2)	0.14(13-II-4)	0.10(12-I-3)	0.13(13-I-2)
151313	0.47(12-I-3)	-0.51(13-II-4)	-0.29(2)	-0.15(13-I-4)	0.09(12-II-3)	0.24(13-I-4)
151314	0.47(12-I-3)	-0.55(13-II-4)	-0.29(2)	-0.16(13-I-4)	0.07(12-I-3)	0.19(13-I-4)
151315	0.46(12-I-3)	-0.57(13-II-3)	-0.29(2)	-0.17(13-I-3)	-0.08(12-I-3)	0.18(13-I-2)
151316	0.46(12-I-3)	-0.55(13-II-2)	-0.29(2)	-0.16(13-I-2)	0.08(12-I-3)	0.15(13-II-4)
151317	0.45(12-I-3)	-0.53(13-II-2)	-0.29(2)	-0.16(13-I-2)	-0.08(12-I-3)	0.18(13-II-2)
151318	0.46(12-I-3)	-0.43(13-I-2)	-0.29(2)	-0.14(13-II-2)	0.08(12-I-3)	-0.27(13-I-2)
151319	0.44(12-I-3)	-0.99(13-II-2)	-0.20(2)	-0.09(13-I-2)	-0.08(2)	-1.80(13-II-2)
151320	0.52(12-I-3)	-0.57(13-II-4)	-0.08(2)	-0.01(13-II-4)	0.24(2)	-0.18(12-I-1)
151321	0.57(12-I-3)	-0.42(13-II-4)	-0.20(2)	0.07(13-I-4)	0.30(12-I-4)	-0.18(12-I-1)
151322	0.62(12-I-3)	0.40(13-I-4)	-0.29(2)	0.09(13-I-4)	0.29(12-I-4)	-0.17(12-I-1)
151323	0.60(12-I-3)	0.39(13-I-4)	-0.29(2)	0.08(13-I-4)	0.28(12-I-3)	0.19(12-II-1)
151324	0.60(12-I-3)	0.43(13-I-4)	-0.29(2)	0.11(13-I-4)	0.31(12-I-3)	0.18(12-II-1)
151325	0.58(12-I-3)	0.42(13-I-2)	-0.29(2)	0.11(13-I-2)	0.29(12-I-3)	-0.17(12-I-1)
151326	0.59(12-I-3)	0.41(13-I-2)	-0.29(2)	0.09(13-I-2)	0.26(12-I-3)	-0.18(12-I-1)
151327	0.58(12-I-3)	0.39(13-I-2)	-0.29(2)	0.08(13-I-2)	0.27(12-I-3)	0.18(12-II-1)
151328	0.57(12-I-3)	-0.35(13-II-2)	-0.27(2)	0.07(13-II-2)	-0.32(12-II-2)	0.22(13-II-2)
151329	-0.50(12-II-3)	-1.64(13-II-2)	-0.13(2)	0.01(13-I-2)	-0.19(2)	0.23(13-II-2)
151380	0.49(12-I-3)	-0.51(13-II-4)	-0.27(2)	0.16(13-II-4)	0.09(12-I-3)	0.13(13-I-2)
151381	0.47(12-I-3)	-0.50(13-II-4)	-0.29(2)	0.15(13-II-4)	0.08(12-I-3)	0.24(13-I-4)
151382	0.47(12-I-3)	-0.55(13-II-4)	-0.29(2)	0.17(13-II-3)	0.07(12-I-3)	-0.19(13-II-4)
151383	0.46(12-I-3)	-0.58(13-II-3)	-0.29(2)	0.19(13-II-3)	-0.08(12-I-3)	0.17(13-I-2)
151384	0.46(12-I-3)	-0.55(13-II-2)	-0.29(2)	-0.18(13-I-3)	0.07(12-I-3)	0.15(13-II-4)
151385	0.46(12-I-3)	-0.52(13-II-2)	-0.29(2)	-0.16(13-I-2)	-0.08(12-I-3)	0.18(13-II-2)
151386	0.46(12-I-3)	-0.43(13-I-2)	-0.29(2)	-0.14(13-II-2)	0.07(12-I-3)	-0.28(13-I-2)
151387	0.44(12-I-3)	-0.98(13-II-2)	-0.20(2)	-0.10(13-I-3)	-0.08(2)	-1.79(13-II-2)
151388	0.43(12-I-3)	-0.58(13-II-4)	-0.08(2)	0.02(13-II-4)	0.23(2)	-0.29(12-II-3)
151389	0.48(12-I-3)	-0.42(13-II-4)	-0.20(2)	0.08(13-II-4)	0.27(12-I-3)	-0.32(12-I-3)
151390	0.52(12-I-3)	0.40(13-I-4)	-0.28(2)	0.08(13-II-4)	0.25(12-I-3)	-0.31(12-I-3)
151391	0.51(12-I-3)	-0.40(13-II-4)	-0.29(2)	0.08(13-II-4)	0.25(12-I-3)	0.32(12-II-3)
151392	0.51(12-I-3)	-0.44(13-II-4)	-0.29(2)	0.09(13-II-4)	0.28(12-I-3)	0.32(12-II-3)
151393	0.50(12-I-3)	-0.43(13-II-2)	-0.29(2)	0.09(13-II-3)	0.27(12-I-3)	-0.31(12-I-3)
151394	0.50(12-I-3)	-0.41(13-II-2)	-0.29(2)	0.08(13-II-2)	0.23(12-I-3)	-0.31(12-I-3)
151395	0.50(12-I-3)	0.39(13-I-2)	-0.29(2)	0.07(13-II-2)	0.24(12-I-3)	0.31(12-II-3)
151396	0.48(12-I-3)	-0.35(13-II-2)	-0.26(2)	0.07(13-II-2)	-0.28(12-II-3)	0.30(12-I-3)
151397	-0.41(12-II-3)	-1.64(13-II-2)	-0.13(2)	0.01(12-I-3)	-0.18(2)	0.26(13-II-2)
151452	0.44(12-I-3)	-0.51(13-II-4)	-0.25(2)	0.20(13-II-4)	0.10(12-I-3)	0.26(12-I-3)
151453	0.43(12-I-3)	-0.50(13-II-4)	-0.27(2)	0.22(13-II-3)	0.08(12-II-3)	-0.25(12-II-3)
151454	0.43(12-I-3)	-0.54(13-II-4)	-0.27(2)	0.25(13-II-3)	0.08(12-I-3)	-0.28(12-II-3)
151455	0.41(12-I-3)	-0.59(13-II-3)	-0.27(2)	0.28(13-II-3)	-0.05(12-I-3)	-0.25(12-II-3)
151456	0.42(12-I-3)	-0.54(13-II-2)	-0.27(2)	0.25(13-II-3)	0.08(12-I-3)	0.28(12-I-3)
151457	0.41(12-I-3)	-0.52(13-II-2)	-0.27(2)	0.23(13-II-3)	-0.07(12-I-3)	0.25(12-I-3)
151458	0.42(12-I-3)	-0.43(13-I-2)	-0.27(2)	0.19(13-I-2)	0.08(12-I-3)	-0.31(13-II-2)
151459	0.40(12-I-3)	-0.98(13-II-2)	-0.18(2)	0.14(13-II-3)	-0.07(2)	-1.80(13-II-2)
151460	1.34(12-I-3)	-0.58(13-II-4)	-0.05(2)	0.05(2)	0.16(2)	2.05(12-II-3)
151461	1.40(12-I-3)	-0.42(13-II-4)	-0.14(2)	0.13(2)	0.12(12-I-4)	2.16(12-II-3)
151462	1.41(12-I-3)	-0.39(13-II-4)	-0.19(2)	0.17(2)	0.08(12-I-4)	2.13(12-II-3)
151463	1.40(12-I-3)	-0.39(13-II-4)	-0.20(2)	0.18(2)	0.07(12-I-4)	2.14(12-II-3)
151464	1.40(12-I-3)	-0.43(13-II-4)	-0.20(2)	0.18(2)	0.09(12-I-3)	-2.15(12-I-3)
151465	1.39(12-I-3)	-0.42(13-II-3)	-0.20(2)	0.18(2)	0.09(12-I-3)	-2.16(12-I-3)
151466	1.40(12-I-3)	-0.41(13-II-2)	-0.20(2)	0.18(2)	0.07(12-I-3)	-2.15(12-I-3)
151467	1.40(12-I-3)	-0.38(13-II-2)	-0.20(2)	0.18(2)	0.07(12-I-3)	-2.15(12-I-3)
151468	1.39(12-I-3)	-0.35(13-II-2)	-0.18(2)	0.17(2)	-0.10(12-II-3)	-2.12(12-I-3)
151469	1.33(12-I-3)	-1.64(13-II-2)	-0.08(2)	0.08(2)	-0.12(2)	-2.00(12-I-3)
151482	2.05(12-I-3)	-0.42(13-II-4)	-0.12(2)	0.15(2)	0.02(2)	0.26(12-I-3)
151484	2.05(12-I-3)	-0.42(13-II-4)	-0.13(2)	0.18(2)	-0.02(12-I-3)	-0.26(12-II-3)
151486	2.05(12-I-3)	-0.46(13-II-4)	-0.13(2)	0.18(2)	-0.01(13-II-4)	-0.28(12-II-3)
151488	2.05(12-I-3)	-0.49(13-II-3)	-0.13(2)	0.19(13-II-3)	-0.01(12-I-3)	0.26(12-I-3)
151490	2.05(12-I-3)	-0.47(13-II-2)	-0.13(2)	0.18(2)	-0.01(13-I-4)	0.28(12-I-3)
151492	2.05(12-I-3)	-0.44(13-II-2)	-0.13(2)	0.18(2)	-0.01(12-I-3)	0.26(12-I-3)
151494	2.05(12-I-3)	-0.35(13-I-2)	-0.13(2)	0.17(2)	-0.01(13-I-2)	-0.28(13-II-2)
151496	2.05(12-I-3)	-0.96(13-II-2)	-0.09(2)	0.12(2)	-0.03(2)	-1.68(13-II-2)
160262	-0.08(12-II-1)	0.07(13-I-1)	-0.04(2)	-0.71(2)	0.24(2)	0.16(12-II-1)
160266	0.08(12-I-1)	0.10(13-I-1)	-0.07(2)	-1.05(2)	-0.05(12-II-1)	-0.19(12-I-1)
160270	-0.08(12-II-1)	0.10(13-I-1)	-0.07(2)	-1.04(2)	0.05(12-I-1)	0.19(12-II-1)
160274	0.08(12-I-1)	0.07(13-I-1)	-0.04(2)	-0.69(2)	-0.23(2)	-0.16(12-I-1)
160279	-0.08(12-II-1)	0.07(13-I-1)	-0.04(2)	-0.71(2)	0.08(2)	0.15(12-II-2)
160283	0.08(12-I-1)	0.07(13-I-1)	-0.05(2)	-0.73(2)	-0.07(13-II-1)	-0.15(12-I-4)
160290	0.07(12-I-1)	0.06(13-I-2)	-0.05(2)	-0.62(2)	-0.32(2)	-0.15(12-I-2)
160294	-0.07(12-II-1)	0.06(13-I-4)	-0.04(2)	-0.61(2)	0.32(2)	0.15(12-II-1)
160303	-0.08(12-II-1)	-0.06(13-II-2)	-0.04(2)	-0.70(2)	-0.06(13-I-2)	0.16(12-II-2)
160312	0.07(12-I-1)	-0.06(13-II-4)	-0.04(2)	-0.69(2)	0.06(13-I-4)	0.16(12-II-4)
160318	-0.25(12-II-1)	0.08(13-I-1)	-0.43(2)	-0.06(13-I-1)	0.71(2)	0.08(12-II-4)
160319	-0.25(12-II-1)	0.10(13-I-1)	-0.65(2)	-0.06(13-I-1)	-0.06(13-II-1)	-0.13(12-I-1)
160320	-0.25(12-II-1)	0.10(13-I-1)	-0.65(2)	-0.06(13-I-1)	0.05(13-II-1)	0.14(12-II-1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
160321	0.25(12-I-1)	0.07(13-I-1)	-0.42(2)	-0.06(2)	-0.67(2)	-0.07(12-II-2)
160323	0.25(12-I-1)	0.07(13-I-1)	-0.42(2)	-0.16(2)	0.68(2)	-0.08(12-I-2)
160324	-0.25(12-II-1)	0.07(13-I-1)	-0.44(2)	-0.17(2)	-0.70(2)	0.08(12-II-4)
160327	0.24(12-I-2)	0.07(13-I-2)	-0.42(2)	0.08(2)	-0.69(2)	-0.08(12-I-1)
160331	-0.24(12-II-1)	0.06(12-II-3)	-0.42(2)	0.09(2)	0.69(2)	0.08(12-II-1)
160333	0.08(12-I-2)	0.08(13-I-2)	-0.07(2)	-0.94(2)	-0.38(2)	-0.19(12-I-2)
160337	0.24(12-I-2)	0.07(12-I-2)	-0.41(2)	-0.29(2)	0.60(2)	-0.07(12-II-2)
160346	-0.08(12-II-4)	0.07(13-I-4)	-0.07(2)	-0.94(2)	0.39(2)	0.19(12-II-4)
160350	-0.24(12-II-1)	0.08(12-II-3)	-0.40(2)	-0.29(2)	-0.59(2)	0.08(12-II-1)
160351	-0.22(12-II-1)	0.08(13-I-1)	-0.05(2)	0.78(2)	0.14(12-II-1)	-0.08(12-II-1)
160354	0.22(12-I-1)	0.10(13-I-1)	-0.08(2)	1.14(2)	0.06(12-II-1)	0.07(12-I-1)
160357	-0.23(12-II-1)	0.10(13-I-1)	-0.08(2)	1.14(2)	-0.06(12-I-1)	-0.07(12-II-2)
160360	-0.22(12-II-1)	0.07(13-I-1)	-0.05(2)	0.76(2)	-0.15(12-I-1)	0.07(12-I-1)
160363	0.22(12-I-1)	0.07(13-I-1)	-0.05(2)	0.72(2)	0.34(2)	-0.08(12-II-1)
160367	-0.22(12-II-1)	0.07(13-I-1)	-0.05(2)	0.74(2)	-0.38(2)	0.08(12-I-1)
160378	0.21(12-I-2)	0.06(13-I-2)	-0.05(2)	0.79(2)	-0.12(12-I-1)	0.07(12-I-2)
160384	0.08(12-I-2)	-0.09(13-II-2)	-0.07(2)	-0.95(2)	-0.34(2)	0.19(12-I-2)
160388	0.25(12-I-2)	0.09(13-I-2)	-0.64(2)	-0.07(13-I-2)	-0.05(13-II-2)	-0.14(12-I-2)
160389	-0.22(12-II-1)	0.06(12-II-3)	-0.05(2)	0.79(2)	0.13(12-II-1)	-0.07(12-II-4)
160392	0.21(12-I-2)	0.07(13-I-2)	-0.05(2)	0.67(2)	0.38(2)	-0.07(12-II-2)
160396	-0.08(12-II-4)	-0.08(13-II-4)	-0.07(2)	-0.94(2)	0.35(2)	-0.18(12-I-4)
160400	-0.25(12-II-4)	0.08(13-I-4)	-0.64(2)	-0.06(13-I-1)	0.05(13-II-4)	0.14(12-II-4)
160401	-0.21(12-II-1)	0.08(12-II-3)	-0.05(2)	0.66(2)	-0.36(2)	0.07(12-I-4)
160418	0.09(12-I-2)	-0.08(13-II-3)	-0.05(2)	-0.53(2)	-0.44(2)	-0.16(12-I-2)
160422	0.25(12-I-2)	0.10(13-I-2)	-0.64(2)	-0.07(13-I-2)	0.06(13-I-1)	-0.13(12-I-2)
160424	0.22(12-I-2)	0.09(13-I-2)	-0.08(2)	1.07(2)	0.40(2)	0.07(12-I-1)
160429	-0.08(12-II-4)	-0.08(13-II-4)	-0.05(2)	-0.52(13-I-4)	0.45(2)	0.15(12-II-4)
160436	-0.25(12-II-4)	0.09(13-I-4)	-0.64(2)	-0.06(13-I-4)	-0.05(13-I-1)	0.14(12-II-4)
160437	-0.22(12-II-4)	0.08(13-I-4)	-0.08(2)	1.06(2)	-0.41(2)	-0.06(12-II-1)
160461	0.09(12-I-2)	-0.09(13-II-3)	-0.05(2)	-0.61(2)	-0.22(13-II-2)	-0.17(12-I-2)
160474	-0.08(12-II-4)	-0.08(13-II-4)	-0.04(2)	-0.70(2)	0.24(13-I-4)	-0.18(12-I-4)
160479	0.25(12-I-2)	-0.09(13-II-3)	-0.42(2)	0.19(2)	-0.69(2)	-0.09(12-II-2)
160481	0.22(12-I-2)	0.10(13-I-2)	-0.08(2)	1.07(2)	0.39(2)	-0.08(12-II-2)
160494	-0.24(12-II-4)	0.11(12-II-4)	-0.43(2)	0.20(2)	0.68(2)	0.09(12-II-4)
160495	-0.23(12-II-4)	0.09(13-I-4)	-0.08(2)	1.07(2)	-0.40(2)	0.08(12-I-4)
160511	0.24(12-I-2)	-0.11(12-II-2)	-0.43(2)	-0.44(2)	0.60(2)	-0.09(12-II-2)
160512	-0.23(12-II-4)	0.12(12-II-4)	-0.43(2)	-0.42(2)	-0.58(2)	0.09(12-II-4)
160518	0.11(12-I-2)	-0.10(13-II-2)	-0.05(2)	-0.50(13-I-3)	-0.51(2)	0.16(12-II-3)
160522	0.22(12-I-2)	0.09(13-I-3)	-0.05(2)	0.80(2)	0.19(12-II-2)	0.07(12-I-2)
160532	-0.12(12-II-3)	0.13(13-I-4)	-0.05(2)	-1.19(2)	0.78(2)	0.22(12-II-4)
160536	-0.22(12-II-4)	0.10(12-II-4)	-0.05(2)	0.81(2)	-0.18(12-I-4)	-0.07(12-II-4)
160546	0.22(12-I-2)	0.10(12-I-2)	-0.05(2)	0.60(2)	0.59(2)	-0.07(12-II-1)
160550	-0.21(12-II-4)	0.12(12-II-4)	-0.05(2)	0.61(2)	-0.56(2)	0.06(12-I-1)
160553	0.12(12-I-2)	0.15(13-I-3)	-0.05(2)	-0.85(13-I-3)	-0.53(13-I-3)	0.31(12-II-3)
160567	0.25(12-I-2)	-0.12(12-II-1)	-0.45(2)	0.32(2)	-0.63(2)	0.10(12-II-3)
160569	-0.25(12-II-4)	0.14(13-I-3)	-0.72(2)	-0.09(2)	-0.10(2)	-0.16(12-I-4)
160590	-0.23(12-II-2)	0.17(12-II-2)	-0.46(2)	-0.55(2)	0.51(2)	0.21(12-II-3)
160592	0.48(13-I-4)	0.79(13-I-4)	-0.04(2)	-0.25(12-II-4)	0.85(2)	-0.30(12-I-4)
160597	0.23(12-I-2)	0.12(12-I-1)	-0.05(2)	0.86(2)	0.26(12-II-2)	0.12(12-II-2)
160600	-0.24(12-II-4)	0.14(13-I-4)	-0.08(2)	1.10(2)	-0.68(2)	-0.21(13-I-4)
160621	-0.22(12-II-2)	0.16(12-II-2)	-0.05(2)	0.54(2)	0.62(2)	0.31(12-II-3)
160630	-0.77(12-II-3)	0.90(12-II-3)	-0.03(2)	-0.41(12-II-3)	-0.74(2)	0.42(12-II-3)
160631	0.49(13-I-4)	0.78(13-I-4)	-0.31(2)	0.83(2)	1.43(2)	-0.22(12-I-4)
160632	0.50(13-I-4)	0.78(13-I-4)	-0.18(2)	0.70(2)	1.38(2)	-0.23(12-I-4)
160656	-0.79(12-II-3)	0.91(12-II-3)	-0.31(2)	1.06(2)	-1.14(2)	0.22(12-II-2)
160665	0.49(13-I-4)	0.78(13-I-4)	-0.05(2)	0.83(2)	0.19(2)	-0.13(13-I-4)
160667	0.50(13-I-4)	0.78(13-I-4)	0.04(2)	0.82(2)	0.26(2)	-0.09(12-I-3)
160681	-0.79(12-II-3)	0.90(12-II-3)	-0.04(2)	0.76(2)	-0.23(12-II-3)	0.41(12-II-3)
170192	-0.25(12-II-1)	0.14(13-I-1)	-0.05(2)	-0.77(2)	0.22(2)	-0.06(12-I-1)
170195	0.25(12-I-1)	0.21(13-I-1)	-0.07(2)	-1.05(2)	-0.10(12-I-1)	0.10(12-II-1)
170198	0.25(12-I-1)	0.20(13-I-1)	-0.07(2)	-1.04(2)	0.10(12-II-1)	-0.11(12-I-1)
170201	0.25(12-I-1)	0.13(13-I-1)	-0.05(2)	-0.74(2)	-0.22(2)	0.07(12-II-1)
170211	0.24(12-I-1)	0.12(13-I-1)	-0.05(2)	-0.77(2)	0.12(12-II-1)	-0.07(12-I-2)
170214	0.25(12-I-1)	0.13(13-I-1)	-0.05(2)	-0.80(2)	-0.11(12-I-1)	0.06(12-II-4)
170217	0.24(12-I-1)	0.10(13-I-2)	-0.05(2)	-0.69(2)	-0.33(2)	0.07(12-II-2)
170221	-0.25(12-II-1)	0.10(13-I-4)	-0.05(2)	-0.68(2)	0.33(2)	0.05(12-II-1)
170228	0.23(12-I-1)	-0.11(13-II-2)	-0.05(2)	-0.74(2)	-0.10(12-I-1)	-0.08(12-I-2)
170234	-0.24(12-II-1)	-0.12(13-II-4)	-0.05(2)	-0.74(2)	0.10(12-II-1)	0.05(12-II-1)
170237	0.30(12-I-1)	0.14(13-I-1)	-0.47(2)	-0.08(13-II-1)	0.72(2)	-0.15(12-II-1)
170238	0.31(12-I-1)	0.21(13-I-1)	-0.65(2)	-0.10(13-II-1)	-0.09(13-I-1)	0.14(12-I-1)
170239	0.31(12-I-1)	0.20(13-I-1)	-0.65(2)	-0.10(13-II-1)	0.09(13-I-1)	0.13(12-I-1)
170240	0.30(12-I-1)	0.13(13-I-1)	-0.45(2)	-0.07(13-II-2)	-0.73(2)	0.14(12-I-1)
170242	0.30(12-I-1)	0.12(13-I-1)	-0.46(2)	-0.17(2)	0.76(2)	-0.14(12-II-1)
170244	-0.30(12-II-1)	0.12(13-I-1)	-0.48(2)	-0.17(2)	-0.75(2)	0.15(12-I-1)
170245	0.29(12-I-1)	0.11(13-I-2)	-0.46(2)	0.10(2)	-0.77(2)	0.13(12-I-1)
170247	-0.29(12-II-1)	-0.10(13-II-4)	-0.46(2)	0.11(2)	0.78(2)	-0.14(12-II-1)
170251	0.23(12-I-2)	0.15(13-I-2)	-0.07(2)	-0.95(2)	-0.37(2)	0.12(12-II-2)
170254	0.28(12-I-1)	-0.12(13-II-2)	-0.45(2)	-0.31(2)	0.66(2)	-0.13(12-II-1)
170258	-0.26(12-II-4)	0.16(13-I-4)	-0.07(2)	-0.95(2)	0.38(2)	-0.09(12-I-4)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
170261	-0.28(12-II-1)	-0.12(13-II-4)	-0.44(2)	-0.32(2)	-0.66(2)	0.14(12-I-1)
170262	0.10(12-I-1)	0.13(13-I-1)	-0.05(2)	0.83(2)	0.18(2)	0.17(12-I-1)
170266	0.10(12-I-1)	0.20(13-I-1)	-0.07(2)	1.20(13-II-1)	-0.08(12-II-1)	-0.22(12-II-1)
170270	-0.10(12-II-1)	0.20(13-I-1)	-0.07(2)	1.18(13-II-1)	0.08(12-I-1)	0.22(12-I-1)
170274	-0.10(12-II-1)	0.13(13-I-1)	-0.05(2)	0.81(2)	-0.19(2)	-0.16(12-II-1)
170279	0.10(12-I-1)	0.12(13-I-1)	-0.05(2)	0.78(2)	0.39(2)	-0.17(12-II-1)
170283	-0.09(12-II-1)	0.12(13-I-1)	-0.05(2)	0.81(2)	-0.41(2)	0.18(12-I-1)
170290	0.09(12-I-1)	-0.10(13-II-2)	-0.05(2)	0.87(2)	-0.09(12-II-1)	-0.16(12-II-1)
170294	-0.09(12-II-1)	-0.10(13-II-1)	-0.05(2)	0.87(2)	0.09(2)	0.16(12-I-1)
170299	0.23(12-I-2)	-0.18(13-II-2)	-0.07(2)	-0.96(2)	-0.36(2)	-0.11(12-I-2)
170302	0.29(12-I-2)	-0.16(13-II-2)	-0.65(2)	-0.09(13-II-2)	-0.08(13-I-2)	0.12(12-I-1)
170303	0.10(12-I-1)	-0.11(13-II-2)	-0.05(2)	0.71(2)	0.46(2)	-0.15(12-II-1)
170308	-0.27(12-II-4)	-0.17(13-II-3)	-0.07(2)	-0.97(2)	0.38(2)	0.07(12-II-1)
170311	-0.29(12-II-4)	-0.16(13-II-4)	-0.65(2)	-0.09(13-II-4)	0.07(13-II-4)	-0.14(12-II-4)
170312	-0.09(12-II-1)	-0.10(13-II-4)	-0.05(2)	0.70(2)	-0.45(2)	0.15(12-I-1)
170328	0.23(12-I-2)	-0.15(13-I-2)	-0.05(2)	-0.71(2)	-0.50(2)	-0.10(12-I-2)
170332	0.30(12-I-2)	-0.19(13-II-2)	-0.65(2)	-0.11(13-II-2)	0.07(13-I-1)	0.12(12-I-1)
170333	0.11(12-I-2)	-0.15(13-II-2)	-0.07(2)	1.12(2)	0.39(2)	-0.21(12-II-1)
170339	-0.26(12-II-4)	-0.16(13-II-4)	-0.05(2)	-0.70(2)	0.49(2)	-0.04(12-I-4)
170344	-0.30(12-II-4)	-0.17(13-II-3)	-0.66(2)	-0.10(13-II-4)	-0.08(13-II-4)	-0.16(12-II-4)
170346	-0.11(12-II-4)	-0.14(13-II-4)	-0.07(2)	1.12(2)	-0.40(2)	0.21(12-I-1)
170370	0.24(12-I-2)	-0.18(13-II-3)	-0.04(2)	-0.93(2)	-0.33(2)	-0.11(12-I-2)
170373	-0.25(12-II-4)	0.14(13-I-4)	-0.04(2)	-0.63(2)	0.34(2)	-0.18(13-I-4)
170381	0.29(12-I-2)	-0.16(13-II-3)	-0.49(2)	0.19(2)	-0.67(2)	0.12(12-I-1)
170384	0.11(12-I-2)	-0.18(13-II-2)	-0.07(2)	1.12(2)	0.45(2)	0.21(12-I-2)
170395	-0.28(12-II-4)	-0.16(13-II-4)	-0.49(2)	0.21(2)	0.71(2)	-0.16(12-II-4)
170396	-0.11(12-II-4)	-0.16(13-II-4)	-0.07(2)	1.13(2)	-0.46(2)	-0.22(12-II-4)
170413	0.29(12-I-2)	-0.20(13-II-3)	-0.52(2)	-0.46(2)	0.65(2)	-0.12(12-II-1)
170414	0.31(12-I-4)	0.34(13-I-4)	-0.04(2)	-0.48(13-I-4)	-0.36(13-II-4)	-0.23(13-I-4)
170416	-0.27(12-II-4)	-0.14(13-II-4)	-0.43(2)	-0.27(2)	-0.34(2)	-0.15(12-II-4)
170418	0.11(12-I-2)	-0.14(13-I-2)	-0.05(2)	0.95(2)	0.21(13-I-2)	-0.15(12-II-2)
170429	-0.10(12-II-4)	-0.15(13-II-4)	-0.05(2)	0.96(2)	-0.21(13-II-4)	-0.15(12-II-4)
170433	0.27(12-I-2)	-0.19(13-II-2)	-0.04(2)	-0.69(2)	-0.59(2)	0.16(13-I-3)
170442	0.31(12-I-4)	0.29(13-I-3)	-0.30(2)	0.16(13-II-4)	-0.53(2)	-0.16(13-I-4)
170461	0.13(12-I-2)	-0.17(13-I-2)	-0.05(2)	0.78(2)	0.72(2)	-0.15(12-II-1)
170474	0.11(12-I-4)	-0.13(13-II-4)	-0.05(2)	0.57(2)	-0.52(2)	-0.16(12-II-1)
170480	-0.28(12-II-2)	0.31(13-I-3)	-0.07(2)	-0.44(13-I-3)	-0.27(13-I-3)	0.34(12-II-3)
170484	0.32(12-I-2)	-0.20(13-II-2)	-0.51(2)	0.37(2)	-0.72(2)	0.14(12-I-1)
170507	0.47(12-I-4)	0.77(13-I-4)	-0.03(2)	-0.36(12-II-4)	0.69(2)	-0.22(13-I-4)
170510	0.33(12-I-4)	0.27(13-I-3)	-0.05(2)	0.36(2)	0.07(12-I-4)	-0.27(12-I-4)
170517	-0.33(12-II-2)	0.30(13-I-3)	-0.45(2)	-0.47(2)	0.41(2)	0.24(12-II-3)
170518	0.16(12-I-2)	-0.18(13-II-2)	-0.06(2)	1.04(2)	0.34(12-I-2)	0.18(12-I-1)
170532	0.20(12-I-3)	0.25(13-I-4)	-0.06(2)	-0.37(13-I-4)	0.25(13-I-4)	-0.31(12-I-4)
170545	0.48(12-I-4)	0.76(13-I-4)	-0.31(2)	-0.07(12-II-3)	0.49(2)	-0.17(12-I-4)
170549	0.49(12-I-4)	0.77(13-I-4)	-0.21(2)	0.14(12-I-3)	0.61(2)	-0.15(12-II-4)
170553	-0.21(12-II-2)	0.27(13-I-3)	-0.05(2)	0.72(13-II-3)	0.61(13-I-3)	0.41(12-II-3)
170566	-0.81(12-II-3)	0.98(12-II-3)	-0.04(2)	0.48(12-I-3)	-0.51(13-I-3)	0.36(12-II-3)
170575	0.49(13-I-4)	0.73(13-I-4)	-0.32(2)	0.29(2)	0.30(2)	-0.37(12-I-4)
170591	-0.83(12-II-3)	0.98(12-II-3)	-0.22(2)	1.04(2)	-1.20(2)	0.22(12-II-2)
170592	0.51(13-I-4)	0.77(13-I-4)	-0.04(2)	0.44(12-I-3)	0.58(2)	-0.29(12-II-4)
170630	-0.83(12-II-3)	0.94(12-II-3)	-0.04(2)	0.60(2)	-0.23(12-II-3)	0.50(12-II-3)
180141	-0.76(12-II-1)	-0.28(12-II-1)	-0.12(13-I-1)	-0.52(13-II-1)	1.08(2)	-1.08(12-I-1)
180144	-0.95(12-II-1)	-0.37(12-I-1)	0.06(13-I-4)	-0.49(2)	-0.58(12-II-1)	0.15(13-II-1)
180145	-0.06(12-II-1)	0.11(13-I-1)	-0.07(2)	0.59(13-II-1)	0.13(12-I-1)	-0.21(12-I-1)
180146	0.06(12-I-1)	0.15(13-I-1)	-0.08(2)	-0.76(13-I-1)	-0.11(12-II-1)	0.22(12-II-1)
180147	-0.06(12-II-1)	0.15(13-I-1)	-0.08(2)	-0.75(13-I-1)	0.11(12-I-1)	-0.23(12-I-1)
180150	0.06(12-I-1)	0.10(13-I-1)	-0.06(2)	0.54(13-II-1)	-0.14(12-II-1)	0.20(12-II-1)
180154	-0.06(12-II-1)	0.09(13-I-2)	-0.06(2)	-0.54(13-I-2)	0.13(12-I-1)	-0.20(12-I-1)
180158	0.95(12-I-1)	-0.35(12-II-1)	-0.07(2)	-0.79(12-I-1)	-1.50(12-II-1)	-0.37(13-I-1)
180162	0.07(12-I-1)	0.10(13-I-1)	-0.07(2)	-0.57(13-I-1)	-0.13(13-II-4)	0.22(12-II-4)
180164	-0.95(12-II-1)	-0.37(12-I-1)	-0.06(2)	-0.89(12-II-1)	1.51(12-I-1)	0.54(12-I-1)
180165	-0.06(12-II-1)	-0.09(13-II-2)	-0.06(2)	-0.60(13-I-2)	-0.21(13-I-2)	-0.18(12-I-1)
180168	0.07(12-I-4)	-0.08(13-II-4)	-0.06(2)	-0.58(13-I-4)	0.22(13-I-4)	0.20(12-II-1)
180169	0.23(12-I-1)	0.11(13-I-1)	-0.39(2)	-0.18(2)	0.62(2)	0.14(12-II-1)
180170	0.23(12-I-1)	0.15(13-I-1)	-0.51(2)	-0.18(2)	-0.09(13-II-2)	-0.16(12-I-1)
180171	0.22(12-I-1)	0.15(13-I-1)	-0.51(2)	-0.18(2)	0.10(13-II-4)	0.16(12-II-1)
180172	-0.21(12-II-1)	0.10(13-I-1)	-0.38(2)	-0.17(2)	-0.67(2)	-0.13(12-I-1)
180173	-0.06(12-II-1)	-0.11(13-II-2)	-0.06(2)	-0.78(13-I-2)	0.20(13-II-2)	-0.19(12-I-1)
180174	-0.57(12-II-4)	0.25(12-II-4)	-0.01(2)	-1.11(2)	-0.26(12-II-4)	-1.43(12-I-4)
180176	0.07(12-I-4)	-0.11(13-II-4)	-0.06(2)	-0.78(13-I-4)	-0.20(13-II-4)	0.22(12-II-4)
180179	0.49(12-I-1)	-0.18(12-II-2)	-0.54(2)	-1.72(2)	2.46(2)	1.07(12-I-1)
180180	-0.21(12-II-1)	0.09(13-I-1)	-0.39(2)	-0.28(2)	0.69(2)	-0.13(12-I-1)
180182	-0.57(12-II-4)	0.24(12-II-4)	-0.12(2)	-2.74(2)	1.35(2)	-0.75(12-I-3)
180183	0.23(12-I-1)	0.10(13-I-1)	-0.41(2)	-0.28(2)	-0.64(2)	0.14(12-II-1)
180184	-0.51(12-II-4)	-0.19(12-I-4)	-0.65(2)	-2.03(2)	-2.21(2)	-0.99(12-II-1)
180185	-0.75(12-II-1)	0.56(12-II-1)	-0.02(2)	0.38(12-I-1)	0.28(12-I-1)	-1.48(12-I-4)
180186	-0.74(12-II-1)	-0.27(12-II-1)	-0.04(2)	-1.49(2)	-1.83(2)	0.42(12-I-1)
180187	0.20(12-I-1)	0.08(13-I-2)	-0.41(2)	-0.06(13-II-2)	-0.72(2)	-0.14(12-I-1)
180188	0.23(12-I-4)	0.09(13-I-4)	-0.41(2)	0.05(13-I-4)	0.73(2)	0.14(12-II-1)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
180189	-0.07(12-II-2)	-0.14(13-II-2)	-0.07(2)	-0.91(13-I-2)	-0.38(13-I-2)	-0.17(12-I-1)
180190	0.19(12-I-1)	-0.10(13-II-2)	-0.41(2)	-0.37(2)	0.60(2)	-0.13(12-I-1)
180192	0.22(12-I-1)	0.10(13-I-1)	-0.06(2)	0.68(2)	0.16(2)	-0.04(12-II-1)
180195	0.22(12-I-1)	0.14(13-I-1)	-0.08(2)	0.94(13-I-1)	-0.07(12-I-1)	0.05(13-I-1)
180198	-0.22(12-II-1)	0.14(13-I-1)	-0.08(2)	0.94(13-I-1)	0.08(12-II-1)	-0.06(13-I-1)
180201	0.22(12-I-1)	0.10(13-I-1)	-0.05(2)	0.65(2)	-0.18(2)	0.04(13-II-1)
180204	0.09(12-I-4)	-0.13(13-II-4)	-0.07(2)	-0.94(13-I-4)	0.40(13-I-4)	0.22(12-II-4)
180207	-0.22(12-II-4)	-0.11(13-II-4)	-0.41(2)	-0.38(2)	-0.61(2)	0.14(12-II-1)
180208	-0.54(12-I-4)	0.34(13-I-4)	-0.02(2)	-0.72(2)	1.14(2)	-0.22(12-II-1)
180209	-0.49(12-II-4)	0.22(12-II-4)	-1.69(2)	-1.88(2)	1.65(2)	-0.32(12-II-4)
180210	-0.30(12-II-4)	-0.13(13-II-4)	-0.60(2)	0.29(13-I-4)	-2.90(2)	-0.55(12-II-4)
180211	0.21(12-I-1)	0.09(13-I-1)	-0.05(2)	0.64(2)	0.33(2)	-0.05(12-II-1)
180214	0.22(12-I-1)	0.10(13-I-1)	-0.06(2)	0.67(2)	-0.34(2)	0.05(12-I-1)
180217	0.21(12-I-1)	0.08(13-I-2)	-0.05(2)	0.76(2)	-0.12(12-I-1)	0.04(13-II-2)
180220	-0.47(12-II-1)	0.18(12-I-2)	-0.98(2)	0.67(2)	-1.06(2)	-0.48(12-II-2)
180221	-0.22(12-II-4)	0.08(13-I-4)	-0.05(2)	0.76(2)	0.11(12-II-1)	-0.04(12-II-4)
180224	-0.07(12-II-2)	-0.14(13-II-2)	-0.07(2)	-0.37(13-I-2)	0.31(2)	-0.17(12-II-2)
180227	0.17(12-I-2)	-0.13(13-II-2)	-0.57(2)	-0.13(13-II-2)	-0.15(2)	-0.15(12-I-2)
180228	0.21(12-I-1)	-0.10(13-II-2)	-0.05(2)	0.65(2)	0.43(2)	-0.07(13-II-3)
180231	-0.49(12-II-4)	0.34(13-I-4)	-0.02(2)	-1.37(2)	1.67(2)	-0.51(13-I-4)
180232	0.10(12-I-4)	-0.12(13-II-4)	-0.08(2)	-0.24(13-II-4)	-0.36(2)	-0.21(12-II-1)
180233	0.24(12-I-4)	-0.14(13-II-4)	-0.56(2)	-0.13(13-II-4)	0.16(2)	0.16(12-II-1)
180234	-0.22(12-II-4)	-0.10(13-II-4)	-0.05(2)	0.64(2)	-0.43(2)	0.05(13-II-3)
180241	-0.29(12-II-4)	0.15(12-II-4)	-1.56(2)	2.69(2)	-0.57(2)	-0.40(12-II-4)
180243	-0.63(12-II-1)	0.39(12-I-2)	-0.03(2)	-1.94(2)	-1.34(2)	-0.38(12-II-1)
180246	-0.43(12-II-4)	0.27(12-II-4)	-0.84(2)	-0.20(2)	2.21(2)	-0.42(12-II-4)
180248	0.07(12-I-2)	0.09(13-II-2)	-0.07(2)	0.74(2)	0.08(12-II-2)	0.29(12-I-2)
180250	0.16(12-I-2)	-0.13(13-II-2)	-0.53(2)	-0.18(2)	0.08(13-II-1)	0.15(12-II-2)
180251	0.20(12-I-2)	0.13(13-I-2)	-0.07(2)	0.94(2)	0.34(2)	0.07(12-I-2)
180255	-0.41(12-II-1)	0.28(12-I-2)	-0.87(2)	-1.17(2)	-0.23(2)	-0.75(12-II-1)
180256	-0.10(12-II-4)	-0.11(13-II-4)	-0.07(2)	1.59(2)	-0.12(2)	-0.19(13-I-4)
180257	0.24(12-I-4)	-0.13(13-II-4)	-0.50(2)	-0.20(2)	0.08(13-I-4)	-0.16(12-I-4)
180258	-0.23(12-II-4)	0.13(13-I-4)	-0.07(2)	0.93(2)	-0.35(2)	-0.05(13-II-4)
180278	-0.34(12-II-4)	0.22(13-I-4)	-0.95(2)	0.42(2)	0.36(2)	-0.62(12-II-4)
180287	0.43(12-I-4)	0.62(13-I-4)	-0.02(2)	-0.93(2)	1.67(2)	-0.56(13-I-4)
180288	0.28(12-I-4)	0.18(13-I-4)	-0.75(2)	1.79(2)	-0.35(2)	-0.43(12-II-4)
180289	-0.09(12-II-2)	0.16(13-II-2)	-0.68(2)	1.21(2)	1.18(2)	0.54(12-I-2)
180298	-0.15(12-II-2)	0.10(13-II-2)	-0.28(2)	0.14(2)	-0.88(2)	0.14(12-II-2)
180299	0.20(12-I-2)	-0.13(13-II-2)	-0.07(2)	0.89(2)	0.33(2)	-0.09(12-II-2)
180307	0.22(12-I-4)	0.13(12-II-4)	-0.16(2)	-0.08(13-I-4)	1.02(2)	0.14(12-II-4)
180308	0.24(12-I-4)	0.12(13-I-4)	-0.07(2)	0.82(2)	-0.31(2)	0.08(13-II-4)
180316	-0.61(12-II-1)	0.39(12-I-2)	-0.03(2)	-1.18(2)	-1.33(2)	-0.34(12-II-2)
180317	0.39(12-I-4)	0.56(13-I-4)	-0.77(2)	-0.76(2)	1.28(2)	-0.45(13-I-4)
180322	0.17(12-I-4)	0.12(13-I-4)	-0.06(2)	0.10(13-II-4)	-1.26(2)	-0.32(13-I-4)
180325	-0.15(12-II-2)	0.16(13-II-2)	-0.04(2)	0.58(2)	0.79(2)	-0.20(12-I-2)
180328	0.19(12-I-2)	0.10(13-I-2)	-0.05(2)	0.44(2)	-0.11(12-I-2)	0.09(12-I-2)
180338	0.50(13-I-4)	0.76(13-I-4)	-0.02(2)	-0.58(2)	1.95(2)	0.28(12-I-1)
180339	0.23(12-I-4)	0.14(12-II-4)	-0.05(2)	0.33(2)	0.13(12-II-4)	-0.04(13-I-4)
180342	0.35(12-I-3)	0.51(13-I-4)	-1.07(2)	-0.84(2)	-0.52(2)	-0.65(13-I-4)
180343	0.24(12-I-4)	0.13(13-I-4)	-0.13(2)	-0.66(2)	-0.75(2)	-0.20(12-I-1)
180345	-0.40(12-II-2)	0.27(12-I-2)	-0.58(2)	0.23(2)	-0.19(13-II-3)	-0.62(12-II-2)
180355	0.48(13-I-4)	0.76(13-I-4)	-0.66(2)	0.26(2)	-0.93(2)	-0.33(12-II-4)
180366	0.50(13-I-4)	0.75(13-I-4)	-0.34(2)	-0.55(2)	2.34(2)	0.36(12-I-1)
180370	-0.21(12-II-2)	0.17(13-II-2)	-0.04(2)	-0.45(2)	0.05(12-II-2)	0.10(12-I-2)
180373	0.25(12-I-4)	0.13(13-I-4)	-0.04(2)	0.27(13-II-4)	-0.16(13-II-4)	0.10(12-II-4)
180376	0.55(12-I-2)	-0.57(12-II-2)	-0.04(2)	-2.64(2)	-1.99(2)	-0.45(12-I-2)
180377	0.49(13-I-4)	0.75(13-I-4)	-0.63(2)	-0.12(2)	2.25(2)	0.36(12-I-1)
180382	-0.17(12-II-2)	0.16(13-I-3)	-0.06(2)	0.60(2)	0.60(2)	-0.40(12-II-2)
180404	0.50(13-I-4)	0.76(13-I-4)	-0.03(2)	-0.23(13-I-3)	2.08(2)	0.31(12-I-1)
180410	0.48(13-I-4)	0.76(13-I-4)	-0.87(2)	0.60(2)	0.95(2)	-0.22(12-II-1)
180411	0.44(12-I-3)	-0.43(13-II-3)	-1.45(2)	-2.32(2)	-0.47(2)	-0.61(12-II-2)
180414	0.32(12-I-4)	0.40(13-I-4)	-0.05(2)	-0.55(13-I-4)	-0.54(2)	-0.89(13-I-4)
180417	0.49(13-I-4)	0.77(13-I-4)	-0.46(2)	0.05(12-I-3)	1.67(2)	0.26(12-I-1)
180433	-0.23(12-II-2)	0.17(13-I-2)	-0.04(2)	-0.06(12-II-2)	-0.29(2)	-0.21(13-II-3)
180441	0.49(13-I-4)	0.77(13-I-4)	-0.10(2)	-0.09(12-II-3)	1.75(2)	-0.27(12-I-1)
180444	0.31(12-I-3)	-0.36(13-II-3)	-1.36(2)	0.57(2)	2.73(2)	-0.40(12-II-2)
180465	-1.06(12-II-3)	-0.98(12-I-2)	-0.02(2)	-1.34(2)	-2.40(2)	-0.50(12-I-2)
180478	0.49(13-I-4)	0.77(13-I-4)	-0.63(2)	0.24(2)	0.81(2)	0.22(12-I-1)
180480	0.33(12-I-2)	-0.37(13-II-3)	-0.08(2)	1.68(2)	1.63(2)	0.29(12-II-3)
180507	0.53(12-I-4)	0.77(13-I-4)	-0.03(2)	0.39(12-I-3)	1.07(2)	-0.19(12-I-1)
180509	-0.99(12-II-3)	0.88(12-II-2)	-1.11(2)	0.46(13-I-3)	-2.69(2)	-0.71(12-II-2)
180525	0.85(12-I-3)	0.90(12-II-3)	-1.09(2)	2.73(2)	-0.57(13-I-3)	0.51(12-I-1)
180566	-0.81(12-II-3)	-0.94(12-I-3)	-0.05(2)	2.04(2)	1.07(2)	0.38(13-I-3)
190093	-1.34(12-II-1)	-0.59(12-I-1)	-8.15(2)	10.39(2)	-4.31(2)	0.20(13-I-4)
190094	-1.34(12-II-1)	-0.63(12-I-1)	-4.64(2)	7.84(2)	-5.10(2)	-0.13(12-II-2)
190095	-1.34(12-II-1)	-0.35(12-I-1)	-0.50(13-I-4)	1.57(13-I-4)	-2.07(2)	-0.19(12-II-1)
190096	-1.33(12-II-1)	-0.37(13-II-1)	0.44(2)	-3.58(2)	0.40(2)	-0.42(12-II-1)
190097	-1.32(12-II-1)	-0.37(13-II-1)	-0.05(2)	-4.95(2)	0.44(12-I-1)	-0.36(12-II-1)
190098	-1.32(12-II-1)	-0.44(13-II-1)	-0.06(2)	-5.56(2)	-0.30(12-II-1)	-0.29(12-II-1)

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
190099	-1.32(12-II-1)	-0.44(13-II-1)	-0.06(2)	-5.55(2)	0.30(12-I-1)	0.28(12-I-1)
190101	-1.32(12-II-1)	-0.34(13-II-1)	-0.05(2)	-4.80(2)	-0.45(12-II-1)	0.36(12-I-1)
190103	-1.33(12-II-1)	-0.36(12-II-1)	0.36(2)	-3.87(2)	-0.41(2)	0.40(12-I-1)
190104	-1.34(12-II-1)	-0.35(13-II-2)	0.36(13-II-2)	1.07(13-I-2)	1.58(2)	0.18(12-I-1)
190105	-1.34(12-II-1)	-0.64(12-II-1)	-4.09(2)	7.31(2)	5.36(2)	0.12(12-I-4)
190106	-1.34(12-II-1)	-0.64(12-II-2)	-8.91(2)	11.09(2)	4.69(2)	-0.22(12-I-2)
190107	-1.27(12-II-1)	-0.36(12-II-2)	-0.06(2)	-4.11(2)	-0.38(12-II-1)	0.46(12-I-1)
190109	-1.26(12-II-1)	-0.38(13-II-1)	-0.06(2)	-4.01(2)	0.39(12-I-1)	-0.48(12-II-1)
190110	-1.36(12-II-1)	-0.61(12-II-1)	-7.14(2)	11.13(2)	3.74(2)	0.18(13-II-1)
190111	-1.32(12-II-1)	-0.63(12-II-1)	-1.62(2)	6.24(2)	4.76(2)	0.24(12-I-1)
190112	-1.30(12-II-1)	-0.61(12-I-1)	-1.84(2)	6.66(2)	-4.75(2)	-0.24(12-II-1)
190113	-1.27(12-II-1)	-0.35(13-II-2)	-0.08(2)	-1.81(2)	-0.51(2)	0.29(12-I-1)
190115	-1.25(12-II-1)	-0.34(13-II-4)	-0.09(2)	-1.52(13-II-4)	0.44(2)	-0.30(12-II-1)
190116	-1.35(12-II-1)	-0.59(12-I-1)	-5.61(2)	9.90(2)	-2.90(2)	-0.19(13-II-1)
190117	-1.06(12-II-1)	-0.37(13-II-1)	-2.20(2)	-3.34(2)	0.64(2)	-0.67(12-II-1)
190118	-1.07(12-II-1)	-0.44(13-II-1)	-2.45(2)	-3.67(2)	0.12(13-II-1)	-0.64(12-II-1)
190119	-1.07(12-II-1)	-0.44(13-II-1)	-2.45(2)	-3.66(2)	-0.15(13-II-1)	-0.64(12-II-1)
190120	-1.06(12-II-1)	-0.34(13-II-1)	-2.12(2)	-3.21(2)	-0.77(2)	-0.66(12-II-1)
190121	-1.04(12-II-1)	-0.35(13-II-2)	-1.99(2)	-3.14(2)	-0.21(13-II-2)	-0.61(12-II-1)
190122	-1.03(12-II-1)	-0.37(13-II-1)	-2.02(2)	-3.20(2)	0.44(2)	-0.60(12-II-1)
190123	-1.20(12-II-1)	-0.58(12-II-1)	-0.11(2)	1.42(13-I-2)	0.83(2)	0.42(12-I-1)
190124	-1.18(12-II-1)	-0.57(12-I-1)	-0.11(2)	1.44(2)	-0.87(2)	-0.39(12-II-1)
190126	-1.33(12-II-1)	-0.60(12-II-1)	-2.84(2)	10.29(2)	2.38(2)	0.28(12-I-1)
190127	-1.31(12-II-1)	-0.59(12-I-1)	-2.23(2)	9.02(2)	-1.82(2)	-0.28(12-II-1)
190128	-1.04(12-II-1)	-0.35(13-II-2)	-1.50(2)	-2.54(2)	-1.65(2)	-0.64(12-II-1)
190129	-1.02(12-II-1)	-0.33(13-II-4)	-1.40(2)	-2.47(2)	1.69(2)	-0.63(12-II-1)
190130	-0.60(12-II-1)	-0.36(13-II-1)	-2.15(2)	3.43(2)	0.39(2)	-0.88(12-II-1)
190131	-0.60(12-II-1)	-0.44(13-II-1)	-2.39(2)	3.84(2)	0.14(13-II-1)	-0.91(12-II-1)
190132	-0.60(12-II-1)	-0.44(13-II-1)	-2.39(2)	3.83(2)	-0.16(13-II-1)	-0.91(12-II-1)
190133	-0.59(12-II-1)	-0.34(13-II-1)	-2.07(2)	3.32(2)	-0.55(2)	-0.89(12-II-1)
190134	0.58(12-I-1)	-0.35(13-II-2)	-1.97(2)	2.99(2)	0.93(2)	-0.89(12-II-1)
190135	-0.98(12-II-1)	-0.50(12-II-1)	-0.88(2)	-2.56(2)	-0.75(2)	-0.61(12-II-1)
190136	-0.58(12-II-1)	-0.36(13-II-1)	-2.02(2)	3.06(2)	-0.84(2)	0.89(12-I-1)
190137	-1.20(12-II-1)	-0.55(12-II-1)	-0.14(2)	1.93(2)	0.96(2)	0.31(12-I-1)
190138	-0.97(12-II-1)	-0.49(12-I-1)	-0.84(2)	-2.56(2)	0.65(2)	-0.60(12-II-1)
190139	-1.17(12-II-1)	-0.54(12-I-1)	-0.13(2)	1.57(2)	-0.80(2)	-0.33(12-II-1)
190141	-1.39(12-II-1)	-0.56(12-II-1)	-0.50(2)	3.85(2)	-3.27(2)	-0.73(12-II-1)
190142	-0.58(12-II-1)	-0.34(13-II-2)	-1.62(2)	2.49(2)	-0.56(2)	-0.89(12-II-1)
190143	-0.58(12-II-1)	-0.33(13-II-4)	-1.55(2)	2.35(2)	0.62(2)	0.87(12-I-1)
190144	1.31(12-I-1)	-0.57(12-I-1)	-0.20(2)	2.45(2)	2.80(2)	0.75(12-I-1)
190145	-0.10(12-II-1)	-0.36(13-II-1)	-0.08(2)	4.28(2)	-0.14(12-II-1)	-0.52(12-II-1)
190146	-0.10(12-II-1)	-0.43(13-II-1)	-0.09(2)	4.79(2)	-0.12(12-II-1)	-0.56(12-II-1)
190147	0.10(12-I-1)	-0.43(13-II-1)	-0.09(2)	4.78(2)	0.12(12-I-1)	-0.55(12-II-1)
190150	0.10(12-I-1)	-0.33(13-II-1)	-0.07(2)	4.14(2)	0.10(12-I-1)	-0.51(12-II-1)
190153	-0.55(12-II-1)	-0.39(13-II-2)	-1.24(2)	1.23(2)	0.69(2)	-0.90(12-II-1)
190154	0.10(12-I-1)	-0.34(13-II-2)	-0.07(2)	3.88(2)	0.78(2)	-0.52(12-II-1)
190157	-0.99(12-II-1)	-0.47(12-II-1)	-0.97(2)	-2.87(2)	-0.78(2)	-0.58(12-II-1)
190158	-1.20(12-II-1)	-0.49(12-II-1)	-0.07(2)	0.97(2)	-1.69(12-II-1)	-0.53(12-II-1)
190161	-0.55(12-II-1)	-0.38(13-II-4)	-1.21(2)	1.14(2)	-0.76(2)	0.88(12-I-1)
190162	-0.11(12-II-1)	-0.35(13-II-1)	-0.08(2)	3.97(2)	-0.84(2)	0.52(12-I-1)
190163	-0.97(12-II-1)	-0.46(12-I-1)	-1.04(2)	-2.89(2)	0.79(13-II-4)	-0.58(12-II-1)
190164	1.16(12-I-1)	-0.51(12-I-1)	-0.06(2)	0.74(12-I-2)	1.70(12-I-1)	0.59(12-I-1)
190165	0.11(12-I-1)	-0.33(13-II-2)	-0.07(2)	3.28(2)	0.41(2)	-0.52(12-II-1)
190168	-0.11(12-II-4)	-0.32(13-II-4)	-0.07(2)	3.17(2)	-0.40(2)	0.50(12-I-1)
190173	0.11(12-I-1)	-0.36(13-II-2)	-0.07(2)	2.51(2)	0.92(2)	-0.52(12-II-1)
190175	-0.56(12-II-1)	-0.43(13-II-2)	-1.39(2)	1.41(13-I-2)	0.69(2)	-0.90(12-II-1)
190176	-0.12(12-II-4)	-0.35(13-II-4)	-0.07(2)	2.44(2)	-0.92(2)	0.51(12-I-1)
190179	-1.00(12-II-1)	-0.42(12-II-1)	-0.53(2)	-0.44(2)	-2.67(2)	0.64(12-I-1)
190181	-0.56(12-II-1)	-0.43(13-II-4)	-1.44(2)	1.48(2)	-0.76(2)	0.89(12-I-1)
190184	0.97(12-I-1)	-0.44(12-I-1)	-0.60(2)	-0.43(2)	2.69(2)	-0.63(12-II-1)
190189	0.12(12-I-2)	-0.40(13-II-2)	-0.08(2)	2.70(2)	1.02(2)	-0.55(12-II-1)
190191	-0.57(12-II-1)	-0.26(12-II-1)	-0.68(2)	1.59(2)	-1.88(2)	-1.10(12-II-1)
190204	-0.13(12-II-4)	-0.41(13-II-4)	-0.08(2)	2.75(2)	-1.08(2)	0.55(12-I-1)
190210	0.56(12-I-1)	-0.28(12-I-1)	-0.72(2)	1.72(2)	1.84(2)	1.08(12-I-1)
190224	-0.09(12-II-2)	-0.22(13-II-2)	-0.08(2)	1.40(2)	-0.21(12-II-3)	-0.72(12-II-1)
190232	0.10(12-I-4)	-0.20(13-II-4)	-0.08(2)	1.39(2)	0.20(12-II-4)	0.73(12-I-1)

Risultati Analisi Dinamica - Reazioni massime - Nodi

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Nodo	Rx	Ry	Rz	Mx	My	Mz
	kg	kg	kg	kg*m	kg*m	kg*m
1	9(12-II-4)	-11(13-I-4)	183(2)	8(13-I-4)	7(12-II-4)	0

Nodo	Rx	Ry	Rz	Mx	My	Mz
2	-10(12-I-2)	-13(2)	198(2)	7(12-II-3)	-7(12-I-2)	0
3	9(12-II-4)	-12(2)	460(2)	7(2)	6(12-II-4)	0
4	494(12-II-4)	-442(13-I-4)	1189(13-II-4)	42(13-I-4)	47(12-II-4)	3(13-I-4)
5	-8(12-II-3)	-503(13-I-4)	1346(2)	48(13-I-4)	-2(12-II-3)	0
6	9(12-I-3)	-407(13-I-1)	1423(2)	41(13-I-1)	2(12-I-3)	0
7	-466(12-I-4)	-449(13-I-4)	1546(2)	43(13-I-4)	-44(12-I-4)	-2(13-I-2)
8	449(12-II-4)	-433(13-I-1)	1525(2)	42(13-I-1)	42(12-II-4)	2(12-II-4)
9	-9(12-II-3)	-402(13-I-2)	1443(2)	41(13-I-2)	-2(12-II-3)	0
10	8(12-I-3)	-474(13-I-2)	1388(2)	45(13-I-2)	2(12-I-3)	0
11	-475(12-I-4)	-370(13-I-2)	1430(2)	35(13-I-2)	-45(12-I-4)	-2(12-I-4)
12	-10(12-I-3)	-16(2)	649(2)	8(2)	-7(12-I-3)	0
13	1(12-II-1)	2(13-II-4)	389(2)	-2(13-II-4)	1(12-II-1)	0
14	438(12-II-1)	-7(13-I-4)	1042(13-I-4)	4(13-I-4)	45(12-II-1)	0
15	-4(12-I-1)	-7(13-I-4)	1214(2)	4(13-I-4)	-2(12-I-1)	0
16	4(12-II-1)	-5(13-I-1)	1288(2)	3(13-I-1)	3(12-II-1)	0
17	-425(12-I-1)	-6(13-I-1)	1324(2)	4(13-I-4)	-44(12-I-1)	0
18	-407(12-I-1)	-6(13-I-1)	1293(2)	4(13-I-1)	-43(12-I-1)	0
19	-4(12-I-1)	-4(13-I-1)	1310(2)	3(13-I-2)	-3(12-I-1)	0
20	4(12-II-1)	-7(13-I-2)	1252(2)	4(13-I-2)	2(12-II-1)	0
21	-420(12-I-1)	-7(13-I-2)	1220(2)	3(13-I-2)	-43(12-I-1)	0
22	-1(12-I-1)	5(13-II-2)	585(2)	-5(13-II-2)	-1(12-I-1)	0
23	2(12-II-1)	2(13-II-4)	375(2)	-2(13-II-4)	2(12-II-1)	0
24	507(12-II-1)	4(13-II-4)	1107(12-II-1)	-3(13-II-4)	52(12-II-1)	0
25	-4(12-I-1)	4(13-II-4)	1233(2)	-3(13-II-4)	-3(12-I-1)	0
26	4(12-II-1)	4(13-II-4)	1310(2)	-3(13-II-4)	3(12-II-1)	0
27	-479(12-I-1)	5(13-II-4)	1350(2)	-3(13-II-4)	-50(12-I-1)	0
28	453(12-II-1)	5(13-II-2)	1322(2)	-3(13-II-2)	-48(12-I-1)	0
29	-4(12-I-1)	4(13-II-2)	1330(2)	-3(13-II-2)	-3(12-I-1)	0
30	4(12-II-1)	4(13-II-2)	1275(2)	-3(13-II-2)	3(12-II-1)	0
31	-486(12-I-1)	4(13-II-2)	1259(2)	-3(13-II-2)	-50(12-I-1)	0
32	-1(12-I-1)	5(13-II-2)	568(2)	-5(13-II-2)	-1(12-I-1)	0
33	2(12-II-1)	2(13-II-4)	373(2)	-2(13-II-4)	2(12-II-1)	0
34	463(12-II-1)	440(13-II-4)	1020(12-II-4)	-45(13-II-4)	47(12-II-1)	-1(12-II-2)
35	-4(12-I-4)	431(13-II-4)	1279(12-I-1)	-45(13-II-4)	-3(12-I-1)	0
36	5(12-II-1)	418(13-II-4)	1296(2)	-44(13-II-4)	3(12-II-1)	0
37	-450(12-I-1)	451(13-II-4)	1335(2)	-46(13-II-4)	-45(12-I-1)	1(12-I-4)
38	-426(12-I-1)	437(13-II-2)	1307(2)	-45(13-II-2)	-44(12-I-1)	0
39	-4(12-I-1)	-435(13-I-2)	1324(2)	-46(13-II-2)	-3(12-I-1)	0
40	4(12-II-2)	419(13-II-2)	1252(2)	-44(13-II-2)	3(12-II-1)	0
41	-450(12-I-2)	365(13-II-2)	1226(2)	-37(13-II-2)	-45(12-I-2)	1(12-I-2)
42	-1(12-I-1)	5(13-II-2)	563(2)	-5(13-II-2)	-1(12-I-1)	0
43	2(12-II-4)	2(13-II-4)	374(2)	-2(13-II-4)	2(12-II-4)	0
44	481(12-II-4)	432(13-II-4)	1025(12-II-4)	-43(13-II-4)	48(12-II-4)	1(12-II-4)
45	-4(12-I-4)	413(13-II-4)	1233(12-I-4)	-43(13-II-4)	-3(12-I-4)	0
46	5(12-II-4)	410(13-II-4)	1317(2)	-42(13-II-4)	3(12-II-4)	0
47	-448(12-I-4)	442(13-II-4)	1359(2)	-44(13-II-4)	-45(12-I-4)	1(13-II-4)
48	-426(12-I-2)	427(13-II-2)	1331(2)	-43(13-II-2)	-44(12-I-2)	-1(12-I-4)
49	-4(12-I-4)	427(13-II-2)	1343(2)	-44(13-II-2)	-3(12-I-4)	0
50	4(12-II-2)	406(13-II-2)	1271(2)	-42(13-II-2)	3(12-II-2)	0
51	-459(12-I-2)	360(13-II-2)	1266(2)	-36(13-II-2)	-46(12-I-2)	-1(12-I-2)
52	-1(12-I-2)	5(13-II-2)	564(2)	-5(13-II-2)	-1(12-I-2)	0
53	2(12-II-3)	2(13-II-4)	374(2)	-2(13-II-4)	2(12-II-3)	0
54	497(12-II-3)	-4(13-I-4)	1054(12-II-3)	3(13-I-4)	51(12-II-3)	0
55	-4(12-I-3)	-4(13-I-4)	1216(2)	2(13-I-4)	-3(12-I-3)	0
56	4(12-II-3)	-4(13-I-4)	1292(2)	2(13-I-4)	3(12-II-3)	0
57	-490(12-I-3)	-4(13-I-4)	1323(2)	3(13-I-4)	-51(12-I-3)	0
58	-463(12-I-3)	-4(13-I-2)	1295(2)	3(13-I-2)	-49(12-I-3)	0
59	-4(12-I-3)	-4(13-I-2)	1312(2)	3(13-I-2)	-3(12-I-3)	0
60	4(12-II-3)	-4(13-I-2)	1257(2)	2(13-I-2)	3(12-II-3)	0
61	-479(12-I-3)	-4(13-I-2)	1217(2)	2(13-I-2)	-50(12-I-3)	0
62	-1(12-I-3)	5(13-II-2)	566(2)	-5(13-II-2)	-1(12-I-3)	0
63	2(12-II-3)	2(13-II-4)	378(2)	-2(13-II-4)	2(12-II-3)	0
64	512(12-II-3)	4(13-II-4)	1045(12-II-3)	-3(13-II-4)	53(12-II-3)	0
65	-4(12-I-3)	4(13-II-4)	1205(2)	-2(13-II-4)	-3(12-I-3)	0
66	4(12-II-3)	3(13-II-4)	1281(2)	-2(13-II-4)	3(12-II-3)	0
67	-488(12-I-3)	4(13-II-4)	1310(2)	-3(13-II-4)	-50(12-I-3)	0
68	-465(12-I-3)	4(13-II-2)	1282(2)	-3(13-II-2)	-49(12-I-3)	0
69	-4(12-I-3)	4(13-II-2)	1301(2)	-2(13-II-2)	-3(12-I-3)	0
70	4(12-II-3)	4(13-II-2)	1246(2)	-2(13-II-2)	3(12-II-3)	0
71	-490(12-I-3)	4(13-II-2)	1224(2)	-2(13-II-2)	-51(12-I-3)	0
72	-1(12-I-3)	5(13-II-2)	572(2)	-5(13-II-2)	-1(12-I-3)	0
73	1(12-II-3)	2(13-II-4)	340(2)	-2(13-II-4)	1(12-II-3)	0
74	452(12-II-3)	-433(13-I-4)	981(13-I-4)	44(13-I-4)	45(12-II-3)	-1(12-II-3)
75	-4(12-I-3)	-416(13-I-4)	1145(12-I-3)	43(13-I-4)	-3(12-I-3)	0
76	4(12-II-3)	-415(13-I-4)	1226(2)	43(13-I-4)	3(12-II-3)	0
77	-434(12-I-3)	-446(13-I-4)	1262(2)	45(13-I-4)	-44(12-I-3)	-1(12-II-3)
78	-411(12-I-3)	-431(13-I-2)	1234(2)	43(13-I-2)	-42(12-I-3)	1(12-I-3)
79	-4(12-I-3)	-434(13-I-2)	1253(2)	45(13-I-2)	-3(12-I-3)	0
80	4(12-II-3)	-410(13-I-2)	1186(2)	42(13-I-2)	3(12-II-3)	0

Nodo	Rx	Ry	Rz	Mx	My	Mz
81	-438(12-I-3)	-360(13-I-2)	1157(2)	36(13-I-2)	-44(12-I-3)	1(12-I-3)
82	-1(12-I-3)	5(13-II-2)	513(2)	-5(13-II-2)	-1(12-I-3)	0
83	6(12-II-3)	-2(13-I-4)	162(2)	2(13-I-4)	7(12-II-3)	0
84	6(12-II-3)	-1(13-I-4)	390(2)	1(13-I-4)	7(12-II-3)	0
85	6(12-II-3)	-1(13-I-4)	587(2)	1(13-I-4)	7(12-II-3)	0
86	6(12-II-3)	-1(13-I-4)	593(2)	1(13-I-4)	-7(12-I-3)	0
87	-6(12-I-3)	-1(13-I-4)	587(2)	1(13-I-4)	-7(12-I-3)	0
88	-6(12-I-3)	-1(13-I-2)	585(2)	1(13-I-2)	-7(12-I-3)	0
89	-6(12-I-3)	-1(13-I-2)	589(2)	1(13-I-2)	-7(12-I-3)	0
90	-6(12-I-3)	-1(13-I-2)	593(2)	1(13-I-2)	-7(12-I-3)	0
91	-6(12-I-3)	-1(13-II-2)	522(2)	1(13-I-2)	-7(12-I-3)	0
92	-6(12-I-3)	5(13-II-2)	250(2)	-5(13-II-2)	-7(12-I-3)	0
11498	-104(12-I-1)	-27(13-I-1)	824(2)	7(13-I-1)	-21(12-I-1)	0
11499	-161(12-I-1)	-193(13-I-1)	614(2)	36(13-I-1)	-31(12-I-1)	-1(12-II-1)
11500	-131(12-I-1)	54(13-II-1)	954(2)	16(13-I-1)	-36(12-I-1)	1(12-I-1)
11501	-103(12-I-1)	-33(13-I-1)	1199(2)	9(13-I-1)	-21(12-I-1)	0
11502	-160(12-I-1)	-285(13-I-1)	1093(2)	53(13-I-1)	-30(12-I-1)	1(13-I-1)
11503	127(12-II-1)	83(13-II-1)	981(2)	23(13-I-1)	35(12-II-1)	-1(12-II-1)
11504	110(12-II-1)	-31(13-I-1)	1190(2)	9(13-I-1)	22(12-II-1)	0
11505	161(12-II-1)	-273(13-I-1)	1094(2)	51(13-I-1)	31(12-II-1)	-1(12-II-1)
11506	-127(12-I-1)	79(13-II-1)	998(2)	22(13-I-1)	-35(12-I-1)	1(12-I-1)
11507	108(12-II-1)	-25(13-I-1)	849(2)	7(13-I-1)	22(12-II-1)	0
11508	162(12-II-1)	-163(13-I-1)	609(2)	31(13-I-1)	31(12-II-1)	1(12-I-1)
11509	130(12-II-1)	-45(13-I-1)	947(2)	13(13-I-1)	35(12-II-1)	-1(12-II-1)
11510	-78(12-I-1)	40(2)	1251(2)	-15(2)	-27(12-I-1)	0
11511	75(12-II-1)	39(2)	1404(2)	-16(13-II-2)	26(12-II-1)	0
11512	75(12-II-1)	40(2)	1189(2)	-14(2)	-27(12-I-1)	-1(13-II-2)
11513	-76(12-I-1)	17(2)	843(2)	-6(13-II-3)	-27(12-I-1)	-1(13-II-2)
11514	76(12-II-1)	43(2)	1174(2)	-17(2)	27(12-II-1)	0
11515	-76(12-I-1)	44(2)	1156(2)	-17(2)	-27(12-I-1)	0
11516	77(12-II-1)	40(2)	1346(2)	-15(2)	27(12-II-1)	0
11517	72(12-II-1)	44(2)	1306(2)	-19(13-II-4)	26(12-II-1)	1(13-II-3)
11518	-74(12-I-1)	37(2)	868(2)	-12(2)	-26(12-I-1)	1(13-II-3)
11519	76(12-II-1)	18(2)	565(2)	-7(13-II-4)	27(12-II-1)	1(12-I-4)
11520	138(12-II-1)	52(12-II-1)	582(2)	-10(13-II-1)	27(12-II-1)	2(13-II-2)
11521	-155(12-I-1)	-61(12-I-1)	424(2)	13(12-I-1)	-30(12-I-1)	-1(13-II-2)
11522	-94(12-I-2)	-58(12-I-2)	911(2)	12(12-I-2)	-19(12-I-2)	0
11523	-100(12-I-2)	-43(13-I-2)	1218(2)	11(13-I-2)	-21(12-I-2)	0
11524	-154(12-I-1)	-58(12-I-1)	974(2)	12(13-I-2)	-30(12-I-1)	-1(13-II-2)
11525	107(12-II-2)	-46(12-I-2)	1230(2)	12(13-I-1)	21(12-II-2)	0
11526	-141(12-I-1)	62(12-II-1)	1248(2)	-18(13-II-1)	-28(12-I-1)	0
11527	104(12-II-2)	-43(12-I-2)	836(2)	8(12-I-2)	21(12-II-2)	0
11528	-142(12-I-1)	56(12-I-1)	570(2)	-10(12-I-1)	-28(12-I-1)	-1(13-II-1)
11529	96(12-II-4)	-56(12-II-4)	912(2)	11(12-II-4)	20(12-II-4)	0
11530	163(12-II-1)	-60(12-II-1)	998(2)	12(12-II-1)	32(12-II-1)	0
11531	-97(12-I-1)	-38(12-II-4)	811(2)	7(12-II-4)	-20(12-I-1)	1(12-I-4)
11532	102(12-II-4)	-46(12-II-4)	1210(2)	11(13-I-1)	21(12-II-4)	0
11533	164(12-II-1)	-63(12-II-1)	431(2)	12(12-II-1)	32(12-II-1)	1(13-II-4)
11534	-99(12-I-4)	-39(12-II-1)	1238(2)	11(13-I-1)	-20(12-I-4)	0
11535	146(12-II-1)	65(12-I-1)	1242(2)	-16(13-II-1)	29(12-II-1)	0
11536	16(12-II-4)	-15(13-I-4)	432(2)	8(13-I-4)	8(12-II-4)	-2(12-II-4)
11537	17(12-II-4)	-16(12-I-3)	477(2)	8(12-I-3)	8(12-II-4)	0
11538	-15(12-I-2)	-13(12-II-2)	434(2)	7(12-II-3)	-8(12-I-2)	2(12-I-4)
11539	-17(12-I-3)	-17(12-II-3)	480(2)	9(12-II-3)	-8(12-I-3)	0
11540	12(12-II-1)	-14(13-I-2)	349(2)	7(13-I-2)	5(12-II-1)	0
11541	34(12-II-2)	-37(13-I-3)	890(2)	8(13-I-3)	8(12-II-2)	0
11542	-13(12-I-1)	-16(13-I-4)	369(2)	7(13-I-4)	-6(12-I-1)	0
11543	-23(12-I-4)	-28(13-I-4)	827(2)	7(13-I-4)	-6(12-I-4)	0
21498	-185(12-I-1)	-289(13-I-1)	868(2)	-29(13-II-1)	-20(12-I-1)	0
21499	173(12-II-1)	369(13-II-1)	1077(2)	-39(13-II-1)	19(12-II-1)	0
21500	-174(12-I-1)	358(13-II-1)	1081(2)	-38(13-II-1)	-19(12-I-1)	0
21501	185(12-II-1)	-256(13-I-1)	875(2)	-25(13-II-1)	20(12-II-1)	0
21502	-183(12-I-2)	-297(13-I-3)	921(2)	29(13-I-3)	-21(12-I-2)	-1(12-II-2)
21503	-249(12-I-2)	-398(13-I-2)	1038(2)	-41(13-II-2)	-26(12-I-2)	1(13-I-2)
21504	-196(12-I-2)	-458(13-I-2)	1061(2)	45(13-I-2)	-22(12-I-2)	-1(13-I-2)
21505	192(12-II-1)	-262(13-I-1)	860(2)	-28(13-II-1)	20(12-II-1)	0
21506	183(12-II-4)	-324(13-I-4)	907(2)	32(13-I-4)	21(12-II-4)	1(12-I-4)
21507	-194(12-I-1)	-239(13-I-1)	858(2)	-25(13-II-1)	-20(12-I-1)	0
21508	212(12-II-4)	-398(13-I-4)	1033(2)	-40(13-II-4)	23(12-II-4)	-1(13-I-1)
21509	201(12-II-4)	-408(13-I-1)	1061(2)	40(13-I-1)	22(12-II-4)	1(12-I-4)
21510	18(12-II-3)	-16(12-I-3)	474(2)	8(12-I-3)	8(12-II-3)	0
21511	-19(12-I-3)	-19(12-II-3)	473(2)	10(12-II-3)	-9(12-I-3)	0
21512	230(13-I-3)	-251(13-I-3)	810(2)	26(13-I-3)	23(13-I-3)	-1(12-II-2)
21513	-205(13-I-4)	-222(13-I-4)	843(2)	23(13-I-4)	-20(13-I-4)	0
31498	-156(12-I-1)	-19(13-I-1)	1075(2)	5(13-I-1)	-32(12-I-1)	1(12-I-1)
31499	155(12-II-1)	-24(13-I-1)	1193(2)	6(13-I-1)	32(12-II-1)	-1(12-II-1)
31500	-155(12-I-1)	-25(13-I-1)	1192(2)	6(13-I-1)	-32(12-I-1)	1(12-I-1)
31501	156(12-II-1)	-20(13-I-1)	1082(2)	5(13-I-1)	32(12-II-1)	-1(12-II-1)
31502	-151(12-I-2)	-69(12-I-2)	1111(2)	13(12-I-2)	-31(12-I-2)	1(12-I-1)

Nodo	Rx	Ry	Rz	Mx	My	Mz
31503	155(12-II-2)	-64(12-I-2)	1180(2)	12(12-I-2)	32(12-II-2)	-1(12-II-1)
31504	147(12-II-2)	-60(12-I-2)	1203(2)	11(12-I-2)	-30(12-I-2)	1(12-I-2)
31505	147(12-II-2)	-62(12-I-2)	1064(2)	12(12-I-2)	30(12-II-1)	-1(12-II-2)
31506	-148(12-I-4)	-61(12-II-4)	1204(2)	11(12-II-4)	30(12-II-4)	-1(12-II-4)
31507	-155(12-I-4)	-68(12-II-4)	1186(2)	13(12-II-4)	-31(12-I-4)	1(12-I-4)
31508	151(12-II-4)	-69(12-II-4)	1109(2)	14(12-II-4)	31(12-II-4)	-1(12-II-4)
31509	-147(12-I-4)	-64(12-II-4)	1067(2)	12(12-II-4)	-30(12-I-4)	1(12-I-4)
31510	23(12-II-4)	-22(12-I-3)	466(2)	10(12-I-3)	10(12-II-4)	0
31511	-23(12-I-3)	-25(12-II-3)	454(2)	12(12-II-3)	-11(12-I-3)	0
31512	29(13-I-3)	-37(13-I-3)	1157(2)	9(12-II-2)	-6(12-I-2)	0
31513	-20(13-I-4)	-28(13-I-3)	1100(2)	8(12-II-4)	6(12-II-4)	0
50445	167(12-II-1)	200(13-II-1)	766(2)	-23(13-II-1)	20(12-II-1)	2(12-I-1)
50449	158(12-II-1)	197(13-II-1)	1065(2)	-22(13-II-1)	18(12-II-1)	-2(12-II-1)
50453	-157(12-I-1)	198(13-II-1)	1062(2)	-23(13-II-1)	-18(12-I-1)	2(12-I-1)
50457	-167(12-I-1)	200(13-II-1)	739(2)	-23(13-II-1)	-20(12-I-1)	-2(12-II-1)
50466	3(12-II-1)	4(2)	509(2)	-1(13-II-3)	2(12-II-1)	0
50470	-4(12-I-1)	3(12-II-2)	501(2)	0	-2(12-I-1)	0
50486	-3(12-I-1)	5(12-II-2)	507(2)	-2(12-II-2)	-1(12-I-1)	0
50490	152(12-II-1)	188(13-II-2)	728(2)	-21(13-II-2)	17(12-II-1)	2(12-I-2)
50499	-151(12-I-1)	184(13-II-4)	721(2)	-21(13-II-4)	-17(12-I-1)	-2(12-II-4)
50503	3(12-II-1)	5(12-I-4)	515(2)	-2(12-I-4)	1(12-II-1)	0
50527	154(12-II-2)	194(13-II-2)	1061(2)	-22(13-II-2)	-18(12-I-1)	-2(12-II-2)
50540	-161(12-I-4)	174(13-II-1)	1054(2)	-20(13-II-1)	18(12-II-4)	2(12-I-4)
50570	-159(12-I-2)	210(13-II-2)	1057(2)	-24(13-II-2)	-19(12-I-2)	2(12-I-1)
50580	154(12-II-4)	199(13-II-4)	1061(2)	-23(13-II-4)	18(12-II-4)	-2(12-II-4)
50603	-167(12-I-2)	227(13-II-3)	805(2)	-25(13-II-3)	-20(12-I-2)	-2(12-II-1)
50612	156(12-II-4)	208(13-II-4)	775(2)	-24(13-II-4)	19(12-II-4)	2(12-I-4)
50622	-132(12-I-2)	-78(12-I-2)	526(2)	9(12-I-2)	-15(12-I-2)	0
50626	130(12-II-4)	-77(12-II-4)	530(2)	9(12-II-4)	15(12-II-4)	0
50668	-136(12-I-2)	-83(12-I-2)	633(2)	10(12-I-2)	-16(12-I-2)	0
50672	131(12-II-4)	-82(12-II-4)	710(2)	10(12-II-4)	15(12-II-4)	0
50676	-182(13-II-3)	205(13-II-3)	636(2)	-25(13-II-3)	-21(13-II-3)	2(12-I-2)
50682	195(13-II-4)	217(13-II-4)	534(2)	-26(13-II-4)	22(13-II-4)	-2(12-II-4)
50717	13(13-II-4)	-24(13-I-4)	403(2)	12(13-I-4)	7(13-II-4)	0
50736	-24(12-I-3)	-24(12-II-3)	468(2)	12(12-II-3)	-11(12-I-3)	0
50737	24(13-II-3)	20(13-II-4)	250(2)	-10(13-II-4)	10(13-II-4)	0
61498	-107(12-I-1)	-19(13-I-1)	745(2)	5(13-I-1)	-22(12-I-1)	0
61499	-107(12-I-1)	-27(13-I-1)	1182(2)	6(13-I-1)	-21(12-I-1)	0
61500	107(12-II-1)	-27(13-I-1)	1185(2)	6(13-I-1)	21(12-II-1)	0
61501	107(12-II-1)	-20(13-I-1)	769(2)	5(13-I-1)	22(12-II-1)	0
61502	-102(12-I-2)	-48(12-I-2)	745(2)	9(12-I-2)	-21(12-I-2)	0
61503	-104(12-I-2)	-45(12-I-2)	1162(2)	8(12-I-2)	-21(12-I-2)	0
61504	104(12-II-2)	-40(12-I-1)	1173(2)	7(12-I-1)	21(12-II-2)	0
61505	104(12-II-2)	-36(12-I-2)	723(2)	7(12-I-2)	21(12-II-2)	0
61506	-103(12-I-4)	-41(12-II-1)	1176(2)	7(12-II-1)	-20(12-I-4)	0
61507	104(12-II-4)	-44(12-II-4)	1161(2)	8(12-II-1)	21(12-II-4)	0
61508	100(12-II-4)	-52(12-II-4)	758(2)	10(12-II-4)	21(12-II-4)	0
61509	-103(12-I-4)	-39(12-II-3)	710(2)	7(12-II-3)	-21(12-I-4)	0
61510	100(12-II-1)	-26(12-I-2)	737(2)	5(12-I-2)	-20(12-I-1)	0
61511	-102(12-I-2)	-20(12-I-2)	742(2)	5(13-I-1)	-20(12-I-1)	0
61512	102(12-II-1)	-24(12-II-4)	762(2)	5(13-I-1)	20(12-II-1)	0
61513	-99(12-I-1)	-29(12-II-3)	732(2)	5(12-II-3)	20(12-II-1)	0
61514	-100(12-I-2)	-56(12-I-2)	718(2)	10(12-I-2)	-20(12-I-2)	0
61515	102(12-II-2)	-58(12-I-1)	773(2)	11(12-I-1)	-21(12-I-2)	0
61516	-106(12-I-4)	-60(12-II-4)	1215(2)	-12(12-I-4)	-21(12-I-4)	-1(12-II-4)
61517	-104(12-I-4)	-58(12-II-4)	725(2)	-11(12-I-4)	-21(12-I-4)	1(12-I-3)
61518	-28(12-I-3)	-29(12-II-3)	479(2)	14(12-II-3)	-13(12-I-3)	0
61519	35(12-II-3)	-35(13-I-3)	761(2)	8(13-I-3)	8(12-II-2)	0
61520	21(13-II-4)	-31(13-I-4)	586(2)	14(13-I-4)	9(13-II-4)	0
70262	171(12-II-1)	-176(13-I-1)	774(2)	-18(13-II-1)	19(12-II-1)	1(12-I-1)
70266	158(12-II-1)	246(13-II-1)	1091(2)	-25(13-II-1)	-17(12-I-1)	0
70270	-159(12-I-1)	241(13-II-1)	1087(2)	-25(13-II-1)	-17(12-I-1)	0
70274	-173(12-I-1)	-170(13-I-1)	751(2)	-18(13-II-1)	-19(12-I-1)	-1(12-II-1)
70279	167(12-II-1)	164(13-II-1)	750(2)	-17(13-II-1)	18(12-II-1)	0
70283	-163(12-I-1)	-166(13-I-1)	775(2)	-18(13-II-1)	-18(12-I-1)	0
70290	-165(12-I-1)	145(13-II-2)	759(2)	-15(13-II-2)	-18(12-I-1)	0
70294	161(12-II-1)	139(13-II-1)	753(2)	-15(13-II-1)	18(12-II-1)	0
70303	173(12-II-1)	153(13-II-2)	754(2)	-16(13-II-2)	18(12-II-1)	0
70312	-168(12-I-1)	145(13-II-4)	748(2)	-16(13-II-4)	-18(12-I-1)	-1(12-II-3)
70333	-178(12-I-2)	193(13-II-2)	1100(2)	-20(13-II-2)	-20(12-I-2)	0
70346	175(12-II-4)	181(13-II-4)	1098(2)	-19(13-II-4)	19(12-II-4)	0
70384	-192(12-I-2)	245(13-II-2)	1097(2)	-25(13-II-2)	-21(12-I-2)	0
70396	192(12-II-4)	215(13-II-4)	1102(2)	-23(13-II-4)	21(12-II-4)	0
70418	-193(12-I-2)	200(13-II-3)	821(2)	-21(13-II-3)	-21(12-I-2)	-1(12-I-2)
70429	174(12-II-4)	189(13-II-4)	832(2)	-19(13-II-4)	20(12-II-4)	0
70461	-210(12-I-2)	228(13-II-3)	815(2)	-24(13-II-3)	-22(12-I-2)	0
70474	182(12-II-4)	189(13-II-4)	726(2)	-20(13-II-4)	20(12-II-4)	-1(12-II-4)
70518	-249(12-I-2)	247(13-II-3)	878(2)	-25(13-II-3)	-27(12-I-2)	-1(12-II-2)
70532	274(12-II-3)	335(13-II-4)	920(2)	-35(13-II-4)	29(12-II-3)	1(12-I-3)

Nodo	Rx	Ry	Rz	Mx	My	Mz
70553	237(13-I-3)	-255(13-I-3)	720(2)	-26(13-II-3)	22(13-I-3)	-1(12-II-2)
70592	25(13-II-4)	30(13-II-4)	480(2)	14(13-I-4)	10(13-II-4)	0
70630	-31(12-I-3)	-31(12-II-3)	458(2)	15(12-II-3)	-14(12-I-3)	0
71498	-10(12-I-4)	-12(13-I-3)	619(2)	5(13-I-3)	-5(12-I-4)	0
91498	-124(12-I-1)	-38(13-I-1)	882(2)	8(13-I-1)	-24(12-I-1)	1(12-I-1)
91499	-122(12-I-1)	-53(13-I-1)	1196(2)	11(13-I-1)	-23(12-I-1)	0
91500	123(12-II-1)	-53(13-I-1)	1199(2)	11(13-I-1)	23(12-II-1)	0
91501	124(12-II-1)	-40(13-I-1)	913(2)	8(13-I-1)	24(12-II-1)	0
91502	108(12-II-2)	-57(12-I-1)	854(2)	9(12-I-1)	-20(12-I-2)	0
91503	109(12-II-2)	-52(13-I-2)	1097(2)	10(13-I-2)	-21(12-I-2)	0
91504	110(12-II-2)	-55(13-I-2)	1127(2)	10(13-I-2)	20(12-II-2)	0
91505	111(12-II-2)	-39(13-I-2)	800(2)	7(13-I-2)	21(12-II-1)	0
91506	-127(12-I-4)	-57(13-I-4)	1132(2)	11(13-I-4)	-24(12-I-4)	-1(12-II-4)
91507	-136(12-I-4)	-55(13-I-4)	1100(2)	10(13-I-4)	-25(12-I-4)	0
91508	-124(12-I-4)	-85(12-II-4)	807(2)	14(12-II-4)	-23(12-I-4)	0
91509	-128(12-I-4)	-50(12-II-3)	793(2)	9(12-II-3)	-24(12-I-4)	1(12-I-4)
91510	115(12-II-1)	-36(13-I-2)	863(2)	7(13-I-2)	-22(12-I-1)	0
91511	-115(12-I-1)	-39(13-I-2)	888(2)	7(13-I-2)	22(12-II-1)	0
91512	-122(12-I-1)	-42(13-I-4)	920(2)	8(13-I-4)	-23(12-I-1)	0
91513	-122(12-I-1)	-37(13-I-4)	843(2)	7(13-I-4)	23(12-II-1)	0
91514	121(12-II-2)	-82(13-II-2)	753(2)	15(13-II-2)	22(12-II-2)	0
91515	126(12-II-2)	-81(13-I-2)	792(2)	15(13-I-2)	23(12-II-2)	0
91516	212(12-II-2)	-189(13-II-2)	755(2)	25(13-II-2)	28(12-II-2)	0
91517	-240(12-I-2)	-206(13-I-3)	981(2)	28(13-I-3)	30(12-II-2)	1(12-II-2)
91518	-37(12-I-4)	-43(13-I-4)	692(2)	8(13-I-4)	-9(12-I-4)	0
91519	-31(12-I-3)	-42(12-II-3)	595(2)	19(12-II-3)	-14(12-I-3)	0
91520	-12(12-I-2)	13(13-II-3)	1012(2)	-5(13-II-3)	-5(12-I-2)	0
91521	-13(12-I-4)	-8(13-I-4)	617(2)	5(13-I-4)	-6(12-I-4)	0
91522	24(12-II-4)	31(13-II-4)	436(2)	14(13-I-4)	10(12-II-4)	0
101498	183(12-II-1)	-316(13-I-1)	1171(2)	27(13-I-1)	17(12-II-1)	1(12-I-1)
101499	-179(12-I-1)	-443(13-I-1)	1327(2)	37(13-I-1)	-16(12-I-1)	-1(12-II-1)
101500	173(12-II-1)	-437(13-I-1)	1327(2)	37(13-I-1)	16(12-II-1)	1(12-I-1)
101501	-181(12-I-1)	-296(13-I-1)	1121(2)	25(13-I-1)	-17(12-I-1)	-1(12-II-1)
101502	-60(12-I-1)	37(2)	593(2)	-12(12-II-1)	-22(12-I-1)	0
101503	-203(12-I-2)	436(13-II-2)	1299(2)	-39(13-II-2)	19(12-II-2)	-1(12-II-1)
101504	-189(12-I-2)	274(13-I-2)	1226(2)	26(13-II-2)	-18(12-I-2)	-1(12-I-2)
101505	-183(12-I-2)	427(13-II-2)	1240(2)	-37(13-II-2)	-17(12-I-2)	-1(12-II-2)
101506	188(12-II-1)	332(13-II-2)	1104(2)	-28(13-II-2)	17(12-II-1)	1(12-I-1)
101507	-304(12-I-4)	391(13-II-4)	1364(2)	-35(13-II-4)	-28(12-I-4)	1(12-I-1)
101508	-219(12-I-4)	329(13-II-4)	1094(2)	-28(13-II-4)	-20(12-I-4)	-1(12-II-1)
101509	233(12-II-4)	340(13-II-4)	1278(2)	31(13-I-4)	22(12-II-4)	0
101510	221(12-II-4)	406(13-II-4)	1240(2)	-35(13-II-4)	21(12-II-4)	1(12-I-4)
101511	182(12-II-1)	-274(13-I-1)	1120(2)	23(13-I-1)	17(12-II-1)	1(12-I-1)
101512	-171(12-I-1)	265(13-II-2)	1075(2)	-22(13-II-2)	-16(12-I-1)	1(12-I-1)
101513	181(12-II-4)	258(13-II-4)	1061(2)	-22(13-II-4)	17(12-II-4)	-1(12-II-4)
101514	-189(12-I-1)	-284(13-I-1)	1159(2)	-24(13-II-1)	-18(12-I-1)	-1(12-II-1)
101515	-45(12-I-1)	45(2)	524(2)	-15(12-II-2)	-17(12-I-1)	0
101516	-42(12-I-1)	33(12-II-2)	455(2)	-12(12-II-2)	-16(12-I-1)	0
101517	38(2)	-33(13-I-4)	375(2)	15(13-I-4)	12(13-II-4)	0
101518	-183(13-I-4)	-271(13-I-4)	974(2)	26(13-I-4)	-19(13-I-4)	-1(12-II-4)
101519	-64(12-I-3)	51(12-I-2)	322(2)	-22(12-I-2)	-26(12-I-3)	0
101520	-48(12-I-2)	62(2)	586(2)	-20(12-II-2)	-17(12-I-2)	0
101521	35(2)	34(13-II-4)	249(2)	-14(13-II-4)	12(13-II-4)	0
101522	33(2)	32(13-II-4)	290(2)	-12(13-II-4)	11(12-II-4)	1(13-I-4)
101523	41(12-II-4)	30(12-I-4)	305(2)	-10(12-I-4)	15(12-II-4)	0
101524	38(12-II-4)	23(12-I-4)	258(2)	-8(13-II-4)	14(12-II-4)	0
101525	27(12-II-4)	25(2)	185(2)	-8(12-I-4)	12(12-II-4)	3(12-I-4)
101526	38(12-II-1)	-31(12-II-1)	302(2)	13(12-II-1)	16(12-II-1)	3(12-I-4)
110097	53(12-II-1)	107(2)	684(2)	-34(2)	24(12-II-1)	0
110098	-51(12-I-1)	120(2)	764(2)	-38(2)	24(12-II-1)	0
110099	52(12-II-1)	120(2)	767(2)	-38(2)	24(12-II-1)	0
110101	-53(12-I-1)	104(2)	655(2)	-33(2)	-24(12-I-1)	0
110107	-48(12-I-1)	90(2)	791(2)	-29(2)	-23(12-I-1)	0
110109	48(12-II-1)	88(2)	867(2)	-28(2)	22(12-II-1)	0
110113	-54(12-I-1)	45(2)	1110(2)	-15(2)	-24(12-I-1)	0
110115	53(12-II-1)	37(13-II-4)	1163(2)	-13(13-II-4)	24(12-II-1)	0
110123	54(12-II-1)	-29(13-I-2)	1503(2)	11(12-I-1)	24(12-II-1)	0
110124	-53(12-I-1)	-30(12-II-1)	1501(2)	11(12-II-1)	-23(12-I-1)	0
110137	58(12-II-1)	-35(12-I-1)	1827(2)	13(12-I-1)	25(12-II-1)	0
110139	-55(12-I-1)	-32(13-I-4)	1791(2)	11(12-II-1)	-24(12-I-1)	0
110158	-32(12-I-2)	15(13-II-1)	1052(2)	-7(12-II-1)	-17(12-I-1)	0
110164	37(12-II-1)	18(12-I-4)	928(2)	-8(12-I-1)	18(12-II-1)	-1(12-I-1)

VERIFICHE STATO LIMITE ULTIMO

Verifica Stabilità aste Metalliche più sollecitate

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Asta : 4 [4 , 10004]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma = 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1386	47	-25	15840	215	215	8	8	1.000	1.000	--	0.524	0.285	0.314	0.475

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1386	25	7	15086	204	204	(12+13)-VIII-4	4.1
1	Z	1386	15	12	15086	204	204	(12+13)-VIII-4	4.5

Asta : 4 [40004 , 70004]

Sez. G: Tubo40x40x4 L=43.0 cm Ln1=43.0 cm Ln2=43.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=6.878

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1057	47	9	15840	215	215	29	29	0.969	0.969	--	0.510	0.241	0.306	0.402

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1057	24	2	14621	204	204	2	5.0
1	Z	1057	14	4	14621	204	204	2	6.3

Asta : 5 [5 , 10005]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma = 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1523	51	0	15840	215	215	8	8	1.000	1.000	--	0.512	0.256	0.307	0.427

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1523	26	0	15086	204	204	(12+13)-VIII-2	4.3
1	Z	1523	16	0	15086	204	204	(12+13)-VIII-2	5.6

Asta : 5 [40005 , 70005]

Sez. G: Tubo40x40x4 L=43.0 cm Ln1=43.0 cm Ln2=43.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=6.878

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1523	60	2	15840	215	215	29	29	0.969	0.969	--	0.514	0.242	0.308	0.403

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1523	31	0	14621	204	204	2	3.9
1	Z	1523	19	1	14621	204	204	2	5.0

Asta : 5 [70005 , 120005]

Sez. G: Tubo40x40x4 L=57.0 cm Ln1=57.0 cm Ln2=57.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=5.189

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-578	-69	-3	15840	215	215	39	39	0.941	0.941	--	0.404	0.243	0.242	0.405

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	578	28	1	14193	204	204	(12+13)-VIII-2	5.5
1	Z	578	17	1	14193	204	204	(12+13)-VIII-2	7.8

Asta : 6 [6 , 10006]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1567	45	-2	15840	215	215	8	8	1.000	1.000	--	0.533	0.520	0.320	0.867

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1567	24	1	15086	204	204	(12+13)-IV-4	4.4
1	Z	1567	14	1	15086	204	204	(12+13)-IV-4	5.5

Asta : 6 [40006 , 70006]

Sez. G: Tubo40x40x4 L=43.0 cm Ln1=43.0 cm Ln2=43.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: **Verificato**

SF_λ=6.878

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1505	58	-4	15840	215	215	29	29	0.969	0.969	--	0.518	0.242	0.311	0.403

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1505	30	1	14621	204	204	2	4.0
1	Z	1505	18	1	14621	204	204	2	5.1

Asta : 7 [7 , 10007]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1373	46	-19	15840	215	215	8	8	1.000	1.000	--	0.516	0.303	0.310	0.504

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1373	24	6	15086	204	204	(12+13)-IV-4	4.3
1	Z	1373	14	9	15086	204	204	(12+13)-IV-4	4.8

Asta : 7 [40007 , 70007]

Sez. G: Tubo40x40x4 L=43.0 cm Ln1=43.0 cm Ln2=43.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: **Verificato**

SF_λ=6.878

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1511	58	4	15840	215	215	29	29	0.969	0.969	--	0.530	0.242	0.318	0.403

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1511	31	1	14621	204	204	2	3.9
1	Z	1511	19	2	14621	204	204	2	5.0

Asta : 8 [8 , 10008]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1665	42	-23	15840	215	215	8	8	1.000	1.000	--	0.519	0.286	0.312	0.477

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1665	22	7	15086	204	204	(12+13)-II-4	4.0
1	Z	1665	13	11	15086	204	204	(12+13)-II-4	4.4

Asta : 8 [40008 , 70008]

Sez. G: Tubo40x40x4 L=43.0 cm Ln1=43.0 cm Ln2=43.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: **Verificato**

SF_λ=6.878

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1502	58	4	15840	215	215	29	29	0.969	0.969	--	0.532	0.242	0.319	0.403

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1502	31	1	14621	204	204	2	3.9
1	Z	1502	18	2	14621	204	204	2	5.0

Asta : 9 [9 , 10009]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1579	46	2	15840	215	215	8	8	1.000	1.000	--	0.539	0.498	0.323	0.831

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1579	25	1	15086	204	204	(12+13)-II-2	4.4
1	Z	1579	15	1	15086	204	204	(12+13)-II-2	5.5

Asta : 9 [40009 , 70009]

Sez. G: Tubo40x40x4 L=43.0 cm Ln1=43.0 cm Ln2=43.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: **Verificato**

SF_λ=6.878

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1495	58	4	15840	215	215	29	29	0.969	0.969	--	0.516	0.242	0.309	0.403

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1495	30	1	14621	204	204	2	4.0
1	Z	1495	18	2	14621	204	204	2	5.1

Asta : 10 [10 , 10010]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1525	49	-2	15840	215	215	8	8	1.000	1.000	--	0.503	0.519	0.302	0.865

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1525	25	1	15086	204	204	(12+13)-II-4	4.4
1	Z	1525	15	1	15086	204	204	(12+13)-II-4	5.6

Asta : 10 [40010 , 70010]

Sez. G: Tubo40x40x4 L=43.0 cm Ln1=43.0 cm Ln2=43.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: **Verificato**

SF_λ=6.878

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1518	58	-3	15840	215	215	29	29	0.969	0.969	--	0.517	0.242	0.310	0.403

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1518	30	1	14621	204	204	2	4.0
1	Z	1518	18	1	14621	204	204	2	5.1

Asta : 10 [70010 , 120010]

Sez. G: Tubo40x40x4 L=57.0 cm Ln1=57.0 cm Ln2=57.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: **Verificato**

SF_λ=5.189

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-579	-60	-9	15840	215	215	39	39	0.941	0.941	--	0.404	0.243	0.242	0.405

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	579	24	2	14193	204	204	(12+13)-VI-2	5.9
1	Z	579	15	4	14193	204	204	(12+13)-VI-2	7.7

Asta : 11 [11 , 10011]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1102	-20	51	15840	215	215	8	8	1.000	1.000	--	0.609	0.295	0.366	0.491

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1102	12	15	15086	204	204	(12+13)-III-1	4.8
1	Z	1102	7	25	15086	204	204	(12+13)-III-1	4.3

Asta : 11 [40011 , 70011]

Sez. G: Tubo40x40x4 L=43.0 cm Ln1=43.0 cm Ln2=43.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq: **Verificato**

SF_λ=6.878

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1375	57	-5	15840	215	215	29	29	0.969	0.969	--	0.516	0.242	0.310	0.403

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1375	30	1	14621	204	204	2	4.1
1	Z	1375	18	2	14621	204	204	2	5.3

Asta : 14 [14 , 10014]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1107	-2	-51	15840	215	215	8	8	1.000	1.000	--	0.896	0.316	0.538	0.527

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1107	2	16	15086	204	204	(12+13)-I-3	6.1
1	Z	1107	1	27	15086	204	204	(12+13)-I-3	4.7

Asta : 17 [17 , 10017]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1370	-2	50	15840	215	215	8	8	1.000	1.000	--	0.907	0.315	0.544	0.525

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1370	2	16	15086	204	204	(12+13)-III-1	5.6
1	Z	1370	1	26	15086	204	204	(12+13)-III-1	4.4

Asta : 18 [18 , 10018]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1338	-2	-47	15840	215	215	8	8	1.000	1.000	--	0.909	0.315	0.545	0.525

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1338	2	15	15086	204	204	(12+13)-I-3	5.9
1	Z	1338	1	25	15086	204	204	(12+13)-I-3	4.6

Asta : 21 [21 , 10021]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1231	-3	49	15840	215	215	8	8	1.000	1.000	--	0.897	0.316	0.538	0.526

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1231	2	15	15086	204	204	(12+13)-III-1	5.9
1	Z	1231	1	26	15086	204	204	(12+13)-III-1	4.7

Asta : 24 [24 , 10024]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1369	2	-55	15840	215	215	8	8	1.000	1.000	--	0.923	0.316	0.554	0.527

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1369	2	17	15086	204	204	(12+13)-III-4	5.4
1	Z	1369	1	29	15086	204	204	(12+13)-III-4	4.2

Asta : 27 [27 , 10027]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1416	1	56	15840	215	215	8	8	1.000	1.000	--	0.917	0.315	0.550	0.526

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1416	1	18	15086	204	204	(12+13)-I-2	5.4
1	Z	1416	1	29	15086	204	204	(12+13)-I-2	4.1

Asta : 28 [28 , 10028]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1401	1	-53	15840	215	215	8	8	1.000	1.000	--	0.917	0.315	0.550	0.526

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1401	1	17	15086	204	204	(12+13)-III-4	5.5
1	Z	1401	1	28	15086	204	204	(12+13)-III-4	4.3

Asta : 31 [31 , 10031]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1391	0	54	15840	215	215	8	8	1.000	1.000	--	0.894	0.316	0.536	0.526

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1391	0	17	15086	204	204	(12+13)-III-2	5.6
1	Z	1391	0	28	15086	204	204	(12+13)-III-2	4.3

Asta : 34 [34 , 10034]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-852	23	-52	15840	215	215	8	8	1.000	1.000	--	0.533	0.310	0.320	0.517

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	852	12	16	15086	204	204	(12+13)-III-4	5.1
1	Z	852	7	27	15086	204	204	(12+13)-III-4	4.5

Asta : 35 [35 , 10035]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1365	-52	1	15840	215	215	8	8	1.000	1.000	--	0.535	0.543	0.321	0.905

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1365	28	1	15086	204	204	(12+13)-IV-1	4.3
1	Z	1365	17	1	15086	204	204	(12+13)-IV-1	5.6

Asta : 36 [36 , 10036]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1370	-49	-2	15840	215	215	8	8	1.000	1.000	--	0.541	0.541	0.325	0.902

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1370	27	1	15086	204	204	(12+13)-IV-3	4.4

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Z	1370	16	1	15086	204	204	(12+13)-IV-3	5.7

Asta : 37 [37 , 10037]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1399	-19	49	15840	215	215	8	8	1.000	1.000	--	0.514	0.307	0.308	0.511

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1399	10	15	15086	204	204	(12+13)-III-1	4.7
1	Z	1399	6	25	15086	204	204	(12+13)-III-1	4.1

Asta : 38 [38 , 10038]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1368	-49	-16	15840	215	215	8	8	1.000	1.000	--	0.523	0.302	0.314	0.503

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1368	26	5	15086	204	204	(12+13)-II-3	4.2
1	Z	1368	15	8	15086	204	204	(12+13)-II-3	4.9

Asta : 39 [39 , 10039]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1360	-51	1	15840	215	215	8	8	1.000	1.000	--	0.535	0.540	0.321	0.901

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1360	28	1	15086	204	204	(12+13)-VI-1	4.4
1	Z	1360	17	1	15086	204	204	(12+13)-VI-1	5.7

Asta : 40 [40 , 10040]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1278	-46	-1	15840	215	215	8	8	1.000	1.000	--	0.536	0.540	0.322	0.901

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1278	24	1	15086	204	204	(12+13)-VI-3	4.8
1	Z	1278	15	1	15086	204	204	(12+13)-VI-3	6.2

Asta : 41 [41 , 10041]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1268	-19	50	15840	215	215	8	8	1.000	1.000	--	0.515	0.309	0.309	0.515

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1268	10	15	15086	204	204	(12+13)-III-1	4.8
1	Z	1268	6	26	15086	204	204	(12+13)-III-1	4.2

Asta : 44 [44 , 10044]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1195	50	-13	15840	215	215	8	8	1.000	1.000	--	0.524	0.306	0.314	0.510

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1195	26	4	15086	204	204	(12+13)-IV-4	4.4
1	Z	1195	16	7	15086	204	204	(12+13)-IV-4	5.3

Asta : 45 [45 , 10045]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1317	49	1	15840	215	215	8	8	1.000	1.000	--	0.535	0.543	0.321	0.905

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1317	26	1	15086	204	204	(12+13)-VIII-2	4.6
1	Z	1317	16	1	15086	204	204	(12+13)-VIII-2	5.9

Asta : 46 [46 , 10046]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1366	49	-1	15840	215	215	8	8	1.000	1.000	--	0.535	0.542	0.321	0.904

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1366	26	1	15086	204	204	(12+13)-VIII-4	4.5
1	Z	1366	16	1	15086	204	204	(12+13)-VIII-4	5.8

Asta : 47 [47 , 10047]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1378	48	16	15840	215	215	8	8	1.000	1.000	--	0.523	0.304	0.314	0.506

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1378	25	5	15086	204	204	(12+13)-VIII-2	4.2
1	Z	1378	15	8	15086	204	204	(12+13)-VIII-2	4.9

Asta : 48 [48 , 10048]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1348	47	-10	15840	215	215	8	8	1.000	1.000	--	0.523	0.302	0.314	0.504

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1348	24	3	15086	204	204	(12+13)-VI-4	4.5
1	Z	1348	15	5	15086	204	204	(12+13)-VI-4	5.4

Asta : 49 [49 , 10049]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1377	50	2	15840	215	215	8	8	1.000	1.000	--	0.535	0.540	0.321	0.901

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1377	27	1	15086	204	204	(12+13)-II-2	4.4
1	Z	1377	16	1	15086	204	204	(12+13)-II-2	5.6

Asta : 50 [50 , 10050]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1282	49	-1	15840	215	215	8	8	1.000	1.000	--	0.535	0.542	0.321	0.904

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1282	26	1	15086	204	204	(12+13)-II-4	4.6
1	Z	1282	16	1	15086	204	204	(12+13)-II-4	6.0

Asta : 51 [51 , 10051]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1321	-22	43	15840	215	215	8	8	1.000	1.000	--	0.531	0.308	0.319	0.514

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1321	12	13	15086	204	204	(12+13)-V-1	4.7
1	Z	1321	7	22	15086	204	204	(12+13)-V-1	4.3

Asta : 54 [54 , 10054]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1312	-1	-54	15840	215	215	8	8	1.000	1.000	--	0.918	0.317	0.551	0.528

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1312	1	17	15086	204	204	(12+13)-VII-3	5.7
1	Z	1312	1	29	15086	204	204	(12+13)-VII-3	4.3

Asta : 57 [57 , 10057]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1424	-1	57	15840	215	215	8	8	1.000	1.000	--	0.917	0.315	0.550	0.525

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1424	1	18	15086	204	204	(12+13)-V-1	5.3
1	Z	1424	1	30	15086	204	204	(12+13)-V-1	4.1

Asta : 58 [58 , 10058]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1427	-1	-54	15840	215	215	8	8	1.000	1.000	--	0.915	0.315	0.549	0.525

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1427	1	17	15086	204	204	(12+13)-VII-3	5.5
1	Z	1427	1	28	15086	204	204	(12+13)-VII-3	4.2

Asta : 61 [61 , 10061]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1370	-2	57	15840	215	215	8	8	1.000	1.000	--	0.690	0.315	0.414	0.526

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1370	1	18	15086	204	204	(12+13)-V-1	5.4
1	Z	1370	1	30	15086	204	204	(12+13)-V-1	4.2

Asta : 64 [64 , 10064]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1295	2	-60	15840	215	215	8	8	1.000	1.000	--	0.921	0.316	0.553

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1295	1	19	15086	204	204	(12+13)-VII-4	5.4
1	Z	1295	1	31	15086	204	204	(12+13)-VII-4	4.1

Asta : 67 [67 , 10067]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1430	1	54	15840	215	215	8	8	1.000	1.000	--	0.923	0.316	0.554

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1430	1	17	15086	204	204	(12+13)-VII-2	5.5
1	Z	1430	1	28	15086	204	204	(12+13)-VII-2	4.2

Asta : 68 [68 , 10068]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1391	2	-54	15840	215	215	8	8	1.000	1.000	--	0.920	0.315	0.552

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1391	1	17	15086	204	204	(12+13)-V-4	5.5
1	Z	1391	1	29	15086	204	204	(12+13)-V-4	4.2

Asta : 71 [71 , 10071]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1419	1	58	15840	215	215	8	8	1.000	1.000	--	0.893	0.315	0.536

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1419	1	18	15086	204	204	(12+13)-V-1	5.4
1	Z	1419	0	30	15086	204	204	(12+13)-V-1	4.1

Asta : 74 [74 , 10074]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1111	14	-55	15840	215	215	8	8	1.000	1.000	--	0.535	0.308	0.321

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1111	8	17	15086	204	204	(12+13)-V-4	5.2
1	Z	1111	5	28	15086	204	204	(12+13)-V-4	4.3

Asta : 75 [75 , 10075]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1211	-50	1	15840	215	215	8	8	1.000	1.000	--	0.536	0.542	0.321

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1211	27	1	15086	204	204	(12+13)-IV-1	4.7
1	Z	1211	16	1	15086	204	204	(12+13)-IV-1	6.1

Asta : 76 [76 , 10076]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1285	-50	-1	15840	215	215	8	8	1.000	1.000	--	0.535	0.536	0.321	0.893

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1285	26	0	15086	204	204	(12+13)-IV-3	4.6
1	Z	1285	16	1	15086	204	204	(12+13)-IV-3	6.0

Asta : 77 [77 , 10077]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1370	-50	20	15840	215	215	8	8	1.000	1.000	--	0.523	0.305	0.314	0.508

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1370	26	6	15086	204	204	(12+13)-VIII-1	4.0
1	Z	1370	16	10	15086	204	204	(12+13)-VIII-1	4.6

Asta : 78 [78 , 10078]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1064	-46	32	15840	215	215	8	8	1.000	1.000	--	0.523	0.313	0.314	0.522

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1064	24	10	15086	204	204	(12+13)-VI-1	4.2
1	Z	1064	14	17	15086	204	204	(12+13)-VI-1	4.5

Asta : 79 [79 , 10079]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1408	-51	2	15840	215	215	8	8	1.000	1.000	--	0.534	0.543	0.321	0.906

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1408	27	1	15086	204	204	(12+13)-VI-1	4.3
1	Z	1408	16	2	15086	204	204	(12+13)-VI-1	5.4

Asta : 80 [80 , 10080]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1353	-43	-2	15840	215	215	8	8	1.000	1.000	--	0.536	0.544	0.322	0.906

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1353	23	1	15086	204	204	(12+13)-VI-3	4.8
1	Z	1353	14	2	15086	204	204	(12+13)-VI-3	6.0

Asta : 81 [81 , 10081]

Sez. G: Tubo40x40x4 L=12.0 cm Ln1=12.0 cm Ln2=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: Fatt.Ampl.Sisma

= 1.1 **Verificato**

SF_λ=24.646

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-911	24	54	15840	215	215	8	8	1.000	1.000	--	0.611	0.309	0.367	0.516

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
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COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	911	15	17	15086	204	204	(12+13)-V-2	4.7
1	Z	911	9	28	15086	204	204	(12+13)-V-2	4.2

Asta : 708 [70890 , 70904]

Sez. G: Tubo40x60x4 L=40.0 cm Ln1=40.0 cm Ln2=40.0 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.776

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-50	-109	0	20240	395	294	18	26	0.997	0.978	--	1.000	0.427	0.600	0.711

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	50	109	0	19222	376	280	2	3.4
1	Z	50	65	0	18859	376	280	2	5.7

Asta : 709 [70891 , 70905]

Sez. G: Tubo40x60x4 L=40.0 cm Ln1=40.0 cm Ln2=40.0 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.776

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-69	-100	-1	20240	395	294	18	26	0.997	0.978	--	1.000	0.240	0.600	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	69	100	0	19222	376	280	2	3.7
1	Z	69	60	0	18859	376	280	2	6.1

Asta : 710 [70893 , 70907]

Sez. G: Tubo40x60x4 L=40.0 cm Ln1=40.0 cm Ln2=40.0 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.776

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
26	-63	-1	20240	395	294	18	26	0.997	0.978	--	1.000	0.360	0.600	0.600

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	26	63	0	19222	376	280	2	5.8
1	Z	26	38	1	18859	376	280	2	9.5

Asta : 711 [70888 , 70902]

Sez. G: Tubo40x60x4 L=40.0 cm Ln1=40.0 cm Ln2=40.0 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.776

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-43	-112	1	20240	395	294	18	26	0.997	0.978	--	1.000	0.266	0.600	0.444

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	43	112	0	19222	376	280	2	3.3
1	Z	43	67	0	18859	376	280	2	5.5

Asta : 712 [70887 , 70901]

Sez. G: Tubo40x60x4 L=40.0 cm Ln1=40.0 cm Ln2=40.0 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.776

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-50	-112	-0	20240	395	294	18	26	0.997	0.978	--	1.000	0.305	0.600	0.509

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	50	112	0	19222	376	280	2	3.3
1	Z	50	67	0	18859	376	280	2	5.5

Asta : 713 [70886 , 70900]

Sez. G: Tubo40x60x4 L=40.0 cm Ln1=40.0 cm Ln2=40.0 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.776

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-50	-110	1	20240	395	294	18	26	0.997	0.978	--	1.000	0.296	0.600	0.493

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	50	110	0	19222	376	280	2	3.4
1	Z	50	66	0	18859	376	280	2	5.6

Asta : 714 [70885 , 70899]

Sez. G: Tubo40x60x4 L=40.0 cm Ln1=40.0 cm Ln2=40.0 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm² **Verificato**
SF_λ=7.776

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-58	-114	-0	20240	395	294	18	26	0.997	0.978	--	0.963	0.296	0.493

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	58	110	0	19222	376	280	2	3.4
1	Z	58	66	0	18859	376	280	2	5.6

Asta : 715 [70884 , 70898]

Sez. G: Tubo40x60x4 L=40.0 cm Ln1=40.0 cm Ln2=40.0 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm² **Verificato**
SF_λ=7.776

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-58	-79	-1	20240	395	294	18	26	0.997	0.978	--	1.000	0.240	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	58	78	0	19222	376	280	2	4.7
1	Z	58	47	0	18859	376	280	2	7.7

Asta : 1813 [180209 , 180241]

Sez. G: Tubo40x60x4 L=43.2 cm Ln1=43.2 cm Ln2=43.2 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm² **Verificato**
SF_λ=7.205

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-35	-93	1	20240	395	294	20	28	0.993	0.973	--	0.913	0.240	0.548

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	35	85	0	19150	376	280	2	4.4
1	Z	35	51	1	18753	376	280	2	7.1

Asta : 1825 [180411 , 180444]

Sez. G: Tubo40x60x4 L=41.3 cm Ln1=41.3 cm Ln2=41.3 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm² **Verificato**
SF_λ=7.535

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-89	-82	1	20240	395	294	19	27	0.996	0.976	--	0.919	0.348	0.551

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	89	75	0	19193	376	280	2	4.9
1	Z	89	45	0	18816	376	280	2	7.9

Asta : 1901 [190120 , 190133]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm² **Verificato**
SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-102	-117	-1	20240	395	294	19	27	0.995	0.975	--	0.962	0.240	0.577

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	102	113	0	19184	376	280	2	3.3
1	Z	102	68	0	18803	376	280	2	5.4

Asta : 1902 [190117 , 190130]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm² **Verificato**
SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-106	-122	0	20240	395	294	19	27	0.995	0.975	--	0.960	0.379	0.576

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	106	117	0	19184	376	280	2	3.2

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Z	106	70	0	18803	376	280	2	5.2

Asta : 1903 [190118 , 190131]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-121	-133	0	20240	395	294	19	27	0.995	0.975	--	1.000	0.413	0.600	0.689

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	121	133	0	19184	376	280	2	2.8
1	Z	121	80	0	18803	376	280	2	4.6

Asta : 1904 [190119 , 190132]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-121	-133	-1	20240	395	294	19	27	0.995	0.975	--	1.000	0.240	0.600	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	121	133	0	19184	376	280	2	2.8
1	Z	121	80	0	18803	376	280	2	4.6

Asta : 1907 [190137 , 190157]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
12	235	-2	20240	395	294	19	27	0.995	0.975	--	0.509	0.240	0.305	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	12	120	0	19184	376	280	2	3.1
1	Z	12	72	1	18803	376	280	2	5.2

Asta : 1907 [190157 , 190175]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
9	-104	-1	20240	395	294	19	27	0.995	0.975	--	0.787	0.244	0.472	0.407

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	9	82	0	19184	376	280	2	4.6
1	Z	9	49	1	18803	376	280	2	7.5

Asta : 1907 [190175 , 190189]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
390	-88	-11	20240	395	294	19	27	0.995	0.975	--	0.643	0.240	0.386	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	390	56	3	19184	376	280	(12+13)-VI-2	5.6
1	Z	390	34	4	18803	376	280	(12+13)-VI-2	7.9

Asta : 1907 [190126 , 190137]

Sez. G: Tubo40x60x4 L=37.1 cm Ln1=37.1 cm Ln2=37.1 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=8.394

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-16	262	-0	20240	395	294	17	24	1.000	0.983	--	0.701	0.241	0.420	0.402

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	16	184	0	19276	376	280	2	2.0
1	Z	16	110	0	18956	376	280	2	3.4

Asta : 1908 [190141 , 190158]

Sez. G: Tubo40x60x4 L=26.8 cm Ln1=26.8 cm Ln2=26.8 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=11.599

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
12	79	3	20240	395	294	12	17	1.000	1.000	--	0.791	0.240	0.475	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	12	63	1	19276	376	280	2	5.9
1	Z	12	38	1	19276	376	280	2	9.6

Asta : 1909 [190123 , 190135]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
22	192	-1	20240	395	294	19	27	0.995	0.975	--	0.514	0.283	0.308	0.472

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	22	98	0	19184	376	280	2	3.8
1	Z	22	59	0	18803	376	280	2	6.3

Asta : 1909 [190135 , 190153]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
23	-90	-1	20240	395	294	19	27	0.995	0.975	--	0.810	0.318	0.486	0.531

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	23	73	0	19184	376	280	2	5.1
1	Z	23	44	0	18803	376	280	2	8.4

Asta : 1909 [190111 , 190123]

Sez. G: Tubo40x60x4 L=29.2 cm Ln1=29.2 cm Ln2=29.2 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=10.644

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2	220	-1	20240	395	294	13	19	1.000	0.996	--	0.741	0.240	0.445	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2	163	0	19276	376	280	2	2.3
1	Z	2	98	0	19207	376	280	2	3.8

Asta : 1912 [190124 , 190138]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
21	192	0	20240	395	294	19	27	0.995	0.975	--	0.518	0.540	0.311	0.900

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	21	99	0	19184	376	280	2	3.8
1	Z	21	60	0	18803	376	280	2	6.2

Asta : 1912 [190138 , 190161]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
22	-89	0	20240	395	294	19	27	0.995	0.975	--	0.805	0.527	0.483	0.878

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	22	71	0	19184	376	280	2	5.2
1	Z	22	43	0	18803	376	280	2	8.6

Asta : 1912 [190112 , 190124]

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Sez. G: Tubo40x60x4 L=31.5 cm Ln1=31.5 cm Ln2=31.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=9.885

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-4	222	-1	20240	395	294	15	20	1.000	0.993	--	0.727	0.240	0.436	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4	161	0	19276	376	280	2	2.3
1	Z	4	97	0	19136	376	280	2	3.9

Asta : 1914 [190139 , 190163]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
2	227	1	20240	395	294	19	27	0.995	0.975	--	0.498	0.240	0.299	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2	113	0	19184	376	280	2	3.3
1	Z	2	68	0	18803	376	280	2	5.5

Asta : 1914 [190163 , 190181]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2	-105	1	20240	395	294	19	27	0.995	0.975	--	0.802	0.301	0.481	0.501

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2	84	0	19184	376	280	2	4.5
1	Z	2	50	0	18803	376	280	2	7.4

Asta : 1914 [190181 , 190204]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
360	-90	12	20240	395	294	19	27	0.995	0.975	--	0.618	0.240	0.371	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	360	56	3	19184	376	280	(12+13)-VIII-4	5.6
1	Z	360	33	5	18803	376	280	(12+13)-VIII-4	8.0

Asta : 1914 [190127 , 190139]

Sez. G: Tubo40x60x4 L=33.5 cm Ln1=33.5 cm Ln2=33.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=9.279

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-18	248	0	20240	395	294	15	22	1.000	0.989	--	0.713	0.321	0.428	0.534

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	18	177	0	19276	376	280	2	2.1
1	Z	18	106	0	19070	376	280	2	3.5

Asta : 1915 [190128 , 190142]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-42	-94	-1	20240	395	294	19	27	0.995	0.975	--	0.948	0.240	0.569	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	42	89	0	19184	376	280	2	4.2
1	Z	42	53	0	18803	376	280	2	6.9

Asta : 1916 [190121 , 190134]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-92	-111	-1	20240	395	294	19	27	0.995	0.975	--	1.000	0.242	0.600	0.404

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	92	111	0	19184	376	280	2	3.3
1	Z	92	66	0	18803	376	280	2	5.5

Asta : 1917 [190095 , 190115]

Sez. G: Tubo40x60x4 L=35.8 cm Ln1=35.8 cm Ln2=35.8 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=8.688

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1	103	0	20240	395	294	17	23	1.000	0.986	--	0.641	0.260	0.384	0.433

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1	66	0	19276	376	280	2	5.7
1	Z	1	39	0	18997	376	280	2	9.5

Asta : 1917 [190129 , 190143]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-33	-92	1	20240	395	294	19	27	0.995	0.975	--	0.928	0.308	0.557	0.513

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	33	86	0	19184	376	280	2	4.3
1	Z	33	51	0	18803	376	280	2	7.2

Asta : 1918 [190122 , 190136]

Sez. G: Tubo40x60x4 L=41.7 cm Ln1=41.7 cm Ln2=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.465

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-91	-113	0	20240	395	294	19	27	0.995	0.975	--	1.000	0.394	0.600	0.656

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	91	113	0	19184	376	280	2	3.3
1	Z	91	68	0	18803	376	280	2	5.4

Asta : 11501 [90710 , 100710]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=7.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-297	39	0	15840	215	215	10	10	1.000	1.000	--	0.983	0.239	0.590	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	297	39	0	15086	204	204	2	4.8
1	Z	297	23	0	15086	204	204	2	7.5

Asta : 11502 [70776 , 90776]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-545	41	-1	15840	215	215	10	10	1.000	1.000	--	0.947	0.281	0.568	0.468

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	545	39	0	15086	204	204	2	4.4
1	Z	545	23	1	15086	204	204	2	6.6

Asta : 11504 [90707 , 100707]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
-308	39	3	15840	215	215	10	10	1.000	1.000	--	0.978	0.239	0.587	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	308	39	1	15086	204	204	2	4.7
1	Z	308	23	1	15086	204	204	2	7.2

Asta : 11505 [11505 , 20773]

Sez. G: Tubo40x40x4 L=27.0 cm Ln1=27.0 cm Ln2=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=10.954

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-910	43	14	15840	215	215	18	18	0.998	0.998	--	0.449	0.259	0.270	0.432

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	910	19	4	15052	204	204	(12+13)-VIII-2	5.8
1	Z	910	12	6	15052	204	204	(12+13)-VIII-2	6.8

Asta : 11505 [70773 , 90773]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=10.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-543	41	2	15840	215	215	10	10	1.000	1.000	--	0.940	0.286	0.564	0.477

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	543	39	0	15086	204	204	2	4.4
1	Z	543	23	1	15086	204	204	2	6.5

Asta : 11510 [20860 , 70860]

Sez. G: Tubo40x40x4 L=75.0 cm Ln1=75.0 cm Ln2=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=3.943

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1126	-29	4	15840	215	215	51	51	0.896	0.896	--	0.657	0.286	0.394	0.477

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1126	19	1	13515	204	204	2	5.5
1	Z	1126	11	2	13515	204	204	2	6.8

Asta : 11511 [20861 , 70861]

Sez. G: Tubo40x40x4 L=75.0 cm Ln1=75.0 cm Ln2=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=3.943

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1280	-28	-7	15840	215	215	51	51	0.896	0.896	--	0.656	0.317	0.394	0.528

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1280	18	2	13515	204	204	2	5.1
1	Z	1280	11	4	13515	204	204	2	6.0

Asta : 11514 [20859 , 70859]

Sez. G: Tubo40x40x4 L=75.0 cm Ln1=75.0 cm Ln2=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=3.943

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1055	-32	0	15840	215	215	51	51	0.896	0.896	--	0.652	0.251	0.391	0.418

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1055	21	0	13515	204	204	2	5.6
1	Z	1055	12	0	13515	204	204	2	7.2

Asta : 11515 [20858 , 70858]

Sez. G: Tubo40x40x4 L=75.0 cm Ln1=75.0 cm Ln2=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=3.943

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1033	-32	2	15840	215	215	51	51	0.896	0.896	--	0.652	0.250	0.391	0.417

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1033	21	0	13515	204	204	2	5.5
1	Z	1033	13	1	13515	204	204	2	7.0

Asta : 11516 [20857 , 70857]

Sez. G: Tubo40x40x4 L=75.0 cm Ln1=75.0 cm Ln2=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=3.943

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1219	-29	-5	15840	215	215	51	51	0.896	0.896	--	0.658	0.304	0.395	0.506

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1219	19	2	13515	204	204	2	5.2
1	Z	1219	11	3	13515	204	204	2	6.3

Asta : 11517 [20856 , 70856]

Sez. G: Tubo40x40x4 L=75.0 cm Ln1=75.0 cm Ln2=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=3.943

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1208	-33	1	15840	215	215	51	51	0.896	0.896	--	0.650	0.521	0.390	0.869

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1208	22	0	13515	204	204	2	5.1
1	Z	1208	13	0	13515	204	204	2	6.5

Asta : 11523 [90765 , 100765]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-295	40	-2	15840	215	215	10	10	1.000	1.000	--	0.991	0.239	0.594	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	295	39	0	15086	204	204	2	4.7
1	Z	295	24	1	15086	204	204	2	7.2

Asta : 11524 [70821 , 90821]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-532	33	5	15840	215	215	10	10	1.000	1.000	--	0.956	0.321	0.574	0.535

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	532	31	2	15086	204	204	2	5.1
1	Z	532	19	3	15086	204	204	2	7.1

Asta : 11525 [90746 , 100746]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-325	42	2	15840	215	215	10	10	1.000	1.000	--	0.932	0.239	0.559	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	325	39	0	15086	204	204	2	4.7
1	Z	325	23	1	15086	204	204	2	7.2

Asta : 11526 [70802 , 90802]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-544	50	2	15840	215	215	10	10	1.000	1.000	--	0.960	0.504	0.576	0.839

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	544	48	1	15086	204	204	2	3.6
1	Z	544	29	1	15086	204	204	2	5.4

Asta : 11530 [70825 , 90825]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-535	35	-5	15840	215	215	10	10	1.000	1.000	--	0.991	0.303	0.595	0.505

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	535	35	2	15086	204	204	2	4.7
1	Z	535	21	3	15086	204	204	2	6.6

Asta : 11532 [90786 , 100786]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-323	41	4	15840	215	215	10	10	1.000	1.000	--	0.969	0.239	0.581	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	323	39	1	15086	204	204	2	4.6
1	Z	323	24	2	15086	204	204	2	6.9

Asta : 11534 [90754 , 100754]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-317	42	-1	15840	215	215	10	10	1.000	1.000	--	0.931	0.239	0.558	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	317	39	0	15086	204	204	2	4.7
1	Z	317	23	0	15086	204	204	2	7.3

Asta : 11535 [70809 , 90809]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-547	51	-1	15840	215	215	10	10	1.000	1.000	--	0.961	0.400	0.576	0.667

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	547	49	1	15086	204	204	2	3.6
1	Z	547	29	1	15086	204	204	2	5.4

Asta : 11541 [90816 , 100816]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-405	29	-19	15840	215	215	10	10	1.000	1.000	--	0.982	0.239	0.589	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	405	28	4	15086	204	204	2	5.4
1	Z	405	17	7	15086	204	204	2	6.9

Asta : 11543 [90817 , 100817]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-285	30	21	15840	215	215	10	10	1.000	1.000	--	0.932	0.239	0.559	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	285	28	5	15086	204	204	2	5.6
1	Z	285	17	8	15086	204	204	2	7.1

Asta : 21498 [100644 , 110644]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-473	38	10	15840	215	215	10	10	1.000	1.000	--	0.867	0.238	0.520

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	473	33	2	15086	204	204	2	4.9
1	Z	473	20	4	15086	204	204	2	6.8

Asta : 21499 [100641 , 110641]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-554	43	-1	15840	215	215	10	10	1.000	1.000	--	0.925	0.238	0.555

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	554	40	0	15086	204	204	2	4.3
1	Z	554	24	0	15086	204	204	2	6.4

Asta : 21500 [100638 , 110638]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-554	44	1	15840	215	215	10	10	1.000	1.000	--	0.923	0.238	0.554

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	554	40	0	15086	204	204	2	4.3
1	Z	554	24	0	15086	204	204	2	6.4

Asta : 21501 [100635 , 110635]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-478	38	-10	15840	215	215	10	10	1.000	1.000	--	0.871	0.238	0.522

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	478	33	2	15086	204	204	2	4.9
1	Z	478	20	4	15086	204	204	2	6.8

Asta : 21502 [100738 , 110738]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-492	38	5	15840	215	215	10	10	1.000	1.000	--	0.900	0.238	0.540

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	492	34	1	15086	204	204	2	4.9
1	Z	492	20	2	15086	204	204	2	7.1

Asta : 21503 [21503 , 30718]

Sez. G: Tubo40x40x4 L=13.0 cm Ln1=13.0 cm Ln2=13.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=22.750

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1006	45	-14	15840	215	215	9	9	1.000	1.000	--	0.523	0.299	0.314

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1006	24	4	15086	204	204	(12+13)-II-4	4.9

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Z	1006	14	7	15086	204	204	(12+13)-II-4	5.9

Asta : 21503 [100718 , 110718]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-552	43	-2	15840	215	215	10	10	1.000	1.000	--	0.934	0.238	0.560

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	552	40	0	15086	204	204	2	4.3
1	Z	552	24	1	15086	204	204	2	6.3

Asta : 21504 [21504 , 30687]

Sez. G: Tubo40x40x4 L=13.0 cm Ln1=13.0 cm Ln2=13.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=22.750

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-997	51	-1	15840	215	215	9	9	1.000	1.000	--	0.508	0.264	0.305

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	997	26	0	15086	204	204	(12+13)-II-2	5.2
1	Z	997	15	0	15086	204	204	(12+13)-II-2	7.0

Asta : 21504 [100687 , 110687]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-552	42	0	15840	215	215	10	10	1.000	1.000	--	0.947	0.249	0.568

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	552	40	0	15086	204	204	2	4.3
1	Z	552	24	0	15086	204	204	2	6.4

Asta : 21505 [100653 , 110653]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-476	38	-10	15840	215	215	10	10	1.000	1.000	--	0.868	0.238	0.521

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	476	33	2	15086	204	204	2	4.9
1	Z	476	20	4	15086	204	204	2	6.8

Asta : 21506 [100750 , 110750]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-485	38	-6	15840	215	215	10	10	1.000	1.000	--	0.890	0.238	0.534

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	485	34	1	15086	204	204	2	4.9
1	Z	485	20	2	15086	204	204	2	7.0

Asta : 21507 [100662 , 110662]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-476	38	10	15840	215	215	10	10	1.000	1.000	--	0.866	0.238	0.519

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	476	33	2	15086	204	204	2	4.9
1	Z	476	20	4	15086	204	204	2	6.8

Asta : 21508 [21508 , 30726]

Sez. G: Tubo40x40x4 L=13.0 cm Ln1=13.0 cm Ln2=13.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=22.750

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1006	39	14	15840	215	215	9	9	1.000	1.000	--	0.516	0.299	0.309	0.498

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1006	20	4	15086	204	204	(12+13)-VIII-2	5.4
1	Z	1006	12	7	15086	204	204	(12+13)-VIII-2	6.3

Asta : 21508 [100726 , 110726]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-553	43	2	15840	215	215	10	10	1.000	1.000	--	0.939	0.238	0.564	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	553	40	0	15086	204	204	2	4.2
1	Z	553	24	1	15086	204	204	2	6.3

Asta : 21509 [100695 , 110695]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-552	42	-0	15840	215	215	10	10	1.000	1.000	--	0.948	0.238	0.569	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	552	40	0	15086	204	204	2	4.3
1	Z	552	24	0	15086	204	204	2	6.4

Asta : 21512 [100762 , 110762]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-498	40	-16	15840	215	215	10	10	1.000	1.000	--	0.847	0.238	0.508	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	498	34	4	15086	204	204	2	4.6
1	Z	498	21	6	15086	204	204	2	6.1

Asta : 21513 [100764 , 110764]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-496	39	16	15840	215	215	10	10	1.000	1.000	--	0.868	0.238	0.521	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	496	34	4	15086	204	204	2	4.6
1	Z	496	20	6	15086	204	204	2	6.1

Asta : 31498 [110563 , 130563]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-324	38	5	15840	215	215	10	10	1.000	1.000	--	0.929	0.270	0.557	0.450

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	324	35	1	15086	204	204	2	5.0
1	Z	324	21	2	15086	204	204	2	7.3

Asta : 31499 [110560 , 130560]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-305	40	-1	15840	215	215	10	10	1.000	1.000	--	0.961	0.295	0.577	0.492

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	305	38	0	15086	204	204	2	4.8
1	Z	305	23	1	15086	204	204	2	7.4

Asta : 31500 [110557 , 130557]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-304	40	1	15840	215	215	10	10	1.000	1.000	--	0.960	0.305	0.576	0.508

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	304	38	0	15086	204	204	2	4.8
1	Z	304	23	1	15086	204	204	2	7.4

Asta : 31501 [110554 , 130554]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-327	38	-5	15840	215	215	10	10	1.000	1.000	--	0.935	0.293	0.561	0.488

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	327	36	1	15086	204	204	2	4.9
1	Z	327	21	2	15086	204	204	2	7.3

Asta : 31502 [110683 , 130683]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-331	38	3	15840	215	215	10	10	1.000	1.000	--	0.957	0.439	0.574	0.732

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	331	37	1	15086	204	204	2	4.8
1	Z	331	22	2	15086	204	204	2	7.2

Asta : 31503 [110649 , 130649]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-297	39	-2	15840	215	215	10	10	1.000	1.000	--	0.971	0.268	0.583	0.447

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	297	38	0	15086	204	204	2	4.8
1	Z	297	23	1	15086	204	204	2	7.4

Asta : 31504 [110608 , 130608]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-309	39	1	15840	215	215	10	10	1.000	1.000	--	0.983	0.426	0.590	0.710

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	309	38	0	15086	204	204	2	4.8
1	Z	309	23	1	15086	204	204	2	7.4

Asta : 31505 [110576 , 130576]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-322	38	-6	15840	215	215	10	10	1.000	1.000	--	0.932	0.267	0.559	0.445

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	322	35	1	15086	204	204	2	5.0
1	Z	322	21	2	15086	204	204	2	7.3

Asta : 31506 [110617 , 130617]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-310	39	-1	15840	215	215	10	10	1.000	1.000	--	0.985	0.502	0.591	0.837

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	310	38	0	15086	204	204	2	4.8
1	Z	310	23	1	15086	204	204	2	7.4

Asta : 31507 [110658 , 130658]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-299	39	2	15840	215	215	10	10	1.000	1.000	--	0.977	0.239	0.586	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	299	38	0	15086	204	204	2	4.8
1	Z	299	23	1	15086	204	204	2	7.4

Asta : 31508 [110691 , 130691]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-334	39	-2	15840	215	215	10	10	1.000	1.000	--	0.950	0.523	0.570	0.871

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	334	37	1	15086	204	204	2	4.8
1	Z	334	22	2	15086	204	204	2	7.2

Asta : 31509 [110585 , 130585]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-321	38	5	15840	215	215	10	10	1.000	1.000	--	0.931	0.268	0.558	0.447

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	321	35	1	15086	204	204	2	5.0
1	Z	321	21	2	15086	204	204	2	7.3

Asta : 31512 [110734 , 130734]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-586	38	-9	15840	215	215	10	10	1.000	1.000	--	0.991	0.246	0.594	0.409

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	586	38	2	15086	204	204	2	4.3
1	Z	586	23	4	15086	204	204	2	6.0

Asta : 31513 [110735 , 130735]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
-440	40	9	15840	215	215	10	10	1.000	1.000	--	0.935	0.239	0.561	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	440	37	2	15086	204	204	2	4.5
1	Z	440	22	4	15086	204	204	2	6.4

Asta : 50445 [130445 , 140445]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-402	27	-12	15840	215	215	10	10	1.000	1.000	--	0.986	0.284	0.591	0.474

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	402	27	3	15086	204	204	2	5.8
1	Z	402	16	6	15086	204	204	2	7.6

Asta : 50449 [130449 , 140449]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-551	43	1	15840	215	215	10	10	1.000	1.000	--	0.907	0.342	0.544	0.569

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	551	39	0	15086	204	204	2	4.3
1	Z	551	24	1	15086	204	204	2	6.5

Asta : 50453 [130453 , 140453]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-549	43	-1	15840	215	215	10	10	1.000	1.000	--	0.908	0.459	0.545	0.766

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	549	39	0	15086	204	204	2	4.4
1	Z	549	24	0	15086	204	204	2	6.5

Asta : 50457 [130457 , 140457]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-391	28	10	15840	215	215	10	10	1.000	1.000	--	0.964	0.279	0.579	0.465

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	391	27	3	15086	204	204	2	5.9
1	Z	391	16	5	15086	204	204	2	7.8

Asta : 50490 [130490 , 140490]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-421	27	-11	15840	215	215	10	10	1.000	1.000	--	0.952	0.306	0.571	0.510

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	421	26	3	15086	204	204	2	5.9
1	Z	421	16	5	15086	204	204	2	7.7

Asta : 50499 [130499 , 140499]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-489	26	11	15840	215	215	10	10	1.000	1.000	--	0.937	0.345	0.562	0.575

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	489	25	4	15086	204	204	2	5.8
1	Z	489	15	6	15086	204	204	2	7.4

Asta : 50527 [130527 , 140527]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-546	43	0	15840	215	215	10	10	1.000	1.000	--	0.920	0.569	0.552	0.949

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	546	39	0	15086	204	204	2	4.4
1	Z	546	23	0	15086	204	204	2	6.5

Asta : 50540 [130540 , 140540]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-545	42	-1	15840	215	215	10	10	1.000	1.000	--	0.920	0.452	0.552	0.754

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	545	39	0	15086	204	204	2	4.4
1	Z	545	23	1	15086	204	204	2	6.5

Asta : 50570 [130570 , 140570]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-552	43	-0	15840	215	215	10	10	1.000	1.000	--	0.916	0.238	0.550	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	552	39	0	15086	204	204	2	4.4
1	Z	552	23	0	15086	204	204	2	6.6

Asta : 50580 [130580 , 140580]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-553	43	1	15840	215	215	10	10	1.000	1.000	--	0.919	0.238	0.552	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	553	39	0	15086	204	204	2	4.4
1	Z	553	24	0	15086	204	204	2	6.5

Asta : 50612 [130612 , 140612]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-324	30	-8	15840	215	215	10	10	1.000	1.000	--	0.951	0.239	0.570	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	324	29	2	15086	204	204	2	5.8
1	Z	324	17	3	15086	204	204	2	8.2

Asta : 50676 [130676 , 140676]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-382	28	-18	15840	215	215	10	10	1.000	1.000	--	0.998	0.244	0.599	0.407

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	382	28	4	15086	204	204	2	5.5
1	Z	382	17	7	15086	204	204	2	7.0

Asta : 61499 [140357 , 160357]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-332	40	-1	15840	215	215	10	10	1.000	1.000	--	0.948	0.239	0.569	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	332	38	0	15086	204	204	2	4.8
1	Z	332	23	0	15086	204	204	2	7.4

Asta : 61500 [140354 , 160354]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-331	40	1	15840	215	215	10	10	1.000	1.000	--	0.947	0.239	0.568	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	331	38	0	15086	204	204	2	4.8
1	Z	331	23	1	15086	204	204	2	7.3

Asta : 61503 [140481 , 160481]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-321	40	-2	15840	215	215	10	10	1.000	1.000	--	0.957	0.239	0.574	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	321	38	0	15086	204	204	2	4.8
1	Z	321	23	1	15086	204	204	2	7.4

Asta : 61504 [140424 , 160424]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-327	39	1	15840	215	215	10	10	1.000	1.000	--	0.959	0.239	0.576	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	327	38	0	15086	204	204	2	4.8
1	Z	327	23	0	15086	204	204	2	7.5

Asta : 61506 [140437 , 160437]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-329	39	-0	15840	215	215	10	10	1.000	1.000	--	0.959	0.350	0.575	0.583

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	329	38	0	15086	204	204	2	4.8
1	Z	329	23	0	15086	204	204	2	7.5

Asta : 61507 [140495 , 160495]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-320	40	2	15840	215	215	10	10	1.000	1.000	--	0.960	0.239	0.576	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	320	38	0	15086	204	204	2	4.8
1	Z	320	23	1	15086	204	204	2	7.3

Asta : 61516 [140600 , 160600]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-364	41	-7	15840	215	215	10	10	1.000	1.000	--	0.984	0.239	0.591	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	364	40	2	15086	204	204	2	4.4
1	Z	364	24	3	15086	204	204	2	6.4

Asta : 70262 [160262 , 170262]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-409	32	-12	15840	215	215	10	10	1.000	1.000	--	0.880	0.239	0.528	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	409	28	3	15086	204	204	2	5.6
1	Z	409	17	5	15086	204	204	2	7.5

Asta : 70266 [160266 , 170266]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-557	44	-1	15840	215	215	10	10	1.000	1.000	--	0.912	0.238	0.547	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	557	40	0	15086	204	204	2	4.3
1	Z	557	24	0	15086	204	204	2	6.4

Asta : 70270 [160270 , 170270]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-557	44	1	15840	215	215	10	10	1.000	1.000	--	0.912	0.238	0.547	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	557	40	0	15086	204	204	2	4.3
1	Z	557	24	0	15086	204	204	2	6.5

Asta : 70274 [160274 , 170274]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-391	31	12	15840	215	215	10	10	1.000	1.000	--	0.882	0.239	0.529	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	391	27	3	15086	204	204	2	5.8
1	Z	391	16	5	15086	204	204	2	7.7

Asta : 70279 [160279 , 170279]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ $f_{yk}/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm²: **Verificato**
SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-388	31	13	15840	215	215	10	10	1.000	1.000	--	0.885	0.239	0.531	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	388	28	3	15086	204	204	2	5.7

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Z	388	17	5	15086	204	204	2	7.6

Asta : 70283 [160283 , 170283]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-399	32	-13	15840	215	215	10	10	1.000	1.000	--	0.887	0.239	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	399	29	3	15086	204	204	2	5.5
1	Z	399	17	5	15086	204	204	2	7.3

Asta : 70290 [160290 , 170290]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-383	31	-13	15840	215	215	10	10	1.000	1.000	--	0.898	0.239	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	383	28	3	15086	204	204	2	5.7
1	Z	383	17	5	15086	204	204	2	7.6

Asta : 70294 [160294 , 170294]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-374	30	13	15840	215	215	10	10	1.000	1.000	--	0.903	0.239	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	374	27	3	15086	204	204	2	5.8
1	Z	374	16	5	15086	204	204	2	7.6

Asta : 70303 [160303 , 170303]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-389	30	-12	15840	215	215	10	10	1.000	1.000	--	0.912	0.239	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	389	27	3	15086	204	204	2	5.8
1	Z	389	16	5	15086	204	204	2	7.8

Asta : 70312 [160312 , 170312]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-388	29	12	15840	215	215	10	10	1.000	1.000	--	0.911	0.239	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	388	27	3	15086	204	204	2	5.9
1	Z	388	16	5	15086	204	204	2	7.8

Asta : 70333 [160333 , 170333]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-552	42	-1	15840	215	215	10	10	1.000	1.000	--	0.936	0.238	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	552	39	0	15086	204	204	2	4.3
1	Z	552	24	0	15086	204	204	2	6.5

Asta : 70346 [160346 , 170346]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-553	42	0	15840	215	215	10	10	1.000	1.000	--	0.934	0.240	0.560	0.401

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	553	39	0	15086	204	204	2	4.3
1	Z	553	24	0	15086	204	204	2	6.5

Asta : 70384 [160384 , 170384]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-553	42	1	15840	215	215	10	10	1.000	1.000	--	0.944	0.238	0.567	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	553	40	0	15086	204	204	2	4.3
1	Z	553	24	0	15086	204	204	2	6.5

Asta : 70396 [160396 , 170396]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-555	42	-2	15840	215	215	10	10	1.000	1.000	--	0.949	0.238	0.569	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	555	40	0	15086	204	204	2	4.3
1	Z	555	24	1	15086	204	204	2	6.4

Asta : 70418 [160418 , 170418]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-402	30	11	15840	215	215	10	10	1.000	1.000	--	0.938	0.239	0.563	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	402	29	3	15086	204	204	2	5.6
1	Z	402	17	4	15086	204	204	2	7.6

Asta : 70429 [160429 , 170429]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-410	29	-9	15840	215	215	10	10	1.000	1.000	--	0.972	0.239	0.583	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	410	28	2	15086	204	204	2	5.7
1	Z	410	17	4	15086	204	204	2	7.8

Asta : 70461 [160461 , 170461]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-408	29	15	15840	215	215	10	10	1.000	1.000	--	0.986	0.239	0.592	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	408	29	4	15086	204	204	2	5.4
1	Z	408	17	6	15086	204	204	2	7.1

Asta : 70474 [160474 , 170474]

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Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-368	28	14	15840	215	215	10	10	1.000	1.000	--	0.936	0.239	0.562	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	368	26	3	15086	204	204	2	5.9
1	Z	368	16	6	15086	204	204	2	7.8

Asta : 70518 [160518 , 170518]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-406	30	-9	15840	215	215	10	10	1.000	1.000	--	0.975	0.239	0.585	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	406	29	2	15086	204	204	2	5.5
1	Z	406	18	4	15086	204	204	2	7.6

Asta : 70532 [70532 , 80532]

Sez. G: Tubo40x40x4 L=13.0 cm Ln1=13.0 cm Ln2=13.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=22.750

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-910	44	-17	15840	215	215	9	9	1.000	1.000	--	0.500	0.308	0.300	0.513

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	910	22	5	15086	204	204	(12+13)-VII-4	5.2
1	Z	910	13	9	15086	204	204	(12+13)-VII-4	6.0

Asta : 70553 [160553 , 170553]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-416	34	-18	15840	215	215	10	10	1.000	1.000	--	0.822	0.239	0.493	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	416	28	4	15086	204	204	2	5.3
1	Z	416	17	7	15086	204	204	2	6.8

Asta : 91499 [170198 , 180198]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-309	36	-2	15840	215	215	10	10	1.000	1.000	--	0.960	0.239	0.576	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	309	34	0	15086	204	204	2	5.3
1	Z	309	20	1	15086	204	204	2	8.0

Asta : 91500 [170195 , 180195]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-309	36	2	15840	215	215	10	10	1.000	1.000	--	0.960	0.239	0.576	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	309	34	0	15086	204	204	2	5.3
1	Z	309	20	1	15086	204	204	2	8.0

Asta : 91503 [170299 , 180299]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-276	35	-3	15840	215	215	10	10	1.000	1.000	--	0.996	0.239	0.598	0.399

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	276	35	1	15086	204	204	2	5.2
1	Z	276	21	1	15086	204	204	2	8.0

Asta : 91504 [170251 , 180251]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-293	36	1	15840	215	215	10	10	1.000	1.000	--	0.982	0.239	0.589	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	293	36	0	15086	204	204	2	5.1
1	Z	293	21	1	15086	204	204	2	7.9

Asta : 91506 [170258 , 180258]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-294	36	-1	15840	215	215	10	10	1.000	1.000	--	0.980	0.239	0.588	0.398

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	294	36	0	15086	204	204	2	5.1
1	Z	294	21	1	15086	204	204	2	7.9

Asta : 91507 [170308 , 180308]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-268	34	3	15840	215	215	10	10	1.000	1.000	--	0.997	0.239	0.598	0.399

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	268	34	1	15086	204	204	2	5.4
1	Z	268	20	1	15086	204	204	2	8.2

Asta : 91519 [170566 , 180566]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-341	42	33	15840	215	215	10	10	1.000	1.000	--	0.778	0.483	0.467	0.806

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	341	33	16	15086	204	204	2	3.8
1	Z	341	20	27	15086	204	204	2	4.0

Asta : 91520 [170480 , 180480]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.717

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-590	58	-18	15840	215	215	10	10	1.000	1.000	--	0.879	0.238	0.527	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	590	51	4	15086	204	204	2	3.2
1	Z	590	31	7	15086	204	204	2	4.5

Asta : 101498 [180145 , 190145]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
-730	86	-11	15840	215	215	10	10	1.000	1.000	--	0.897	0.256	0.538	0.427

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	730	77	3	15086	204	204	2	2.3
1	Z	730	46	5	15086	204	204	2	3.4

Asta : 101499 [180146 , 190146]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-787	95	2	15840	215	215	10	10	1.000	1.000	--	0.922	0.237	0.553	0.396

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	787	87	1	15086	204	204	2	2.1
1	Z	787	52	1	15086	204	204	2	3.2

Asta : 101500 [180147 , 190147]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-790	94	-2	15840	215	215	10	10	1.000	1.000	--	0.922	0.250	0.553	0.416

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	790	87	0	15086	204	204	2	2.1
1	Z	790	52	1	15086	204	204	2	3.2

Asta : 101501 [180150 , 190150]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-694	83	12	15840	215	215	10	10	1.000	1.000	--	0.899	0.238	0.539	0.396

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	694	74	3	15086	204	204	2	2.4
1	Z	694	45	5	15086	204	204	2	3.5

Asta : 101503 [101503 , 110224]

Sez. G: Tubo40x40x4 L=11.0 cm Ln1=11.0 cm Ln2=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=26.886

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1082	42	-13	15840	215	215	7	7	1.000	1.000	--	0.503	0.311	0.302	0.518

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1082	21	4	15086	204	204	(12+13)-II-4	5.1
1	Z	1082	13	7	15086	204	204	(12+13)-II-4	6.0

Asta : 101503 [180224 , 190224]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-291	36	-21	15840	215	215	10	10	1.000	1.000	--	0.775	0.563	0.465	0.938

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	291	28	12	15086	204	204	2	4.7
1	Z	291	17	20	15086	204	204	2	5.1

Asta : 101505 [180189 , 190189]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-687	59	9	15840	215	215	10	10	1.000	1.000	--	0.998	0.261	0.599	0.435

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	687	59	2	15086	204	204	2	2.9
1	Z	687	35	4	15086	204	204	2	4.2

Asta : 101506 [180173 , 190173]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-552	51	-15	15840	215	215	10	10	1.000	1.000	--	0.995	0.238	0.597

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	552	51	4	15086	204	204	2	3.3
1	Z	552	31	6	15086	204	204	2	4.6

Asta : 101507 [101507 , 110232]

Sez. G: Tubo40x40x4 L=11.0 cm Ln1=11.0 cm Ln2=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=26.886

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1121	37	17	15840	215	215	7	7	1.000	1.000	--	0.514	0.311	0.308

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1121	19	5	15086	204	204	(12+13)-IV-2	5.2
1	Z	1121	11	9	15086	204	204	(12+13)-IV-2	5.8

Asta : 101507 [180232 , 190232]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-303	41	19	15840	215	215	10	10	1.000	1.000	--	0.614	0.585	0.368

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	303	25	11	15086	204	204	2	5.1
1	Z	303	15	18	15086	204	204	2	5.5

Asta : 101508 [180176 , 190176]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-547	51	16	15840	215	215	10	10	1.000	1.000	--	0.992	0.238	0.595

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	547	50	4	15086	204	204	2	3.3
1	Z	547	30	6	15086	204	204	2	4.7

Asta : 101510 [180204 , 190204]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-695	60	-9	15840	215	215	10	10	1.000	1.000	--	0.991	0.256	0.594

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	695	60	2	15086	204	204	2	2.9
1	Z	695	36	4	15086	204	204	2	4.1

Asta : 101511 [180154 , 190154]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-657	78	-13	15840	215	215	10	10	1.000	1.000	--	0.914	0.238	0.548

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	657	72	3	15086	204	204	2	2.4
1	Z	657	43	5	15086	204	204	2	3.6

Asta : 101512 [180165 , 190165]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-612	65	8	15840	215	215	10	10	1.000	1.000	--	0.942	0.238	0.565	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	612	62	2	15086	204	204	2	2.9
1	Z	612	37	3	15086	204	204	2	4.2

Asta : 101513 [180168 , 190168]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-591	62	8	15840	215	215	10	10	1.000	1.000	--	0.952	0.238	0.571	0.397

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	591	59	2	15086	204	204	2	2.9
1	Z	591	36	3	15086	204	204	2	4.4

Asta : 101514 [180162 , 190162]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-676	80	12	15840	215	215	10	10	1.000	1.000	--	0.918	0.238	0.551	0.396

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	676	73	3	15086	204	204	2	2.4
1	Z	676	44	5	15086	204	204	2	3.5

Asta : 110097 [110097 , 190097]

Sez. G: Tubo40x40x4 L=90.0 cm Ln1=90.0 cm Ln2=90.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=3.286

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-684	-63	3	15840	215	215	61	61	0.847	0.847	--	0.411	0.250	0.246	0.417

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	684	26	1	12781	204	204	2	5.4
1	Z	684	15	1	12781	204	204	2	7.3

Asta : 110098 [110098 , 190098]

Sez. G: Tubo40x40x4 L=90.0 cm Ln1=90.0 cm Ln2=90.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=3.286

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-764	-70	-0	15840	215	215	61	61	0.847	0.847	--	0.412	0.414	0.247	0.690

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	764	29	0	12781	204	204	2	5.0
1	Z	764	17	0	12781	204	204	2	6.9

Asta : 110099 [110099 , 190099]

Sez. G: Tubo40x40x4 L=90.0 cm Ln1=90.0 cm Ln2=90.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=3.286

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-767	-70	1	15840	215	215	61	61	0.847	0.847	--	0.412	0.252	0.247	0.419

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	767	29	0	12781	204	204	2	4.9
1	Z	767	17	0	12781	204	204	2	6.8

Asta : 110101 [110101 , 190101]

Sez. G: Tubo40x40x4 L=90.0 cm Ln1=90.0 cm Ln2=90.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=3.286

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-655	-61	-4	15840	215	215	61	61	0.847	0.847	--	0.410	0.264	0.246	0.440

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	655	25	1	12781	204	204	2	5.6
1	Z	655	15	2	12781	204	204	2	7.6

Asta : 110107 [110107 , 190107]

Sez. G: Tubo40x40x4 L=90.0 cm Ln1=90.0 cm Ln2=90.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=3.286

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-791	-52	8	15840	215	215	61	61	0.847	0.847	--	0.412	0.252	0.247	0.420

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	791	21	2	12781	204	204	2	5.6
1	Z	791	13	3	12781	204	204	2	7.0

Asta : 110109 [110109 , 190109]

Sez. G: Tubo40x40x4 L=90.0 cm Ln1=90.0 cm Ln2=90.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=3.286

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-867	-51	-8	15840	215	215	61	61	0.847	0.847	--	0.414	0.253	0.248	0.422

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	867	21	2	12781	204	204	2	5.5
1	Z	867	13	3	12781	204	204	2	6.8

Asta : 110137 [110137 , 190137]

Sez. G: Tubo40x40x4 L=90.0 cm Ln1=90.0 cm Ln2=90.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=3.286

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1827	21	5	15840	215	215	61	61	0.847	0.847	--	0.470	0.268	0.282	0.446

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1827	10	1	12781	204	204	2	5.1
1	Z	1827	6	2	12781	204	204	2	5.5

Asta : 110139 [110139 , 190139]

Sez. G: Tubo40x40x4 L=90.0 cm Ln1=90.0 cm Ln2=90.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=3.286

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1791	17	-3	15840	215	215	61	61	0.847	0.847	--	0.480	0.267	0.288	0.445

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1791	8	1	12781	204	204	2	5.4
1	Z	1791	5	2	12781	204	204	2	5.8

Asta : 110158 [180158 , 190158]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-612	25	-37	15840	215	215	10	10	1.000	1.000	--	0.598	0.566	0.359	0.943

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	612	15	21	15086	204	204	2	4.7

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Z	612	9	34	15086	204	204	2	4.0

Asta : 110164 [180164 , 190164]

Sez. G: Tubo40x40x4 L=15.0 cm Ln1=15.0 cm Ln2=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**
 SF_λ=19.716

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-556	32	32	15840	215	215	10	10	1.000	1.000	--	0.448	0.585	0.269	0.975

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	556	14	18	15086	204	204	2	5.1
1	Z	556	9	31	15086	204	204	2	4.4

Verifica Resistenza aste Metalliche più sollecitate

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Asta : 3 [70003 , 120003]

Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-22	-49	55	-2	-20	-14	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4304	4304	204	204	139	78	5.9	86	5.9

Asta : 4 [4 , 10004]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1386	-268	-477	1	47	-25	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4309	4309	204	204	139	9.0	2.3	94	2.3

Asta : 4 [40004 , 70004]

Sez. G: Tubo40x40x4 L=43.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-544	-106	143	-0	43	27	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	15086	4345	4345	204	204	139	30	2.6	>100	2.6

Asta : 4 [70004 , 120004]

Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-355	66	79	1	-30	20	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4327	4327	204	204	139	55	3.7	>100	3.7

Asta : 5 [5 , 10005]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1523	0	-533	0	51	0	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	8.2	2.8	>100	2.8

Asta : 5 [40005 , 70005]

Sez. G: Tubo40x40x4 L=43.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-766	-111	219	-1	63	29	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	15086	4314	4314	204	204	139	20	2.0	>100	2.0

Asta : 5 [70005 , 120005]

Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-578	-9	194	-1	-69	-3	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4332	4332	204	204	139	22	2.6	>100	2.6

Asta : 5 [120005 , 150005]

Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-220	9	-143	-0	32	2	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4343	4343	204	204	139	30	5.5	>100	5.5

Asta : 6 [6 , 10006]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1567	1	-437	-0	45	-2	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	10.0	3.0	>100	3.0

Asta : 6 [40006 , 70006]

Sez. G: Tubo40x40x4 L=43.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-1503	14	164	0	58	-4	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	15086	4348	4348	204	204	139	27	2.5	>100	2.5

Asta : 6 [70006 , 120006]

Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-727	-2	112	-0	-48	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	39	3.5	>100	3.5

Asta : 7 [7 , 10007]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1373	-187	-465	-1	46	-19	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4316	4316	204	204	139	9.3	2.5	>100	2.5

Asta : 7 [40007 , 70007]

Sez. G: Tubo40x40x4 L=43.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
43	1	-1509	18	162	-0	58	-4	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	15086	4353	4353	204	204	139	27	2.5	>100	2.5

Asta : 7 [70007 , 120007]

Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-722	-3	114	-0	-49	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	38	3.4	>100	3.4

Asta : 8 [8 , 10008]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1665	-246	-420	0	42	-23	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4345	4345	204	204	139	10	2.3	>100	2.3

Asta : 8 [40008 , 70008]

Sez. G: Tubo40x40x4 L=43.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-1500	-19	159	0	58	4	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	15086	4353	4353	204	204	139	27	2.5	>100	2.5

Asta : 8 [70008 , 120008]

Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-713	3	115	0	-49	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4352	4352	204	204	139	38	3.4	>100	3.4

Asta : 9 [9 , 10009]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1579	-1	-440	-0	46	1	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4355	4355	204	204	139	9.9	3.0	>100	3.0

Asta : 9 [40009 , 70009]

Sez. G: Tubo40x40x4 L=43.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-1492	-16	166	-0	58	4	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	15086	4347	4347	204	204	139	26	2.5	>100	2.5

Asta : 9 [70009 , 120009]

Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-718	2	110	-0	-47	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
---	-----	----	-----	-----	-----	-----	------	-------	------	-------	----

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4351	4351	204	204	139	40	3.5	>100	3.5

Asta : 10 [10 , 10010]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1525	-1	-505	0	49	-2	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	8.6	2.9	>100	2.9

Asta : 10 [40010 , 70010]

Sez. G: Tubo40x40x4 L=43.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-766	-112	189	-1	55	29	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	15086	4330	4330	204	204	139	23	2.1	>100	2.1

Asta : 10 [70010 , 120010]

Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-579	-29	166	0	-60	-9	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4353	4353	204	204	139	26	2.6	>100	2.6

Asta : 10 [120010 , 150010]

Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-213	22	-124	0	28	5	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4344	4344	204	204	139	35	5.7	>100	5.7

Asta : 11 [11 , 10011]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1102	529	219	3	-20	51	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4276	4276	204	204	139	8.1	2.4	55	2.4

Asta : 11 [40011 , 70011]

Sez. G: Tubo40x40x4 L=43.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-820	121	161	1	49	-30	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	15086	4338	4338	204	204	139	27	2.3	>100	2.3

Asta : 11 [70011 , 120011]

Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-242	70	90	1	-34	23	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4320	4320	204	204	139	48	3.4	>100	3.4

Asta : 12 [70012 , 120012]Sez. G: Tubo40x40x4 L=57.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-56	35	173	2	-56	12	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4288	4288	204	204	139	25	3.0	65	3.0

Asta : 12 [120012 , 150012]Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-88	-22	-172	1	40	-6	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4310	4310	204	204	139	25	4.3	98	4.3

Asta : 14 [14 , 10014]Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1107	-497	5	0	-2	-51	--	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4350	4350	204	204	139	8.8	3.0	>100	3.0

Asta : 17 [17 , 10017]Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1370	489	4	0	-2	50	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	8.9	2.9	>100	2.9

Asta : 18 [18 , 10018]Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1338	-460	4	0	-2	-47	--	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	9.5	3.0	>100	3.0

Asta : 21 [21 , 10021]Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1231	475	5	-0	-3	49	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4350	4350	204	204	139	9.2	3.0	>100	3.0

Asta : 24 [24 , 10024]Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1369	-533	-3	-0	2	-55	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4351	4351	204	204	139	8.2	2.7	>100	2.7

Asta : 27 [27 , 10027]Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1416	542	-2	0	1	56	--	--	(12+13)-I-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4344	4344	204	204	139	8.0	2.7	>100	2.7

Asta : 28 [28 , 10028]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1401	-516	-2	-0	1	-53	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4344	4344	204	204	139	8.4	2.8	>100	2.8

Asta : 31 [31 , 10031]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1448	510	-1	0	1	53	--	--	(12+13)-I-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4344	4344	204	204	139	8.5	2.8	>100	2.8

Asta : 34 [34 , 10034]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-852	-514	-225	1	23	-52	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4311	4311	204	204	139	8.4	2.4	99	2.4

Asta : 35 [35 , 10035]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1365	2	507	0	-52	1	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	8.6	2.8	>100	2.8

Asta : 36 [36 , 10036]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1370	-3	476	-0	-49	-2	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4353	4353	204	204	139	9.1	3.0	>100	3.0

Asta : 37 [37 , 10037]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1399	487	193	1	-19	49	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4313	4313	204	204	139	8.9	2.3	>100	2.3

Asta : 38 [38 , 10038]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1377	-474	182	-1	-18	-48	--	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4315	4315	204	204	139	9.1	2.4	>100	2.4

Asta : 39 [39 , 10039]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1360	2	498	0	-51	1	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	8.7	2.9	>100	2.9

Asta : 40 [40 , 10040]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1278	-2	441	-0	-46	-1	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4346	4346	204	204	139	9.9	3.2	>100	3.2

Asta : 41 [41 , 10041]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1268	495	191	1	-19	50	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4317	4317	204	204	139	8.7	2.4	>100	2.4

Asta : 44 [44 , 10044]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1181	-453	-203	1	20	-46	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4318	4318	204	204	139	9.5	2.5	>100	2.5

Asta : 45 [45 , 10045]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1317	2	-473	-0	49	1	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4353	4353	204	204	139	9.2	3.0	>100	3.0

Asta : 46 [46 , 10046]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1366	-2	-479	0	49	-1	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4353	4353	204	204	139	9.1	3.0	>100	3.0

Asta : 47 [47 , 10047]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1378	165	-479	-1	48	16	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4326	4326	204	204	139	9.0	2.5	>100	2.5

Asta : 48 [48 , 10048]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1045	142	-480	1	48	15	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4314	4314	204	204	139	9.0	2.6	>100	2.6

Asta : 49 [49 , 10049]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1377	2	-488	-0	50	2	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	8.9	2.9	>100	2.9

Asta : 50 [50 , 10050]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1282	-2	-471	0	49	-1	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4346	4346	204	204	139	9.2	3.0	>100	3.0

Asta : 51 [51 , 10051]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1321	430	219	1	-22	43	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4316	4316	204	204	139	10	2.4	>100	2.4

Asta : 54 [54 , 10054]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1312	-525	3	0	-1	-54	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	8.3	2.8	>100	2.8

Asta : 57 [57 , 10057]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1424	552	2	-0	-1	57	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4347	4347	204	204	139	7.9	2.6	>100	2.6

Asta : 58 [58 , 10058]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1427	-523	2	0	-1	-54	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4353	4353	204	204	139	8.3	2.7	>100	2.7

Asta : 61 [61 , 10061]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1370	547	3	-0	-2	57	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4343	4343	204	204	139	7.9	2.7	>100	2.7

Asta : 64 [64 , 10064]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1295	-577	-3	0	2	-60	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	7.5	2.6	>100	2.6

Asta : 67 [67 , 10067]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1430	518	-2	0	1	54	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	8.4	2.8	>100	2.8

Asta : 68 [68 , 10068]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1391	-526	-3	-0	2	-54	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	8.3	2.7	>100	2.7

Asta : 71 [71 , 10071]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1419	560	-1	-0	1	58	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4347	4347	204	204	139	7.8	2.6	>100	2.6

Asta : 74 [74 , 10074]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1111	-550	-136	2	14	-55	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4300	4300	204	204	139	7.8	2.4	80	2.4

Asta : 75 [75 , 10075]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1211	2	481	0	-50	1	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4346	4346	204	204	139	9.0	3.0	>100	3.0

Asta : 76 [76 , 10076]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1285	-1	480	-0	-50	-1	--	--	(12+13)-IV-3

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	9.1	3.0	>100	3.0

Asta : 77 [77 , 10077]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1306	335	427	-2	-43	33	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4304	4304	204	204	139	10	2.2	86	2.2

Asta : 78 [78 , 10078]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1064	318	458	-2	-46	32	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4305	4305	204	204	139	9.4	2.2	88	2.2

Asta : 79 [79 , 10079]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1408	4	497	0	-51	2	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4342	4342	204	204	139	8.7	2.8	>100	2.8

Asta : 80 [80 , 10080]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1066	-2	471	0	-49	-1	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4350	4350	204	204	139	9.2	3.2	>100	3.2

Asta : 81 [81 , 10081]

Sez. G: Tubo40x40x4 L=12.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² Fatt.Ampl.Sisma = 1.1 : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-911	536	-231	-2	24	54	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4291	4291	204	204	139	8.0	2.3	69	2.3

Asta : 702 [70776 , 70814]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	134	-5	-263	1	-79	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4433	6649	376	280	220	25	4.6	>100	4.6

Asta : 702 [70814 , 70832]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	134	3	254	-1	-79	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4425	6637	376	280	220	26	4.6	>100	4.6

Asta : 703 [70773 , 70813]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	130	4	-261	-1	-78	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4434	6652	376	280	220	26	4.6	>100	4.6

Asta : 703 [70813 , 70830]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	129	-4	257	2	-79	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4415	6623	376	280	220	26	4.6	>100	4.6

Asta : 705 [70834 , 70832]

Sez. G: Tubo40x60x4 L=116.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	121	0	-317	-2	70	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4417	6625	376	280	220	21	5.2	>100	5.2

Asta : 705 [70830 , 70828]

Sez. G: Tubo40x60x4 L=116.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
116	1	121	-1	311	2	67	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
116	1	19276	4417	6626	376	280	220	21	5.4	>100	5.4

Asta : 705 [70828 , 70840]

Sez. G: Tubo40x60x4 L=95.1 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2	2	-365	4	93	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4362	6542	376	280	220	18	4.0	49	4.0

Asta : 705 [70838 , 70834]

Sez. G: Tubo40x60x4 L=96.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
96	1	-4	-2	367	-3	90	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	19276	4385	6578	376	280	220	18	4.1	67	4.1

Asta : 707 [70860 , 70889]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-57	5	-466	-2	-109	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4412	6617	376	280	220	14	3.4	>100	3.4

Asta : 707 [70889 , 70903]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
8	1	-57	-1	-1	-0	-109	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
8	1	19276	4445	6668	376	280	220	>100	3.4	>100	3.4

Asta : 707 [70903 , 70009]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-56	-0	546	-0	105	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4446	6669	376	280	220	12	3.5	>100	3.5

Asta : 708 [70861 , 70890]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-49	-9	-477	4	-108	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4369	6554	376	280	220	14	3.4	54	3.4

Asta : 708 [70890 , 70904]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
12	1	-50	-0	2	0	-109	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
12	1	19276	4442	6664	376	280	220	>100	3.4	>100	3.4

Asta : 708 [70904 , 70010]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-52	-2	550	0	106	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4448	6672	376	280	220	12	3.5	>100	3.5

Asta : 709 [70862 , 70891]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-70	-3	-437	0	-102	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4450	6675	376	280	220	15	3.6	>100	3.6

Asta : 709 [70891 , 70905]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
8	1	-69	-4	-5	1	-100	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
8	1	19276	4436	6653	376	280	220	>100	3.7	>100	3.7

Asta : 709 [70905 , 70011]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-69	-5	518	3	99	1	--	--	2

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4390	6585	376	280	220	13	3.7	72	3.7

Asta : 710 [70863 , 70893]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	20	13	-415	-7	83	4	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4303	6455	376	280	220	16	4.3	30	4.3

Asta : 710 [70909 , 70012]

Sez. G: Tubo40x60x4 L=14.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
14	1	168	-101	188	1	51	-10	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
14	1	19276	4426	6640	376	280	220	35	5.6	>100	5.6

Asta : 710 [70893 , 70907]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	26	-6	-7	-2	-63	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4409	6614	376	280	220	>100	5.7	>100	5.7

Asta : 711 [70859 , 70888]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-42	-8	-458	-0	-112	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4443	6665	376	280	220	15	3.3	>100	3.3

Asta : 711 [70888 , 70902]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-43	2	-5	0	-112	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4450	6675	376	280	220	>100	3.3	>100	3.3

Asta : 711 [70902 , 70008]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-43	-0	553	-0	107	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4448	6671	376	280	220	12	3.5	>100	3.5

Asta : 712 [70858 , 70887]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-51	8	-453	-0	-112	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4444	6666	376	280	220	15	3.3	>100	3.3

Asta : 712 [70887 , 70901]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-50	-1	-4	-0	-112	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4448	6672	376	280	220	>100	3.3	>100	3.3

Asta : 712 [70901 , 70007]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-49	1	553	0	107	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4448	6672	376	280	220	12	3.5	>100	3.5

Asta : 713 [70857 , 70886]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-50	-10	-471	3	-109	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4396	6593	376	280	220	14	3.4	79	3.4

Asta : 713 [70886 , 70900]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
8	1	-50	3	-2	1	-110	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
8	1	19276	4441	6662	376	280	220	>100	3.4	>100	3.4

Asta : 713 [70900 , 70006]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-51	0	548	1	106	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4441	6662	376	280	220	12	3.5	>100	3.5

Asta : 714 [70856 , 70885]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-56	14	-465	-1	-116	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4437	6656	376	280	220	14	3.2	>100	3.2

Asta : 714 [70885 , 70899]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-58	2	0	-0	-114	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4450	6675	376	280	220	>100	3.3	>100	3.3

Asta : 714 [70899 , 70005]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-59	3	570	-0	111	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4447	6670	376	280	220	12	3.3	>100	3.3

Asta : 715 [70855 , 70884]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-56	10	-332	5	-80	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4358	6537	376	280	220	20	4.5	48	4.5

Asta : 715 [70884 , 70898]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
4	1	-58	6	-7	-1	-78	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
4	1	19276	4435	6652	376	280	220	>100	4.7	>100	4.7

Asta : 715 [70898 , 70904]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-63	7	408	-8	78	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4284	6426	376	280	220	16	4.6	27	4.6

Asta : 718 [70879 , 70861]

Sez. G: Tubo40x60x4 L=93.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
93	1	134	3	308	10	78	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
93	1	19276	4251	6377	376	280	220	21	4.6	22	4.6

Asta : 718 [70868 , 70856]

Sez. G: Tubo40x60x4 L=74.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
74	1	151	-87	204	11	51	37	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
74	1	19276	4229	6344	376	280	220	31	3.7	20	3.7

Asta : 718 [70862 , 70879]

Sez. G: Tubo40x60x4 L=27.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	146	-17	-400	-33	62	-4	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	3790	5685	376	280	220	14	5.4	6.7	5.4

Asta : 718 [70861 , 70877]

Sez. G: Tubo40x60x4 L=31.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	146	211	-308	-27	49	39	--	--	(12+13)-VI-3

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	3913	5870	376	280	220	19	3.6	8.3	3.6

Asta : 718 [70860 , 70874]

Sez. G: Tubo40x60x4 L=101.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	127	-0	-308	-6	67	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4338	6508	376	280	220	21	5.4	39	5.4

Asta : 718 [70859 , 70872]

Sez. G: Tubo40x60x4 L=97.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-47	-1	-304	-7	62	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4316	6473	376	280	220	21	5.9	33	5.9

Asta : 718 [70858 , 70870]

Sez. G: Tubo40x60x4 L=93.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	135	1	-296	-9	60	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4276	6415	376	280	220	22	5.9	25	5.9

Asta : 718 [70857 , 70868]

Sez. G: Tubo40x60x4 L=46.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-46	-4	-417	-28	89	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	3880	5819	376	280	220	14	4.1	7.8	4.1

Asta : 718 [70856 , 70866]

Sez. G: Tubo40x60x4 L=50.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-159	-164	-210	-8	51	-46	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4289	6433	376	280	220	26	3.3	27	3.3

Asta : 718 [70876 , 70860]

Sez. G: Tubo40x60x4 L=15.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-47	18	398	46	73	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	19276	3521	5282	376	280	220	13	4.9	4.8	4.8

Asta : 718 [70874 , 70859]

Sez. G: Tubo40x60x4 L=19.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
19	1	187	-227	159	18	30	25	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
19	1	19276	4080	6119	376	280	220	18	5.6	12	5.6

Asta : 718 [70872 , 70858]

Sez. G: Tubo40x60x4 L=23.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
23	1	-141	232	158	15	29	-31	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
23	1	19276	4141	6212	376	280	220	18	5.1	14	5.1

Asta : 718 [70870 , 70857]

Sez. G: Tubo40x60x4 L=27.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
27	1	169	-210	189	10	41	30	--	--	(12+13)-VIII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
27	1	19276	4242	6362	376	280	220	20	4.5	21	4.5

Asta : 720 [70844 , 70863]

Sez. G: Tubo40x60x4 L=34.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
35	1	-81	-286	158	1	49	45	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
35	1	19276	4440	6660	376	280	220	16	3.4	>100	3.4

Asta : 721 [70847 , 70854]

Sez. G: Tubo40x60x4 L=31.9 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
32	1	-321	330	163	-4	38	-50	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
32	1	19276	4362	6543	376	280	220	13	3.4	50	3.4

Asta : 723 [70809 , 70840]

Sez. G: Tubo40x60x4 L=60.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
60	1	-3	-3	-262	-7	-97	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	19276	4315	6473	376	280	220	25	3.9	33	3.9

Asta : 723 [70840 , 70868]

Sez. G: Tubo40x60x4 L=60.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-8	0	210	3	-91	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4392	6587	376	280	220	31	4.1	74	4.1

Asta : 724 [70802 , 70838]

Sez. G: Tubo40x60x4 L=61.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
61	1	-1	1	-265	5	-103	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
61	1	19276	4348	6522	376	280	220	25	3.7	43	3.7

Asta : 724 [70838 , 70877]

Sez. G: Tubo40x60x4 L=61.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6	-1	240	-12	-95	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4203	6304	376	280	220	26	3.9	18	3.9

Asta : 725 [70894 , 70896]

Sez. G: Tubo40x60x4 L=42.4 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	13	-185	-40	-3	-10	46	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4393	6590	376	280	220	24	5.3	77	5.3

Asta : 728 [70895 , 70897]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-117	-199	-27	3	-13	46	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4392	6588	376	280	220	22	4.9	74	4.9

Asta : 902 [90710 , 90743]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-36	0	-259	-0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4447	6670	376	280	220	26	4.8	>100	4.8

Asta : 902 [90743 , 90776]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-36	-1	238	0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4449	6673	376	280	220	28	4.8	>100	4.8

Asta : 903 [90707 , 90742]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-40	-1	-258	0	-78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4450	6674	376	280	220	26	4.8	>100	4.8

Asta : 903 [90742 , 90773]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-41	1	238	-0	-78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4449	6673	376	280	220	28	4.8	>100	4.8

Asta : 908 [90765 , 90801]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-21	2	-270	0	-80	-0	--	--	2

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

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PROGETTO ESECUTIVO

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4450	6676	376	280	220	25	4.7	>100	4.7

Asta : 908 [90801 , 90821]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-23	-1	226	-0	-80	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4448	6672	376	280	220	30	4.7	>100	4.7

Asta : 909 [90746 , 90768]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	29	-1	-259	0	-76	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4447	6671	376	280	220	26	4.9	>100	4.9

Asta : 909 [90768 , 90802]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	31	-0	240	-0	-76	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6670	376	280	220	28	4.9	>100	4.9

Asta : 911 [90754 , 90789]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	29	1	-259	-0	-76	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4445	6668	376	280	220	26	4.9	>100	4.9

Asta : 911 [90789 , 90809]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	31	0	242	0	-76	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4447	6671	376	280	220	28	4.9	>100	4.9

Asta : 913 [90786 , 90808]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-4	-2	-268	-0	-79	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4449	6673	376	280	220	25	4.7	>100	4.7

Asta : 913 [90808 , 90825]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-4	0	229	0	-79	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4450	6675	376	280	220	29	4.8	>100	4.8

Asta : 1002 [100641 , 100679]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	161	-5	-259	0	-79	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4446	6669	376	280	220	26	4.5	>100	4.5

Asta : 1002 [100679 , 100710]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	161	6	244	-0	-79	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4445	6667	376	280	220	27	4.5	>100	4.5

Asta : 1003 [100638 , 100678]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	161	4	-259	-0	-79	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4446	6669	376	280	220	26	4.5	>100	4.5

Asta : 1003 [100678 , 100707]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	161	-5	244	1	-79	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4440	6661	376	280	220	27	4.5	>100	4.5

Asta : 1007 [100763 , 100798]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	121	-3	183	3	-62	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4384	6576	376	280	220	36	5.8	66	5.8

Asta : 1008 [100718 , 100745]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	170	-5	-261	0	-79	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4445	6667	376	280	220	26	4.5	>100	4.5

Asta : 1008 [100745 , 100765]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	170	6	242	-0	-79	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4443	6664	376	280	220	28	4.5	>100	4.5

Asta : 1009 [100687 , 100721]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
45	1	194	4	-265	-0	-80	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4447	6671	376	280	220	25	4.5	>100	4.5

Asta : 1009 [100721 , 100746]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	195	-7	237	0	-80	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4442	6662	376	280	220	28	4.4	>100	4.4

Asta : 1011 [100695 , 100729]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	193	-4	-266	0	-80	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4447	6671	376	280	220	25	4.5	>100	4.5

Asta : 1011 [100729 , 100754]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	194	8	238	-0	-80	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	28	4.4	>100	4.4

Asta : 1013 [100726 , 100753]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	181	3	-263	-0	-79	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4445	6667	376	280	220	25	4.5	>100	4.5

Asta : 1013 [100753 , 100786]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	181	-5	241	1	-79	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4440	6660	376	280	220	28	4.5	>100	4.5

Asta : 1016 [100794 , 100816]

Sez. G: Tubo40x60x4 L=45.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	26	-3	183	-4	-63	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4369	6554	376	280	220	36	5.9	54	5.9

Asta : 1018 [100795 , 100817]

Sez. G: Tubo40x60x4 L=45.3 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	109	3	184	4	-61	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4367	6551	376	280	220	36	5.9	53	5.9

Asta : 1101 [110563 , 110596]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-67	-0	-199	-3	-64	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4400	6600	376	280	220	33	5.8	87	5.8

Asta : 1101 [110596 , 110644]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-68	1	216	2	-70	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4408	6612	376	280	220	31	5.3	>100	5.3

Asta : 1103 [110560 , 110595]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-55	1	-257	0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4444	6666	376	280	220	26	4.7	>100	4.7

Asta : 1103 [110595 , 110641]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-55	-0	243	-0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6670	376	280	220	27	4.7	>100	4.7

Asta : 1104 [110557 , 110594]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-56	-1	-257	-0	-78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4444	6666	376	280	220	26	4.7	>100	4.7

Asta : 1104 [110594 , 110638]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-56	0	243	0	-78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4447	6670	376	280	220	27	4.8	>100	4.8

Asta : 1105 [110554 , 110593]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-64	0	-200	2	-64	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4402	6603	376	280	220	33	5.8	89	5.8

Asta : 1105 [110593 , 110635]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-65	-1	219	-2	-70	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4408	6612	376	280	220	30	5.2	>100	5.2

Asta : 1115 [110683 , 110716]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-63	1	-211	-2	-66	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4411	6616	376	280	220	31	5.5	>100	5.5

Asta : 1115 [110716 , 110738]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-64	2	224	1	-73	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4425	6637	376	280	220	30	5.1	>100	5.1

Asta : 1117 [110649 , 110686]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-48	2	-257	0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4444	6666	376	280	220	26	4.7	>100	4.7

Asta : 1117 [110686 , 110718]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-48	1	241	-0	-78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	28	4.8	>100	4.8

Asta : 1118 [110608 , 110652]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-39	0	-260	-0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4445	6667	376	280	220	26	4.8	>100	4.8

Asta : 1118 [110652 , 110687]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-38	1	241	0	-78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4447	6671	376	280	220	28	4.8	>100	4.8

Asta : 1119 [110576 , 110611]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-65	1	-198	3	-63	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4400	6600	376	280	220	33	5.8	86	5.8

Asta : 1119 [110611 , 110653]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-66	-1	217	-2	-70	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4406	6609	376	280	220	30	5.3	98	5.3

Asta : 1127 [110617 , 110661]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-38	0	-260	0	-78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4445	6668	376	280	220	26	4.8	>100	4.8

Asta : 1127 [110661 , 110695]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-37	-1	241	-0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4447	6671	376	280	220	28	4.8	>100	4.8

Asta : 1128 [110585 , 110620]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-67	-1	-200	-3	-64	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4401	6601	376	280	220	33	5.8	87	5.8

Asta : 1128 [110620 , 110662]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-69	1	218	2	-70	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4409	6613	376	280	220	30	5.3	>100	5.3

Asta : 1130 [110658 , 110694]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-44	-2	-259	-0	-78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4444	6666	376	280	220	26	4.7	>100	4.7

Asta : 1130 [110694 , 110726]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-43	-1	241	0	-78	-0	--	--	2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	28	4.8	>100	4.8

Asta : 1134 [110691 , 110725]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-67	-1	-209	2	-65	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4409	6613	376	280	220	32	5.6	>100	5.6

Asta : 1134 [110725 , 110750]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-68	-2	222	-2	-72	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4421	6632	376	280	220	30	5.1	>100	5.1

Asta : 1153 [110734 , 110758]

Sez. G: Tubo40x60x4 L=45.3 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-98	0	-209	2	-65	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4406	6609	376	280	220	32	5.6	98	5.6

Asta : 1153 [110758 , 110762]

Sez. G: Tubo40x60x4 L=45.3 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-101	-3	230	-2	-73	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4413	6619	376	280	220	29	5.0	>100	5.0

Asta : 1155 [110735 , 110759]

Sez. G: Tubo40x60x4 L=45.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
46	1	-81	-2	-205	-3	-66	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
46	1	19276	4401	6602	376	280	220	32	5.5	88	5.5

Asta : 1155 [110759 , 110764]

Sez. G: Tubo40x60x4 L=45.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-83	0	228	2	-73	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4404	6606	376	280	220	29	5.0	94	5.0

Asta : 1301 [130457 , 130516]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	97	-7	-244	1	-71	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4421	6632	376	280	220	27	5.1	>100	5.1

Asta : 1301 [130516 , 130563]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	95	-4	246	0	-80	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4450	6675	376	280	220	27	4.6	>100	4.6

Asta : 1302 [130453 , 130515]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	142	-4	-251	-0	-77	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4446	6669	376	280	220	27	4.7	>100	4.7

Asta : 1302 [130515 , 130566]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	141	6	240	0	-77	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4451	6677	376	280	220	28	4.6	>100	4.6

Asta : 1303 [130449 , 130514]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	141	3	-251	0	-77	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4446	6669	376	280	220	27	4.7	>100	4.7

Asta : 1303 [130514 , 130557]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	141	-5	240	-0	-77	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4452	6677	376	280	220	28	4.7	>100	4.7

Asta : 1304 [130445 , 130513]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	103	8	-242	-2	-71	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4413	6619	376	280	220	27	5.1	>100	5.1

Asta : 1304 [130513 , 130554]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	101	4	248	-0	-80	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4450	6675	376	280	220	27	4.6	>100	4.6

Asta : 1307 [130603 , 130648]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	120	-1	-268	3	-74	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4391	6587	376	280	220	25	4.9	74	4.9

Asta : 1307 [130648 , 130683]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	119	-4	254	-1	-83	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4422	6633	376	280	220	26	4.4	>100	4.4

Asta : 1308 [130570 , 130607]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	146	-5	-249	-1	-76	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4440	6661	376	280	220	27	4.7	>100	4.7

Asta : 1308 [130607 , 130649]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	146	6	235	0	-76	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4447	6670	376	280	220	28	4.7	>100	4.7

Asta : 1309 [130527 , 130574]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	152	2	-253	0	-77	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4445	6668	376	280	220	26	4.7	>100	4.7

Asta : 1309 [130574 , 130608]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	152	-6	238	-0	-77	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4450	6675	376	280	220	28	4.6	>100	4.6

Asta : 1310 [130490 , 130531]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	99	5	-244	-2	-71	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4420	6630	376	280	220	27	5.2	>100	5.2

Asta : 1310 [130531 , 130576]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	97	4	245	-0	-80	0	--	--	2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4449	6673	376	280	220	27	4.6	>100	4.6

Asta : 1313 [130540 , 130584]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	153	-2	-253	-0	-77	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4444	6666	376	280	220	26	4.7	>100	4.7

Asta : 1313 [130584 , 130617]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	153	6	239	0	-77	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4449	6674	376	280	220	28	4.6	>100	4.6

Asta : 1314 [130499 , 130544]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	97	-5	-248	2	-70	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4414	6621	376	280	220	27	5.2	>100	5.2

Asta : 1314 [130544 , 130585]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	95	-3	244	0	-79	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4451	6676	376	280	220	27	4.6	>100	4.6

Asta : 1315 [130580 , 130616]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	150	4	-251	0	-77	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4444	6666	376	280	220	27	4.7	>100	4.7

Asta : 1315 [130616 , 130658]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	149	-6	238	-0	-77	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4450	6675	376	280	220	28	4.7	>100	4.7

Asta : 1316 [130612 , 130657]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	111	7	-256	-2	-75	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4401	6602	376	280	220	26	4.8	89	4.8

Asta : 1316 [130657 , 130691]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	109	4	257	1	-84	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4431	6646	376	280	220	26	4.4	>100	4.4

Asta : 1321 [130676 , 130701]Sez. G: Tubo40x60x4 L=45.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
46	1	-2	7	-260	-3	-77	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
46	1	19276	4385	6578	376	280	220	25	4.9	67	4.9

Asta : 1321 [130701 , 130734]Sez. G: Tubo40x60x4 L=45.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-8	-5	261	1	-89	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4441	6662	376	280	220	26	4.1	>100	4.1

Asta : 1324 [130682 , 130702]Sez. G: Tubo40x60x4 L=44.9 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	102	-14	-252	2	-74	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4410	6615	376	280	220	26	4.8	>100	4.8

Asta : 1324 [130702 , 130735]Sez. G: Tubo40x60x4 L=44.9 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	99	3	263	-0	-85	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4442	6663	376	280	220	25	4.2	>100	4.2

Asta : 1402 [140357 , 140407]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-66	0	-254	-0	-77	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4446	6669	376	280	220	26	4.8	>100	4.8

Asta : 1402 [140407 , 140453]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-66	-1	241	0	-77	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	28	4.8	>100	4.8

Asta : 1403 [140354 , 140406]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-67	-0	-255	0	-77	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4448	6672	376	280	220	26	4.8	>100	4.8

Asta : 1403 [140406 , 140449]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-67	0	242	-0	-77	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4449	6673	376	280	220	28	4.8	>100	4.8

Asta : 1408 [140481 , 140526]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-59	1	-257	-0	-77	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4449	6674	376	280	220	26	4.8	>100	4.8

Asta : 1408 [140526 , 140570]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-59	1	241	0	-77	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4447	6670	376	280	220	28	4.8	>100	4.8

Asta : 1409 [140424 , 140485]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-57	0	-254	0	-77	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4445	6667	376	280	220	26	4.8	>100	4.8

Asta : 1409 [140485 , 140527]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-57	1	239	-0	-77	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	28	4.8	>100	4.8

Asta : 1413 [140437 , 140498]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-57	0	-254	-0	-76	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4443	6664	376	280	220	26	4.8	>100	4.8

Asta : 1413 [140498 , 140540]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-57	-2	240	0	-77	-0	--	--	2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4445	6667	376	280	220	28	4.8	>100	4.8

Asta : 1415 [140495 , 140539]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-57	-1	-257	0	-77	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4449	6674	376	280	220	26	4.8	>100	4.8

Asta : 1415 [140539 , 140580]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-57	-2	242	-0	-77	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4448	6671	376	280	220	28	4.8	>100	4.8

Asta : 1425 [140600 , 140634]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
40	1	-40	2	-298	-1	-75	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
40	1	19276	4433	6650	376	280	220	22	4.9	>100	4.9

Asta : 1425 [140634 , 140666]

Sez. G: Tubo40x60x4 L=40.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-42	1	198	-3	-76	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4388	6582	376	280	220	33	4.9	70	4.9

Asta : 1602 [160270 , 160320]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	137	-4	-256	-0	-78	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4451	6677	376	280	220	26	4.6	>100	4.6

Asta : 1602 [160320 , 160357]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	137	6	243	-0	-78	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4448	6672	376	280	220	27	4.6	>100	4.6

Asta : 1603 [160266 , 160319]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	137	4	-257	-0	-78	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4450	6676	376	280	220	26	4.6	>100	4.6

Asta : 1603 [160319 , 160354]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	137	-5	244	0	-78	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	27	4.6	>100	4.6

Asta : 1608 [160384 , 160422]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	152	-4	-260	0	-78	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4450	6675	376	280	220	26	4.6	>100	4.6

Asta : 1608 [160422 , 160481]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	152	5	242	-0	-78	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	28	4.6	>100	4.6

Asta : 1609 [160333 , 160388]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	149	4	-258	0	-78	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4451	6677	376	280	220	26	4.6	>100	4.6

Asta : 1609 [160388 , 160424]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	150	-6	241	0	-78	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4449	6673	376	280	220	28	4.6	>100	4.6

Asta : 1611 [160346 , 160400]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	149	-3	-258	-0	-78	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4450	6675	376	280	220	26	4.6	>100	4.6

Asta : 1611 [160400 , 160437]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	149	6	242	-0	-78	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4449	6674	376	280	220	28	4.6	>100	4.6

Asta : 1613 [160396 , 160436]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	155	5	-260	-0	-78	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4449	6674	376	280	220	26	4.6	>100	4.6

Asta : 1613 [160436 , 160495]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	155	-5	243	0	-78	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	27	4.6	>100	4.6

Asta : 1621 [160532 , 160569]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	166	-3	-259	-1	-85	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4428	6643	376	280	220	26	4.2	>100	4.2

Asta : 1621 [160569 , 160600]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	163	9	268	1	-86	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4435	6653	376	280	220	25	4.1	>100	4.1

Asta : 1702 [170198 , 170239]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-64	1	-257	0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4445	6668	376	280	220	26	4.7	>100	4.7

Asta : 1702 [170239 , 170270]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-64	-0	245	-0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4448	6672	376	280	220	27	4.7	>100	4.7

Asta : 1703 [170195 , 170238]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-64	-0	-257	-0	-79	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4445	6667	376	280	220	26	4.7	>100	4.7

Asta : 1703 [170238 , 170266]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-64	0	245	0	-79	0	--	--	2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4447	6670	376	280	220	27	4.7	>100	4.7

Asta : 1708 [170299 , 170332]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-39	2	-262	0	-79	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4443	6664	376	280	220	25	4.7	>100	4.7

Asta : 1708 [170332 , 170384]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-39	0	241	-0	-79	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	28	4.7	>100	4.7

Asta : 1709 [170251 , 170302]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-46	0	-260	-0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4446	6669	376	280	220	26	4.7	>100	4.7

Asta : 1709 [170302 , 170333]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-46	1	241	0	-78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4448	6672	376	280	220	28	4.7	>100	4.7

Asta : 1711 [170258 , 170311]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-48	0	-260	0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4447	6670	376	280	220	26	4.7	>100	4.7

Asta : 1711 [170311 , 170346]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-47	-1	242	-0	-78	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4449	6673	376	280	220	28	4.7	>100	4.7

Asta : 1713 [170308 , 170344]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-36	-2	-262	-1	-79	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4441	6662	376	280	220	25	4.7	>100	4.7

Asta : 1713 [170344 , 170396]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-36	-1	243	0	-79	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4444	6667	376	280	220	27	4.7	>100	4.7

Asta : 1719 [170484 , 170518]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	23	-7	180	3	-61	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4386	6579	376	280	220	37	5.9	68	5.9

Asta : 1720 [170413 , 170461]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	19	4	182	-4	-62	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4374	6561	376	280	220	36	5.9	57	5.9

Asta : 1724 [170480 , 170517]

Sez. G: Tubo40x60x4 L=45.3 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	240	65	-171	1	42	15	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4424	6636	376	280	220	39	5.6	>100	5.6

Asta : 1724 [170517 , 170553]

Sez. G: Tubo40x60x4 L=45.3 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-415	-81	158	-1	41	19	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4426	6639	376	280	220	42	5.0	>100	5.0

Asta : 1802 [180145 , 180169]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	105	-1	-273	3	61	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4383	6574	376	280	220	24	5.9	64	5.9

Asta : 1803 [180146 , 180170]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	142	1	-351	-0	77	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4447	6671	376	280	220	19	4.7	>100	4.7

Asta : 1803 [180170 , 180195]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	142	-4	209	1	-68	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4441	6662	376	280	220	32	5.2	>100	5.2

Asta : 1804 [180147 , 180171]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	142	-1	-351	0	77	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4447	6670	376	280	220	19	4.7	>100	4.7

Asta : 1804 [180171 , 180198]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	143	4	209	-1	-68	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4441	6662	376	280	220	32	5.2	>100	5.2

Asta : 1805 [180414 , 180355]

Sez. G: Tubo40x60x4 L=48.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
48	1	-298	-81	-112	-6	-28	25	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
48	1	19276	4335	6502	376	280	220	53	5.6	38	5.6

Asta : 1807 [180186 , 180220]

Sez. G: Tubo40x60x4 L=51.9 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
52	1	-58	-6	-244	-0	-99	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
52	1	19276	4446	6669	376	280	220	27	3.7	>100	3.7

Asta : 1807 [180220 , 180248]

Sez. G: Tubo40x60x4 L=51.9 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-62	-4	345	6	-100	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4339	6508	376	280	220	19	3.7	40	3.7

Asta : 1809 [180189 , 180227]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	193	0	-280	0	-72	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4447	6670	376	280	220	24	4.9	>100	4.9

Asta : 1809 [180227 , 180251]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	194	-6	221	1	-72	-1	--	--	2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4439	6658	376	280	220	30	4.9	>100	4.9

Asta : 1810 [180224 , 180250]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	212	-1	-346	-2	72	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4408	6611	376	280	220	19	4.9	>100	4.9

Asta : 1810 [180250 , 180299]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	212	2	214	-1	-70	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4440	6660	376	280	220	31	5.0	>100	5.0

Asta : 1810 [180158 , 180179]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	85	-155	-118	19	33	-41	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4067	6100	376	280	220	26	4.2	12	4.2

Asta : 1810 [180141 , 180158]

Sez. G: Tubo40x60x4 L=26.8 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
27	1	91	-230	67	6	15	49	--	--	(12+13)-I-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
27	1	19276	4322	6484	376	280	220	19	4.6	34	4.6

Asta : 1812 [180232 , 180257]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	218	2	-354	2	79	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4407	6611	376	280	220	19	4.5	>100	4.5

Asta : 1812 [180257 , 180308]

Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	218	-3	206	0	-68	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6669	376	280	220	32	5.2	>100	5.2

Asta : 1812 [180210 , 180232]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	277	-7	274	16	76	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4124	6186	376	280	220	23	4.4	14	4.4

Asta : 1812 [180164 , 180184]Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	67	160	-145	-19	37	37	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4065	6098	376	280	220	25	4.3	12	4.3

Asta : 1813 [180182 , 180209]Sez. G: Tubo40x60x4 L=43.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-29	5	-361	4	-93	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	19276	4369	6554	376	280	220	18	4.0	54	4.0

Asta : 1813 [180256 , 180307]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	205	5	-308	3	97	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4387	6580	376	280	220	21	3.6	69	3.6

Asta : 1813 [180209 , 180241]Sez. G: Tubo40x60x4 L=43.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-35	-6	27	-3	-93	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4390	6585	376	280	220	>100	3.9	72	3.9

Asta : 1813 [180241 , 180256]Sez. G: Tubo40x60x4 L=43.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-33	4	569	0	139	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	19276	4448	6672	376	280	220	12	2.7	>100	2.7

Asta : 1814 [180204 , 180233]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	188	-1	-280	-0	-72	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	19276	4449	6673	376	280	220	24	4.9	>100	4.9

Asta : 1814 [180233 , 180258]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	189	6	222	-1	-72	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4438	6656	376	280	220	30	4.9	>100	4.9

Asta : 1818 [180162 , 180183]Sez. G: Tubo40x60x4 L=45.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	114	1	-286	-4	63	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4375	6562	376	280	220	23	5.8	58	5.8

Asta : 1819 [180382 , 180325]

Sez. G: Tubo40x60x4 L=115.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	83	0	-310	-0	67	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4448	6672	376	280	220	22	5.4	>100	5.4

Asta : 1819 [180444 , 180382]

Sez. G: Tubo40x60x4 L=81.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
81	1	-17	-6	273	5	78	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
81	1	19276	4346	6519	376	280	220	24	4.6	42	4.6

Asta : 1820 [180243 , 180255]

Sez. G: Tubo40x60x4 L=36.4 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
36	1	-52	-8	-286	5	-79	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
36	1	19276	4358	6538	376	280	220	23	4.6	48	4.6

Asta : 1820 [180255 , 180289]

Sez. G: Tubo40x60x4 L=36.4 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-48	-6	125	-0	-80	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4451	6677	376	280	220	53	4.6	>100	4.6

Asta : 1820 [180289 , 180325]

Sez. G: Tubo40x60x4 L=36.4 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
36	1	-46	7	286	-0	64	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
36	1	19276	4449	6674	376	280	220	23	5.6	>100	5.6

Asta : 1821 [180316 , 180345]

Sez. G: Tubo40x60x4 L=42.1 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-36	-0	-199	2	-75	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4417	6626	376	280	220	33	4.9	>100	4.9

Asta : 1821 [180345 , 180382]

Sez. G: Tubo40x60x4 L=42.1 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-33	2	313	3	-81	1	--	--	2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4382	6573	376	280	220	21	4.5	64	4.5

Asta : 1822 [180322 , 180342]

Sez. G: Tubo40x60x4 L=56.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-97	-19	-333	6	70	-6	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4324	6486	376	280	220	19	4.7	35	4.7

Asta : 1823 [180322 , 180343]

Sez. G: Tubo40x60x4 L=34.8 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	123	8	-309	0	70	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4446	6668	376	280	220	22	5.0	>100	5.0

Asta : 1823 [180246 , 180278]

Sez. G: Tubo40x60x4 L=18.9 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
19	1	-87	13	-18	-20	-59	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
19	1	19276	4050	6076	376	280	220	>100	5.8	11	5.8

Asta : 1823 [180288 , 180322]

Sez. G: Tubo40x60x4 L=37.8 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
38	1	-107	-1	321	-13	78	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
38	1	19276	4186	6278	376	280	220	20	4.7	17	4.7

Asta : 1823 [180278 , 180288]

Sez. G: Tubo40x60x4 L=18.9 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-105	6	149	2	-73	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4418	6627	376	280	220	45	4.8	>100	4.8

Asta : 1824 [180509 , 180525]

Sez. G: Tubo40x60x4 L=41.3 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	6	-96	24	-1	-42	-19	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4440	6661	376	280	220	46	5.6	>100	5.6

Asta : 1825 [180376 , 180411]

Sez. G: Tubo40x60x4 L=41.3 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
41	1	-82	-5	-312	7	-90	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
41	1	19276	4319	6479	376	280	220	21	4.1	34	4.1

Asta : 1825 [180411 , 180444]

Sez. G: Tubo40x60x4 L=41.3 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-172	-94	28	1	-48	-25	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4431	6646	376	280	220	47	4.4	>100	4.4

Asta : 1825 [180444 , 180480]

Sez. G: Tubo40x60x4 L=41.3 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
41	1	-279	-78	225	-5	51	19	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
41	1	19276	4354	6531	376	280	220	29	4.6	46	4.6

Asta : 1827 [180174 , 180182]

Sez. G: Tubo40x60x4 L=11.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
11	1	-11	17	-340	60	-18	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
11	1	19276	3236	4853	376	280	220	14	18	3.7	3.7

Asta : 1834 [180411 , 180345]

Sez. G: Tubo40x60x4 L=89.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
89	1	-6	-3	226	-7	62	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	19276	4312	6469	376	280	220	29	5.9	32	5.9

Asta : 1834 [180345 , 180255]

Sez. G: Tubo40x60x4 L=120.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-7	1	-286	3	63	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4401	6601	376	280	220	23	5.9	87	5.9

Asta : 1835 [180144 , 180185]

Sez. G: Tubo40x60x4 L=101.9 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
102	1	-282	-47	76	0	22	30	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	19276	4448	6672	376	280	220	88	5.6	>100	5.6

Asta : 1836 [180185 , 180174]

Sez. G: Tubo40x60x4 L=27.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
28	1	-58	246	-127	4	-30	-34	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
28	1	19276	4366	6548	376	280	220	18	4.9	52	4.9

Asta : 1901 [190101 , 190120]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-103	-2	-394	-3	-113	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4389	6583	376	280	220	17	3.3	71	3.3

Asta : 1901 [190120 , 190133]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-102	-3	3	2	-117	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4420	6630	376	280	220	>100	3.1	>100	3.1

Asta : 1901 [190133 , 190150]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-107	-6	442	4	-110	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4370	6556	376	280	220	15	3.3	55	3.3

Asta : 1902 [190097 , 190117]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-106	-1	-410	3	-117	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4398	6597	376	280	220	16	3.1	83	3.1

Asta : 1902 [190117 , 190130]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-106	0	5	-2	-122	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4417	6625	376	280	220	>100	3.0	>100	3.0

Asta : 1902 [190130 , 190145]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-111	3	464	-3	-115	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4383	6575	376	280	220	14	3.2	65	3.2

Asta : 1903 [190098 , 190118]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-120	-0	-468	0	-134	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4442	6663	376	280	220	14	2.8	>100	2.8

Asta : 1903 [190118 , 190131]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
4	1	-121	0	0	0	-133	0	--	--	2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
4	1	19276	4444	6667	376	280	220	>100	2.8	>100	2.8

Asta : 1903 [190131 , 190146]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-122	1	505	-1	-125	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4441	6661	376	280	220	13	2.9	>100	2.9

Asta : 1904 [190099 , 190119]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-120	-2	-468	-1	-134	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4440	6660	376	280	220	14	2.7	>100	2.7

Asta : 1904 [190119 , 190132]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-121	-3	-5	-0	-133	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4445	6667	376	280	220	>100	2.8	>100	2.8

Asta : 1904 [190132 , 190147]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-123	-3	505	1	-125	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4440	6659	376	280	220	13	2.9	>100	2.9

Asta : 1907 [190137 , 190157]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	12	-7	-719	0	235	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4443	6665	376	280	220	9.3	1.6	>100	1.6

Asta : 1907 [190110 , 190126]

Sez. G: Tubo40x60x4 L=37.1 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
37	1	-15	4	287	-8	76	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
37	1	19276	4291	6437	376	280	220	22	4.9	28	4.9

Asta : 1907 [190157 , 190175]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	9	-5	-107	-1	-104	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4433	6650	376	280	220	62	3.6	>100	3.6

Asta : 1907 [190175 , 190189]Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	5	-17	381	-1	-106	-3	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4431	6646	376	280	220	17	3.4	>100	3.4

Asta : 1907 [190126 , 190137]Sez. G: Tubo40x60x4 L=37.1 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
37	1	-16	-1	552	13	262	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
37	1	19276	4194	6290	376	280	220	11	1.4	17	1.4

Asta : 1908 [190158 , 190179]Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-149	-2	-272	-3	84	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4385	6577	376	280	220	24	4.3	66	4.3

Asta : 1908 [190141 , 190158]Sez. G: Tubo40x60x4 L=26.8 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
27	1	12	-18	163	28	79	3	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
27	1	19276	3886	5830	376	280	220	36	4.5	7.9	4.5

Asta : 1909 [190123 , 190135]Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	22	-2	-585	-1	192	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4436	6654	376	280	220	11	2.0	>100	2.0

Asta : 1909 [190105 , 190111]Sez. G: Tubo40x60x4 L=29.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
29	1	-3	-1	270	-2	68	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
29	1	19276	4413	6619	376	280	220	25	5.5	>100	5.5

Asta : 1909 [190135 , 190153]Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	23	-2	-77	0	-90	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4449	6673	376	280	220	86	4.1	>100	4.1

Asta : 1909 [190153 , 190173]Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	21	-13	315	-2	-91	-3	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4418	6626	376	280	220	21	4.0	>100	4.0

Asta : 1909 [190111 , 190123]

Sez. G: Tubo40x60x4 L=29.2 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
29	1	-2	4	507	-20	220	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
29	1	19276	4042	6063	376	280	220	12	1.7	11	1.7

Asta : 1910 [190158 , 190137]

Sez. G: Tubo40x60x4 L=116.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
116	1	-47	4	326	-5	66	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
116	1	19276	4357	6536	376	280	220	20	5.4	47	5.4

Asta : 1911 [190139 , 190164]

Sez. G: Tubo40x60x4 L=116.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-34	-4	-306	5	63	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4358	6537	376	280	220	21	5.7	47	5.7

Asta : 1912 [190094 , 190112]

Sez. G: Tubo40x60x4 L=31.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
31	1	-6	3	258	-1	67	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
31	1	19276	4432	6647	376	280	220	26	5.6	>100	5.6

Asta : 1912 [190124 , 190138]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	21	-0	-579	-0	192	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4449	6673	376	280	220	12	2.0	>100	2.0

Asta : 1912 [190138 , 190161]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	22	-0	-78	0	-89	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4449	6673	376	280	220	85	4.2	>100	4.2

Asta : 1912 [190161 , 190176]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	20	10	311	2	-90	2	--	--	2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4406	6609	376	280	220	21	4.0	97	4.0

Asta : 1912 [190112 , 190124]

Sez. G: Tubo40x60x4 L=31.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
31	1	-4	-7	504	16	222	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
31	1	19276	4127	6191	376	280	220	12	1.7	14	1.7

Asta : 1913 [190164 , 190184]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-274	1	-263	4	76	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4371	6556	376	280	220	25	4.6	55	4.6

Asta : 1914 [190139 , 190163]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2	5	-708	-1	227	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4434	6651	376	280	220	9.4	1.6	>100	1.6

Asta : 1914 [190163 , 190181]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-2	3	-99	1	-105	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4433	6650	376	280	220	67	3.6	>100	3.6

Asta : 1914 [190181 , 190204]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6	15	390	1	-107	3	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4428	6642	376	280	220	17	3.4	>100	3.4

Asta : 1914 [190127 , 190139]

Sez. G: Tubo40x60x4 L=33.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
34	1	-18	2	552	-16	248	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
34	1	19276	4124	6185	376	280	220	11	1.5	14	1.5

Asta : 1914 [190116 , 190127]

Sez. G: Tubo40x60x4 L=33.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
34	1	-16	-8	293	6	74	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
34	1	19276	4329	6493	376	280	220	22	5.0	36	5.0

Asta : 1915 [190113 , 190128]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-42	-3	-492	-7	115	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4307	6461	376	280	220	13	3.2	31	3.2

Asta : 1915 [190104 , 190113]

Sez. G: Tubo40x60x4 L=31.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
32	1	1	2	248	-17	86	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
32	1	19276	4113	6169	376	280	220	25	4.4	13	4.4

Asta : 1915 [190128 , 190142]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-42	-4	-5	1	-94	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4425	6638	376	280	220	>100	3.9	>100	3.9

Asta : 1915 [190142 , 190165]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-46	-12	371	6	-97	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4333	6500	376	280	220	18	3.7	38	3.7

Asta : 1916 [190107 , 190121]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-91	-1	-424	-2	-108	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4420	6630	376	280	220	16	3.4	>100	3.4

Asta : 1916 [190121 , 190134]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
4	1	-92	-3	-2	-0	-111	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
4	1	19276	4451	6677	376	280	220	>100	3.3	>100	3.3

Asta : 1916 [190134 , 190154]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-95	-8	424	-2	-106	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4407	6611	376	280	220	16	3.4	>100	3.4

Asta : 1917 [190115 , 190129]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-33	1	-499	7	124	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4305	6458	376	280	220	13	3.0	30	3.0

Asta : 1917 [190095 , 190115]

Sez. G: Tubo40x60x4 L=35.8 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
36	1	1	-1	277	17	103	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
36	1	19276	4104	6156	376	280	220	22	3.7	13	3.7

Asta : 1917 [190129 , 190143]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-33	2	-17	-1	-92	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4430	6645	376	280	220	>100	4.0	>100	4.0

Asta : 1917 [190143 , 190168]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-36	10	356	-6	-95	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4329	6494	376	280	220	18	3.8	36	3.8

Asta : 1918 [190109 , 190122]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
42	1	-90	-1	-454	4	-111	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	19276	4379	6569	376	280	220	14	3.3	62	3.3

Asta : 1918 [190122 , 190136]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
8	1	-91	1	-0	-1	-113	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
8	1	19276	4439	6659	376	280	220	>100	3.3	>100	3.3

Asta : 1918 [190136 , 190162]

Sez. G: Tubo40x60x4 L=41.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-95	6	436	1	-110	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	19276	4427	6640	376	280	220	15	3.3	>100	3.3

Asta : 11498 [11498 , 30713]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-662	112	16	-1	-4	23	--	--	(12+13)-I-1

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4331	4331	204	204	139	39	5.8	>100	5.8

Asta : 11498 [90713 , 100713]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-200	185	27	0	28	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4344	4344	204	204	139	24	4.7	>100	4.7

Asta : 11499 [11499 , 20779]

Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-349	174	94	-0	-17	33	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4343	4343	204	204	139	25	3.7	>100	3.7

Asta : 11500 [11500 , 20834]

Sez. G: Tubo40x40x4 L=44.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-775	141	24	-1	-7	39	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4312	4312	204	204	139	30	3.6	>100	3.6

Asta : 11501 [90710 , 100710]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-303	42	-301	-0	44	3	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4345	4345	204	204	139	14	4.0	>100	4.0

Asta : 11502 [11502 , 20776]

Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-903	-88	-197	1	39	-17	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4320	4320	204	204	139	22	3.0	>100	3.0

Asta : 11502 [70776 , 90776]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-544	11	36	-0	41	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4347	4347	204	204	139	>100	4.1	>100	4.1

Asta : 11503 [11503 , 20832]

Sez. G: Tubo40x40x4 L=44.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-784	-117	23	1	-8	-32	--	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4322	4322	204	204	139	37	4.1	>100	4.1

Asta : 11504 [11504 , 30707]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-849	112	17	-1	-4	22	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4333	4333	204	204	139	39	5.4	>100	5.4

Asta : 11504 [90707 , 100707]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-300	17	-327	0	47	1	--	--	(12+13)-VIII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	13	3.9	>100	3.9

Asta : 11505 [11505 , 20773]

Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-910	73	-219	-1	43	14	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4324	4324	204	204	139	20	3.0	>100	3.0

Asta : 11505 [70773 , 90773]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-542	-14	41	0	41	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	>100	4.1	>100	4.1

Asta : 11506 [11506 , 20830]

Sez. G: Tubo40x40x4 L=44.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-780	138	27	-1	-8	38	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4323	4323	204	204	139	31	3.6	>100	3.6

Asta : 11507 [11507 , 30704]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-673	-114	16	1	-4	-23	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4323	4323	204	204	139	38	5.7	>100	5.7

Asta : 11507 [90704 , 100704]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-292	-119	35	-0	29	8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	36	5.1	>100	5.1

Asta : 11508 [11508 , 20770]

Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-341	-174	92	1	-17	-33	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4332	4332	204	204	139	25	3.7	>100	3.7

Asta : 11508 [70770 , 90770]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-381	-89	21	0	19	-10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4342	4342	204	204	139	49	5.9	>100	5.9

Asta : 11509 [11509 , 20828]

Sez. G: Tubo40x40x4 L=44.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-782	-119	25	1	-7	-32	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4321	4321	204	204	139	36	4.1	>100	4.1

Asta : 11510 [11510 , 20860]

Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-751	84	-20	0	8	29	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4343	4343	204	204	139	52	4.3	>100	4.3

Asta : 11510 [20860 , 70860]

Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-1122	-7	-35	-0	-29	4	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4343	4343	204	204	139	>100	4.3	>100	4.3

Asta : 11511 [11511 , 20861]

Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-797	-80	-29	-0	13	-28	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	54	3.9	>100	3.9

Asta : 11511 [20861 , 70861]

Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-1275	11	-34	0	-28	-7	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4345	4345	204	204	139	>100	3.9	>100	3.9

Asta : 11512 [11512 , 20862]

Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-537	-81	-31	0	13	-28	--	--	(12+13)-I-4

COMUNE DI ANDRIA
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2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4346	4346	204	204	139	54	4.3	>100	4.3

Asta : 11512 [20862 , 70862]

Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-920	10	-36	-0	-28	-6	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4343	4343	204	204	139	>100	4.4	>100	4.4

Asta : 11513 [11513 , 20863]

Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-288	-79	-14	1	6	-28	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4315	4315	204	204	139	55	5.4	>100	5.4

Asta : 11514 [11514 , 20859]

Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-709	-81	-26	-0	9	-29	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4354	4354	204	204	139	54	4.3	>100	4.3

Asta : 11514 [20859 , 70859]

Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-1051	0	-39	0	-32	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4346	4346	204	204	139	>100	4.4	>100	4.4

Asta : 11515 [11515 , 20858]

Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-701	82	-23	0	9	29	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4348	4348	204	204	139	53	4.3	>100	4.3

Asta : 11515 [20858 , 70858]

Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-1029	-4	-40	-0	-32	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4346	4346	204	204	139	>100	4.2	>100	4.2

Asta : 11516 [11516 , 20857]

Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-798	-82	-24	-1	10	-29	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4338	4338	204	204	139	53	4.1	>100	4.1

Asta : 11516 [20857 , 70857]Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-1214	9	-35	0	-29	-5	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4341	4341	204	204	139	>100	4.0	>100	4.0

Asta : 11517 [11517 , 20856]Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-763	76	-34	-0	15	27	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4353	4353	204	204	139	58	3.9	>100	3.9

Asta : 11517 [20856 , 70856]Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-1203	0	-41	-0	-33	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4351	4351	204	204	139	>100	4.1	>100	4.1

Asta : 11518 [11518 , 20855]Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-370	80	-29	-1	12	28	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4339	4339	204	204	139	54	4.6	>100	4.6

Asta : 11518 [20855 , 70855]Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-538	-16	-30	0	-22	10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4341	4341	204	204	139	>100	5.2	>100	5.2

Asta : 11519 [11519 , 20854]Sez. G: Tubo40x40x4 L=56.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-176	74	-15	-1	7	27	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4319	4319	204	204	139	58	5.7	>100	5.7

Asta : 11520 [11520 , 20782]Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-438	-163	-2	-0	0	-32	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4344	4344	204	204	139	27	5.4	>100	5.4

Asta : 11521 [11521 , 20844]Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-382	182	5	-1	-5	36	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4335	4335	204	204	139	24	4.5	>100	4.5

Asta : 11522 [11522 , 30798]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-768	112	26	-1	-5	23	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4326	4326	204	204	139	39	5.3	>100	5.3

Asta : 11522 [90798 , 100798]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-220	85	-245	1	34	7	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4333	4333	204	204	139	18	4.7	>100	4.7

Asta : 11523 [11523 , 30765]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-925	66	38	-0	-11	13	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4341	4341	204	204	139	66	5.6	>100	5.6

Asta : 11523 [90765 , 100765]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-366	-16	-498	-0	61	-1	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4348	4348	204	204	139	8.7	3.0	>100	3.0

Asta : 11524 [11524 , 20821]

Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-724	-162	2	0	-1	-31	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4343	4343	204	204	139	27	4.8	>100	4.8

Asta : 11524 [70821 , 90821]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-196	34	-370	1	44	4	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4309	4309	204	204	139	12	4.0	94	4.0

Asta : 11525 [11525 , 30746]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1133	64	36	0	-11	13	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4346	4346	204	204	139	68	5.3	>100	5.3

Asta : 11525 [90746 , 100746]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-352	0	-586	0	68	0	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4346	4346	204	204	139	7.4	2.8	>100	2.8

Asta : 11526 [11526 , 20802]

Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-852	161	-15	0	4	32	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4353	4353	204	204	139	27	4.3	>100	4.3

Asta : 11526 [20802 , 70802]

Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-615	15	-43	0	-28	-4	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4341	4341	204	204	139	>100	5.1	>100	5.1

Asta : 11526 [70802 , 90802]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-338	-10	423	0	56	1	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	10	3.3	>100	3.3

Asta : 11527 [90722 , 100722]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-291	-126	45	-0	30	8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4349	4349	204	204	139	34	4.9	>100	4.9

Asta : 11528 [11528 , 20790]

Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-383	170	4	1	-2	33	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4338	4338	204	204	139	26	5.0	>100	5.0

Asta : 11529 [11529 , 30805]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-811	-113	31	1	-7	-23	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4327	4327	204	204	139	38	4.9	>100	4.9

Asta : 11529 [90805 , 100805]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-338	-55	-330	-0	42	-5	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4346	4346	204	204	139	13	4.0	>100	4.0

Asta : 11530 [11530 , 20825]Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-750	171	8	-0	-4	33	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4343	4343	204	204	139	25	4.4	>100	4.4

Asta : 11530 [70825 , 90825]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-201	-29	-342	3	43	-3	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4271	4271	204	204	139	12	4.1	52	4.1

Asta : 11531 [11531 , 30731]Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-708	108	19	-1	-4	22	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4323	4323	204	204	139	40	5.7	>100	5.7

Asta : 11531 [90731 , 100731]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-196	193	35	0	29	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4344	4344	204	204	139	22	4.6	>100	4.6

Asta : 11532 [11532 , 30786]Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-962	86	25	-1	-6	17	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4335	4335	204	204	139	50	5.6	>100	5.6

Asta : 11532 [90786 , 100786]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-363	-1	-474	1	59	0	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4325	4325	204	204	139	9.1	3.2	>100	3.2

Asta : 11533 [11533 , 20847]Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-390	-193	-4	-1	2	-38	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4330	4330	204	204	139	22	4.6	>100	4.6

Asta : 11534 [11534 , 30754]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-599	107	23	-1	-6	21	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4336	4336	204	204	139	41	5.8	>100	5.8

Asta : 11534 [90754 , 100754]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-325	24	-449	1	56	2	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4338	4338	204	204	139	9.7	3.3	>100	3.3

Asta : 11535 [11535 , 20809]

Sez. G: Tubo40x40x4 L=27.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-848	-168	-25	0	8	-33	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4351	4351	204	204	139	26	3.9	>100	3.9

Asta : 11535 [20809 , 70809]

Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-1141	-2	-28	-0	-18	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4354	4354	204	204	139	>100	5.9	>100	5.9

Asta : 11535 [70809 , 90809]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-547	8	-33	-1	51	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4336	4336	204	204	139	>100	3.5	>100	3.5

Asta : 11536 [70895 , 90895]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-68	-131	-241	2	24	-10	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4285	4285	204	204	139	18	5.9	62	5.9

Asta : 11537 [90853 , 100853]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-227	-174	-2	0	18	14	--	--	2

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4353	4353	204	204	139	25	5.7	>100	5.7

Asta : 11538 [70894 , 90894]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-152	11	297	-7	33	-1	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4132	4132	204	204	139	14	5.6	20	5.6

Asta : 11539 [90852 , 100852]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-162	55	283	-1	32	-6	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4329	4329	204	204	139	15	5.2	>100	5.2

Asta : 11541 [90816 , 100816]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-405	-228	-9	-0	29	-19	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	19	3.9	>100	3.9

Asta : 11543 [90817 , 100817]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-343	208	-228	-1	33	17	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4339	4339	204	204	139	19	3.7	>100	3.7

Asta : 21498 [21498 , 30644]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-735	99	-194	-0	21	11	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4345	4345	204	204	139	22	4.9	>100	4.9

Asta : 21498 [100644 , 110644]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-472	116	84	0	38	-8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4350	4350	204	204	139	38	3.9	>100	3.9

Asta : 21499 [21499 , 30641]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-900	-89	-288	1	31	-10	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4337	4337	204	204	139	15	3.9	>100	3.9

Asta : 21499 [100641 , 110641]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-553	-10	54	-0	43	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4347	4347	204	204	139	80	4.0	>100	4.0

Asta : 21500 [21500 , 30638]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-890	69	-317	-1	34	7	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4334	4334	204	204	139	14	3.8	>100	3.8

Asta : 21500 [100638 , 110638]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-553	10	56	0	44	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4346	4346	204	204	139	78	4.0	>100	4.0

Asta : 21501 [21501 , 30635]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-606	-191	135	0	-12	-21	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	23	4.9	>100	4.9

Asta : 21501 [100635 , 110635]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-477	-115	82	-0	38	7	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4350	4350	204	204	139	38	3.9	>100	3.9

Asta : 21502 [21502 , 30738]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-701	231	-197	-0	21	25	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4348	4348	204	204	139	19	3.7	>100	3.7

Asta : 21502 [100738 , 110738]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-491	54	63	0	38	-3	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4349	4349	204	204	139	69	4.3	>100	4.3

Asta : 21503 [21503 , 30718]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
---	-----	---	----	----	----	----	----	-----	-----	-------

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1006	-131	-372	1	45	-14	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4330	4330	204	204	139	12	2.8	>100	2.8

Asta : 21503 [100718 , 110718]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-551	-26	48	-0	43	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	91	3.9	>100	3.9

Asta : 21504 [21504 , 30687]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-801	-108	-407	-1	43	-11	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4337	4337	204	204	139	11	3.1	>100	3.1

Asta : 21504 [100687 , 110687]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-551	3	37	0	42	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4345	4345	204	204	139	>100	4.1	>100	4.1

Asta : 21505 [21505 , 30653]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-805	-132	-205	0	22	-14	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4342	4342	204	204	139	21	4.3	>100	4.3

Asta : 21505 [100653 , 110653]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-475	-120	84	-0	38	8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	36	3.9	>100	3.9

Asta : 21506 [21506 , 30750]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-606	-231	278	0	-27	-25	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4347	4347	204	204	139	16	3.4	>100	3.4

Asta : 21506 [100750 , 110750]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-484	-66	69	-0	38	4	--	--	2

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4350	4350	204	204	139	63	4.2	>100	4.2

Asta : 21507 [21507 , 30662]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-797	129	-191	-0	21	14	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4344	4344	204	204	139	23	4.5	>100	4.5

Asta : 21507 [100662 , 110662]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-475	118	85	0	38	-8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	37	3.9	>100	3.9

Asta : 21508 [21508 , 30726]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1006	131	-361	-1	39	14	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4332	4332	204	204	139	12	3.1	>100	3.1

Asta : 21508 [100726 , 110726]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-552	26	43	0	43	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4347	4347	204	204	139	>100	3.9	>100	3.9

Asta : 21509 [21509 , 30695]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-711	105	-314	0	34	11	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4347	4347	204	204	139	14	3.8	>100	3.8

Asta : 21509 [100695 , 110695]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-551	-3	36	-0	42	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4346	4346	204	204	139	>100	4.1	>100	4.1

Asta : 21510 [100819 , 110819]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-227	-186	-5	0	18	15	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4355	4355	204	204	139	23	5.6	>100	5.6

Asta : 21511 [100818 , 110818]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-159	43	284	-4	32	-4	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4228	4228	204	204	139	15	5.4	34	5.4

Asta : 21512 [21512 , 30762]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-739	-6	-334	0	38	-1	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	13	4.2	>100	4.2

Asta : 21512 [100762 , 110762]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-497	-188	103	0	40	12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4352	4352	204	204	139	23	3.4	>100	3.4

Asta : 21513 [21513 , 30764]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-778	3	-343	-0	38	1	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4347	4347	204	204	139	13	4.2	>100	4.2

Asta : 21513 [100764 , 110764]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-495	197	87	-0	39	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4354	4354	204	204	139	22	3.5	>100	3.5

Asta : 31498 [31498 , 60563]Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-822	165	8	-1	-1	34	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4309	4309	204	204	139	26	4.4	96	4.4

Asta : 31498 [110563 , 130563]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-323	46	45	1	38	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4338	4338	204	204	139	93	4.6	>100	4.6

Asta : 31499 [31499 , 60560]Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-878	-161	11	1	-1	-33	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4311	4311	204	204	139	27	4.4	99	4.4

Asta : 31499 [110560 , 130560]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-304	-11	26	-1	40	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4339	4339	204	204	139	>100	4.6	>100	4.6

Asta : 31500 [31500 , 60557]

Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-888	163	14	-1	-2	34	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4310	4310	204	204	139	26	4.3	98	4.3

Asta : 31500 [110557 , 130557]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-303	10	27	1	40	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4338	4338	204	204	139	>100	4.6	>100	4.6

Asta : 31501 [31501 , 60554]

Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-823	-164	3	1	1	-34	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4311	4311	204	204	139	26	4.4	100	4.4

Asta : 31501 [110554 , 130554]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-326	-42	41	-1	38	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4338	4338	204	204	139	>100	4.7	>100	4.7

Asta : 31502 [31502 , 60683]

Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-904	165	12	-1	3	34	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4313	4313	204	204	139	26	4.1	>100	4.1

Asta : 31502 [110683 , 130683]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-330	-11	28	0	38	3	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4343	4343	204	204	139	>100	4.5	>100	4.5

Asta : 31503 [31503 , 60649]

Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-899	-162	18	1	-4	-33	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4313	4313	204	204	139	27	4.2	>100	4.2

Asta : 31503 [110649 , 130649]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-296	-16	19	-1	39	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4337	4337	204	204	139	>100	4.7	>100	4.7

Asta : 31504 [31504 , 60608]

Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-745	164	11	-1	2	34	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4310	4310	204	204	139	26	4.4	96	4.4

Asta : 31504 [110608 , 130608]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-308	4	11	0	39	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4340	4340	204	204	139	>100	4.7	>100	4.7

Asta : 31505 [31505 , 60576]

Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-852	-161	15	1	-3	-33	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4310	4310	204	204	139	27	4.3	97	4.3

Asta : 31505 [110576 , 130576]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-321	-52	43	-1	38	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4336	4336	204	204	139	84	4.6	>100	4.6

Asta : 31506 [31506 , 60617]

Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-761	-165	11	1	2	-34	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4310	4310	204	204	139	26	4.4	97	4.4

Asta : 31506 [110617 , 130617]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-309	-2	10	-0	39	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4341	4341	204	204	139	>100	4.7	>100	4.7

Asta : 31507 [31507 , 60658]Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-891	163	18	-1	-4	33	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4312	4312	204	204	139	26	4.1	>100	4.1

Asta : 31507 [110658 , 130658]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-298	21	15	1	39	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4336	4336	204	204	139	>100	4.6	>100	4.6

Asta : 31508 [31508 , 60691]Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-918	-165	19	1	-4	-34	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4312	4312	204	204	139	26	4.1	>100	4.1

Asta : 31508 [110691 , 130691]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-333	4	32	-0	39	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4341	4341	204	204	139	>100	4.5	>100	4.5

Asta : 31509 [31509 , 60585]Sez. G: Tubo40x40x4 L=31.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-850	162	14	-1	-3	33	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4311	4311	204	204	139	27	4.3	99	4.3

Asta : 31509 [110585 , 130585]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-320	49	44	1	38	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4336	4336	204	204	139	89	4.6	>100	4.6

Asta : 31510 [110793 , 130793]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-222	-169	-9	0	18	13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	26	5.9	>100	5.9

Asta : 31511 [110769 , 130769]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-157	34	189	1	33	-4	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4333	4333	204	204	139	23	5.2	>100	5.2

Asta : 31512 [110734 , 130734]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-586	-87	-6	-0	38	-9	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4352	4352	204	204	139	50	3.7	>100	3.7

Asta : 31513 [110735 , 130735]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-439	93	43	0	40	-5	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4345	4345	204	204	139	47	4.0	>100	4.0

Asta : 50445 [50445 , 60445]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-584	-174	-88	1	11	-21	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4320	4320	204	204	139	25	5.1	>100	5.1

Asta : 50445 [130445 , 140445]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-402	-102	-7	1	27	-12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4310	4310	204	204	139	42	4.6	96	4.6

Asta : 50449 [50449 , 60449]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-730	46	-184	-1	21	6	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4338	4338	204	204	139	24	5.5	>100	5.5

Asta : 50449 [130449 , 140449]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-550	7	67	0	43	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4352	4352	204	204	139	65	4.0	>100	4.0

Asta : 50453 [50453 , 60453]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-782	-155	-73	1	10	-18	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4315	4315	204	204	139	28	5.3	>100	5.3

Asta : 50453 [130453 , 140453]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-548	2	66	-0	43	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4352	4352	204	204	139	66	4.0	>100	4.0

Asta : 50457 [50457 , 60457]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-567	172	-85	-1	11	20	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4320	4320	204	204	139	25	5.3	>100	5.3

Asta : 50457 [130457 , 140457]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-391	93	-16	-1	28	10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4316	4316	204	204	139	47	4.7	>100	4.7

Asta : 50466 [130466 , 140466]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-244	-92	81	-2	23	8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4297	4297	204	204	139	47	5.8	75	5.8

Asta : 50470 [130470 , 140470]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-248	106	71	2	22	-11	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4284	4284	204	204	139	40	5.7	61	5.7

Asta : 50486 [130486 , 140486]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-209	89	81	2	23	-8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4298	4298	204	204	139	48	5.9	76	5.9

Asta : 50490 [50490 , 60490]Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-561	-96	-171	1	20	-11	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4337	4337	204	204	139	25	5.3	>100	5.3

Asta : 50490 [130490 , 140490]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-421	-86	-22	1	27	-11	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4315	4315	204	204	139	50	4.7	>100	4.7

Asta : 50499 [50499 , 60499]Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-560	97	-168	-1	19	11	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4339	4339	204	204	139	26	5.4	>100	5.4

Asta : 50499 [130499 , 140499]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-489	77	-27	-1	26	11	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4314	4314	204	204	139	56	4.6	>100	4.6

Asta : 50503 [130503 , 140503]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-138	-85	84	-2	24	9	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4298	4298	204	204	139	50	5.9	76	5.9

Asta : 50527 [50527 , 60527]Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-801	148	-131	-1	16	18	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4313	4313	204	204	139	29	4.6	>100	4.6

Asta : 50527 [130527 , 140527]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-545	-0	57	0	43	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4349	4349	204	204	139	76	4.1	>100	4.1

Asta : 50540 [50540 , 60540]Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-788	-146	-110	1	14	-17	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4314	4314	204	204	139	29	4.9	>100	4.9

Asta : 50540 [130540 , 140540]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-544	3	57	-0	42	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	77	4.0	>100	4.0

Asta : 50570 [50570 , 60570]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-804	-81	-234	1	26	-9	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4330	4330	204	204	139	18	4.4	>100	4.4

Asta : 50570 [130570 , 140570]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-551	-2	59	-0	43	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4353	4353	204	204	139	73	4.1	>100	4.1

Asta : 50580 [50580 , 60580]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-797	78	-227	-1	26	9	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4335	4335	204	204	139	19	4.5	>100	4.5

Asta : 50580 [130580 , 140580]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-552	7	57	-0	43	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4353	4353	204	204	139	76	4.0	>100	4.0

Asta : 50603 [50603 , 60603]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-551	135	-188	-1	21	16	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4321	4321	204	204	139	23	4.6	>100	4.6

Asta : 50603 [130603 , 140603]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-362	102	15	-0	25	-7	--	--	2

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4345	4345	204	204	139	42	5.6	>100	5.6

Asta : 50612 [50612 , 60612]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-529	-134	-164	1	19	-16	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4329	4329	204	204	139	26	4.9	>100	4.9

Asta : 50612 [130612 , 140612]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-324	-94	-25	1	30	-8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4321	4321	204	204	139	46	4.8	>100	4.8

Asta : 50626 [130626 , 140626]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-328	139	72	2	23	-10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4293	4293	204	204	139	31	5.4	71	5.4

Asta : 50672 [130672 , 140672]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-462	-27	133	-4	33	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4245	4245	204	204	139	32	5.0	39	5.0

Asta : 50676 [50676 , 60676]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-606	-9	-315	-2	37	-4	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4303	4303	204	204	139	14	4.1	84	4.1

Asta : 50676 [130676 , 140676]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-382	-174	1	2	28	-18	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4299	4299	204	204	139	25	4.0	78	4.0

Asta : 50682 [50682 , 60682]

Sez. G: Tubo40x40x4 L=14.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-565	8	-356	0	41	1	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4350	4350	204	204	139	12	4.1	>100	4.1

Asta : 50682 [130682 , 140682]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-153	97	-98	-3	28	13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4251	4251	204	204	139	43	4.8	42	4.8

Asta : 50736 [130736 , 140736]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-141	70	273	-4	31	-6	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4217	4217	204	204	139	15	5.3	32	5.3

Asta : 61498 [140360 , 160360]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-215	142	15	0	22	12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4346	4346	204	204	139	31	5.4	>100	5.4

Asta : 61499 [61499 , 80357]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-797	-105	15	1	-2	-21	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4328	4328	204	204	139	41	5.9	>100	5.9

Asta : 61499 [140357 , 160357]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-331	-12	35	-0	40	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4341	4341	204	204	139	>100	4.5	>100	4.5

Asta : 61500 [61500 , 80354]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-800	105	12	-1	-2	21	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4326	4326	204	204	139	41	5.9	>100	5.9

Asta : 61500 [140354 , 160354]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-330	14	35	0	40	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4340	4340	204	204	139	>100	4.5	>100	4.5

Asta : 61501 [140351 , 160351]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-229	-147	15	-0	23	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4347	4347	204	204	139	30	5.2	>100	5.2

Asta : 61502 [140522 , 160522]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-198	137	14	0	25	-9	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4350	4350	204	204	139	32	5.5	>100	5.5

Asta : 61503 [140481 , 160481]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-320	-22	29	-1	40	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4339	4339	204	204	139	>100	4.5	>100	4.5

Asta : 61504 [61504 , 80424]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-769	105	19	-1	-4	21	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4327	4327	204	204	139	41	5.8	>100	5.8

Asta : 61504 [140424 , 160424]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-326	7	27	0	39	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4341	4341	204	204	139	>100	4.6	>100	4.6

Asta : 61505 [140392 , 160392]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-212	-143	11	-0	22	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4345	4345	204	204	139	30	5.4	>100	5.4

Asta : 61506 [140437 , 160437]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-328	-3	27	-0	39	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4342	4342	204	204	139	>100	4.7	>100	4.7

Asta : 61507 [61507 , 80495]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-825	105	17	-1	-3	21	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4328	4328	204	204	139	41	5.8	>100	5.8

Asta : 61507 [140495 , 160495]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-319	26	26	1	40	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4338	4338	204	204	139	>100	4.5	>100	4.5

Asta : 61508 [61508 , 80536]

Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-648	-114	19	1	-3	-23	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4328	4328	204	204	139	38	5.8	>100	5.8

Asta : 61508 [140536 , 160536]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-197	-128	4	-0	24	-10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4348	4348	204	204	139	34	5.5	>100	5.5

Asta : 61509 [140401 , 160401]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-219	141	11	0	22	13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4345	4345	204	204	139	31	5.4	>100	5.4

Asta : 61510 [140378 , 160378]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-185	152	25	0	25	-12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4350	4350	204	204	139	29	5.1	>100	5.1

Asta : 61511 [140363 , 160363]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-193	-155	26	-0	25	12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	28	5.1	>100	5.1

Asta : 61512 [140367 , 160367]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-194	164	26	0	26	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	27	4.8	>100	4.8

Asta : 61513 [140389 , 160389]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-173	-151	25	-0	25	13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4350	4350	204	204	139	29	5.1	>100	5.1

Asta : 61514 [61514 , 80546]Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-633	-113	17	1	-4	-23	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4329	4329	204	204	139	38	5.8	>100	5.8

Asta : 61514 [140546 , 160546]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-187	-183	7	-0	24	14	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4343	4343	204	204	139	24	5.0	>100	5.0

Asta : 61515 [61515 , 80597]Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-566	-111	22	1	-5	-22	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4335	4335	204	204	139	39	5.9	>100	5.9

Asta : 61515 [140597 , 160597]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-177	119	12	0	26	-11	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4350	4350	204	204	139	37	5.3	>100	5.3

Asta : 61516 [61516 , 80600]Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-933	117	43	-1	-9	23	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4332	4332	204	204	139	37	4.5	>100	4.5

Asta : 61516 [140600 , 160600]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-363	84	11	-0	41	-7	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4345	4345	204	204	139	52	3.9	>100	3.9

Asta : 61517 [61517 , 80550]Sez. G: Tubo40x40x4 L=30.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-596	119	13	-1	-3	24	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4321	4321	204	204	139	36	5.9	>100	5.9

Asta : 61517 [140550 , 160550]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-179	180	15	0	26	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4344	4344	204	204	139	24	4.9	>100	4.9

Asta : 61518 [140681 , 160681]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-235	185	27	-0	21	-15	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4352	4352	204	204	139	24	5.3	>100	5.3

Asta : 61519 [140621 , 160621]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-306	-213	41	-0	27	14	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4354	4354	204	204	139	20	4.5	>100	4.5

Asta : 61520 [140665 , 160665]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-173	-149	151	-2	25	-12	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4305	4305	204	204	139	28	5.2	87	5.2

Asta : 70262 [160262 , 170262]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-408	-147	64	-0	32	10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4353	4353	204	204	139	30	4.3	>100	4.3

Asta : 70266 [70266 , 80266]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-774	61	-222	-0	23	7	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4341	4341	204	204	139	20	5.1	>100	5.1

Asta : 70266 [160266 , 170266]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-556	9	64	0	44	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	68	3.9	>100	3.9

Asta : 70270 [70270 , 80270]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-785	-61	-210	0	22	-7	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4340	4340	204	204	139	21	5.2	>100	5.2

Asta : 70270 [160270 , 170270]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-556	-7	64	-0	44	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	68	3.9	>100	3.9

Asta : 70274 [70274 , 80274]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-595	179	-58	-1	7	20	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4339	4339	204	204	139	24	5.9	>100	5.9

Asta : 70274 [160274 , 170274]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-390	150	61	0	31	-10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4353	4353	204	204	139	29	4.4	>100	4.4

Asta : 70279 [160279 , 170279]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-387	-162	60	-0	31	13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4352	4352	204	204	139	27	4.1	>100	4.1

Asta : 70283 [160283 , 170283]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-398	162	61	0	32	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4352	4352	204	204	139	27	4.0	>100	4.0

Asta : 70290 [160290 , 170290]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-382	166	52	0	31	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4352	4352	204	204	139	26	4.2	>100	4.2

Asta : 70294 [160294 , 170294]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-373	-167	49	-0	30	13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	26	4.2	>100	4.2

Asta : 70303 [160303 , 170303]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-388	-148	43	-0	30	10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4354	4354	204	204	139	29	4.5	>100	4.5

Asta : 70312 [160312 , 170312]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-387	151	43	0	29	-10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4355	4355	204	204	139	29	4.6	>100	4.6

Asta : 70333 [70333 , 80333]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-810	154	-126	-1	14	17	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4333	4333	204	204	139	28	4.9	>100	4.9

Asta : 70333 [160333 , 170333]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-551	6	45	0	42	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4347	4347	204	204	139	96	4.1	>100	4.1

Asta : 70346 [70346 , 80346]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-818	-163	-125	1	14	-18	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4334	4334	204	204	139	27	4.8	>100	4.8

Asta : 70346 [160346 , 170346]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-552	-2	47	-0	42	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4346	4346	204	204	139	93	4.1	>100	4.1

Asta : 70384 [70384 , 80384]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-847	-92	-224	1	28	-10	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4338	4338	204	204	139	19	4.1	>100	4.1

Asta : 70384 [160384 , 170384]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-552	-12	39	-0	42	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4349	4349	204	204	139	>100	4.1	>100	4.1

Asta : 70396 [70396 , 80396]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-820	92	-194	-0	25	10	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4340	4340	204	204	139	22	4.5	>100	4.5

Asta : 70396 [160396 , 170396]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-554	20	36	0	42	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4349	4349	204	204	139	>100	4.0	>100	4.0

Asta : 70418 [70418 , 80418]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-637	185	-147	-0	16	20	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4345	4345	204	204	139	23	4.6	>100	4.6

Asta : 70418 [160418 , 170418]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-401	135	31	-0	30	-10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4353	4353	204	204	139	32	4.5	>100	4.5

Asta : 70429 [70429 , 80429]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-527	-188	116	0	-10	-21	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4345	4345	204	204	139	23	5.4	>100	5.4

Asta : 70429 [160429 , 170429]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-409	-120	14	-0	29	9	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4347	4347	204	204	139	36	4.7	>100	4.7

Asta : 70461 [70461 , 80461]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-727	-133	213	1	-20	-14	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4339	4339	204	204	139	20	4.7	>100	4.7

Asta : 70461 [160461 , 170461]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-408	-192	-7	-0	29	-14	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	23	4.2	>100	4.2

Asta : 70474 [70474 , 80474]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-629	116	-174	-0	19	13	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4347	4347	204	204	139	25	5.2	>100	5.2

Asta : 70474 [160474 , 170474]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-367	178	30	-0	28	-13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4342	4342	204	204	139	24	4.5	>100	4.5

Asta : 70518 [70518 , 80518]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-780	192	-232	-1	24	21	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4326	4326	204	204	139	19	3.7	>100	3.7

Asta : 70518 [160518 , 170518]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-405	99	-13	1	28	-9	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4339	4339	204	204	139	44	4.8	>100	4.8

Asta : 70532 [70532 , 80532]

Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-910	-157	-419	1	44	-17	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4319	4319	204	204	139	10	2.8	>100	2.8

Asta : 70532 [160532 , 170532]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-218	132	274	-0	32	-10	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4345	4345	204	204	139	16	4.5	>100	4.5

Asta : 70553 [70553 , 80553]Sez. G: Tubo40x40x4 L=13.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-742	-7	-388	0	40	-3	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4350	4350	204	204	139	11	3.9	>100	3.9

Asta : 70553 [160553 , 170553]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-232	-122	388	-2	42	10	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4286	4286	204	204	139	11	3.7	63	3.7

Asta : 70592 [160592 , 170592]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-126	-45	-249	5	30	-3	--	--	(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4212	4212	204	204	139	17	5.9	31	5.9

Asta : 70630 [160630 , 170630]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-216	188	30	0	19	-15	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4355	4355	204	204	139	23	5.5	>100	5.5

Asta : 91498 [91498 , 110201]Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-668	127	18	-1	-3	24	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4322	4322	204	204	139	34	5.7	>100	5.7

Asta : 91498 [170201 , 180201]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-219	141	27	0	27	-10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4349	4349	204	204	139	31	5.2	>100	5.2

Asta : 91499 [91499 , 110198]Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-863	-125	31	1	-5	-24	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4326	4326	204	204	139	35	5.1	>100	5.1

Asta : 91499 [170198 , 180198]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-308	-24	24	-0	36	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4343	4343	204	204	139	>100	4.9	>100	4.9

Asta : 91500 [91500 , 110195]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-870	126	29	-1	-4	24	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4323	4323	204	204	139	34	5.2	>100	5.2

Asta : 91500 [170195 , 180195]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-308	23	24	0	36	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4343	4343	204	204	139	>100	4.9	>100	4.9

Asta : 91501 [91501 , 110192]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-746	-130	28	1	-4	-25	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4323	4323	204	204	139	33	5.2	>100	5.2

Asta : 91501 [170192 , 180192]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-229	-134	26	-0	27	9	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	33	5.2	>100	5.2

Asta : 91503 [91503 , 110299]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-831	-103	29	1	-5	-20	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4332	4332	204	204	139	42	5.7	>100	5.7

Asta : 91503 [170299 , 180299]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-275	-34	2	-0	35	3	--	--	2

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4340	4340	204	204	139	>100	4.9	>100	4.9

Asta : 91504 [91504 , 110251]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-825	117	33	-1	-6	22	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4328	4328	204	204	139	37	5.2	>100	5.2

Asta : 91504 [170251 , 180251]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-292	18	11	0	36	-1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4344	4344	204	204	139	>100	4.9	>100	4.9

Asta : 91505 [91505 , 110228]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-757	-117	28	1	-5	-22	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4325	4325	204	204	139	37	5.5	>100	5.5

Asta : 91505 [170228 , 180228]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-197	-146	8	-0	25	-12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4343	4343	204	204	139	30	5.1	>100	5.1

Asta : 91506 [91506 , 110258]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-816	-134	32	1	-6	-25	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4323	4323	204	204	139	32	4.9	>100	4.9

Asta : 91506 [170258 , 180258]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-293	-17	12	-0	36	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4343	4343	204	204	139	>100	4.9	>100	4.9

Asta : 91507 [91507 , 110308]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-888	132	32	-1	-6	25	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4337	4337	204	204	139	33	4.8	>100	4.8

Asta : 91507 [170308 , 180308]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-268	35	-2	0	34	3	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4342	4342	204	204	139	>100	5.1	>100	5.1

Asta : 91508 [91508 , 110339]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-807	-137	49	1	-8	-26	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4330	4330	204	204	139	32	4.5	>100	4.5

Asta : 91509 [91509 , 110234]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-705	121	22	-1	-4	25	--	--	(12+13)-I-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4324	4324	204	204	139	36	5.3	>100	5.3

Asta : 91509 [170234 , 180234]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-197	148	9	0	25	12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4344	4344	204	204	139	29	5.2	>100	5.2

Asta : 91510 [170217 , 180217]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-214	161	27	0	28	-12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	27	4.7	>100	4.7

Asta : 91511 [91511 , 110211]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-755	-119	28	1	-5	-23	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4326	4326	204	204	139	36	5.4	>100	5.4

Asta : 91511 [170211 , 180211]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-221	-160	28	-0	27	12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4346	4346	204	204	139	27	4.8	>100	4.8

Asta : 91512 [91512 , 110214]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-730	127	25	-1	-4	24	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4328	4328	204	204	139	34	5.4	>100	5.4

Asta : 91512 [170214 , 180214]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-230	150	30	0	29	-12	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4346	4346	204	204	139	29	4.7	>100	4.7

Asta : 91513 [91513 , 110221]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-705	-131	23	1	-4	-25	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4324	4324	204	204	139	33	5.3	>100	5.3

Asta : 91513 [170221 , 180221]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-204	-164	24	-0	28	13	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4350	4350	204	204	139	27	4.8	>100	4.8

Asta : 91514 [91514 , 110370]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-729	-112	65	1	-11	-21	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4334	4334	204	204	139	39	4.9	>100	4.9

Asta : 91515 [91515 , 110433]

Sez. G: Tubo40x40x4 L=28.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-558	-109	70	1	-13	-20	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4327	4327	204	204	139	40	5.1	>100	5.1

Asta : 91516 [91516 , 110325]

Sez. G: Tubo40x40x4 L=17.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-501	-222	146	-0	-20	-28	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4343	4343	204	204	139	20	3.7	>100	3.7

Asta : 91517 [91517 , 110382]

Sez. G: Tubo40x40x4 L=17.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-977	196	-180	0	22	24	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4344	4344	204	204	139	22	3.4	>100	3.4

Asta : 91519 [91519 , 170566]

Sez. G: Tubo40x40x4 L=88.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-260	-34	49	1	-22	-17	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4329	4329	204	204	139	88	4.8	>100	4.8

Asta : 91519 [170566 , 180566]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-340	105	155	0	42	17	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	28	3.2	>100	3.2

Asta : 91520 [170480 , 180480]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-590	-218	117	-1	58	15	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4331	4331	204	204	139	20	2.5	>100	2.5

Asta : 91521 [170414 , 180414]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-369	302	15	-1	4	-30	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4329	4329	204	204	139	14	5.2	>100	5.2

Asta : 91522 [170507 , 180507]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-173	-302	-20	0	2	33	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4352	4352	204	204	139	14	5.6	>100	5.6

Asta : 101498 [101498 , 110145]

Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-849	-103	-252	1	21	-9	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4330	4330	204	204	139	17	4.9	>100	4.9

Asta : 101498 [180145 , 190145]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-729	-103	147	0	86	5	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4353	4353	204	204	139	30	2.0	>100	2.0

Asta : 101499 [101499 , 110146]Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-864	-58	-397	-0	33	-5	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4341	4341	204	204	139	11	4.1	>100	4.1

Asta : 101499 [180146 , 190146]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-786	-26	123	-0	95	2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4350	4350	204	204	139	35	1.9	>100	1.9

Asta : 101500 [101500 , 110147]Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-858	51	-398	0	33	5	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4345	4345	204	204	139	11	4.1	>100	4.1

Asta : 101500 [180147 , 190147]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-789	17	124	0	94	-2	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4352	4352	204	204	139	35	1.9	>100	1.9

Asta : 101501 [101501 , 110150]Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-841	91	-271	-1	23	8	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4328	4328	204	204	139	16	4.8	>100	4.8

Asta : 101501 [180150 , 190150]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-693	123	140	-0	83	-7	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	31	2.1	>100	2.1

Asta : 101502 [101502 , 180186]Sez. G: Tubo40x40x4 L=79.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
79	1	-298	49	-43	1	-20	-19	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
79	1	15086	4327	4327	204	204	139	88	4.7	>100	4.7

Asta : 101503 [101503 , 110224]Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1082	-142	-476	1	42	-13	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4318	4318	204	204	139	9.1	2.9	>100	2.9

Asta : 101503 [180224 , 190224]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-290	-20	135	-0	36	-18	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	32	3.5	>100	3.5

Asta : 101504 [101504 , 110248]

Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-916	124	-319	-0	27	12	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4341	4341	204	204	139	14	4.0	>100	4.0

Asta : 101505 [101505 , 110189]

Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-798	-113	-475	-0	41	-10	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4343	4343	204	204	139	9.1	3.3	>100	3.3

Asta : 101505 [180189 , 190189]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-686	-86	-2	-0	59	9	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	51	2.7	>100	2.7

Asta : 101506 [101506 , 110173]

Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-944	-147	-289	1	25	-13	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4334	4334	204	204	139	15	4.0	>100	4.0

Asta : 101506 [180173 , 190173]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-552	-173	4	-0	51	-15	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4350	4350	204	204	139	25	2.8	>100	2.8

Asta : 101507 [101507 , 110232]

Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1121	182	-420	-1	37	17	--	--	(12+13)-IV-2

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4310	4310	204	204	139	10	3.0	97	3.0

Asta : 101507 [180232 , 190232]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-302	6	262	0	41	18	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4348	4348	204	204	139	17	3.3	>100	3.3

Asta : 101508 [101508 , 110176]

Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-967	169	-350	-1	30	15	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4328	4328	204	204	139	12	3.5	>100	3.5

Asta : 101508 [180176 , 190176]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-346	175	-349	0	54	15	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	12	2.8	>100	2.8

Asta : 101509 [101509 , 110256]

Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-814	-264	233	0	-23	-26	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4342	4342	204	204	139	16	3.4	>100	3.4

Asta : 101509 [110256 , 180256]

Sez. G: Tubo40x40x4 L=75.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-1010	-10	36	-0	20	6	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	15086	4350	4350	204	204	139	>100	5.3	>100	5.3

Asta : 101510 [101510 , 110204]

Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-799	131	-376	0	32	12	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4348	4348	204	204	139	12	3.7	>100	3.7

Asta : 101510 [180204 , 190204]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-694	89	9	0	60	-9	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	49	2.6	>100	2.6

Asta : 101511 [101511 , 110154]Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-855	-95	-251	1	21	-9	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4333	4333	204	204	139	17	5.0	>100	5.0

Asta : 101511 [180154 , 190154]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-656	-160	113	0	78	11	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4354	4354	204	204	139	27	2.1	>100	2.1

Asta : 101512 [101512 , 110165]Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-810	156	-160	-1	14	15	--	--	(12+13)-I-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4314	4314	204	204	139	27	5.2	>100	5.2

Asta : 101512 [180165 , 190165]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-611	100	63	-0	65	-8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4353	4353	204	204	139	43	2.5	>100	2.5

Asta : 101513 [101513 , 110168]Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-657	77	-294	0	25	7	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4349	4349	204	204	139	15	5.1	>100	5.1

Asta : 101513 [180168 , 190168]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-590	-107	50	-0	62	8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4354	4354	204	204	139	41	2.6	>100	2.6

Asta : 101514 [101514 , 110162]Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-895	111	-287	-1	24	10	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4329	4329	204	204	139	15	4.4	>100	4.4

Asta : 101514 [180162 , 190162]Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
---	-----	---	----	----	----	----	----	-----	-----	-------

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-675	151	109	-0	80	-11	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4351	4351	204	204	139	29	2.0	>100	2.0

Asta : 101515 [101515 , 180243]

Sez. G: Tubo40x40x4 L=81.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
81	1	-519	-9	-53	-0	-29	5	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
81	1	15086	4353	4353	204	204	139	83	5.0	>100	5.0

Asta : 101517 [101517 , 180404]

Sez. G: Tubo40x40x4 L=86.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
86	1	-370	-34	-17	0	-11	20	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
86	1	15086	4353	4353	204	204	139	>100	5.6	>100	5.6

Asta : 101518 [101518 , 110322]

Sez. G: Tubo40x40x4 L=11.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-885	13	-322	-0	29	3	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	15086	4351	4351	204	204	139	13	4.7	>100	4.7

Asta : 101519 [101519 , 180465]

Sez. G: Tubo40x40x4 L=86.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
86	1	-185	24	-84	-1	-38	-11	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
86	1	15086	4328	4328	204	204	139	52	4.0	>100	4.0

Asta : 101520 [101520 , 180376]

Sez. G: Tubo40x40x4 L=84.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
84	1	-582	-9	-76	-0	-42	5	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
84	1	15086	4353	4353	204	204	139	57	3.7	>100	3.7

Asta : 101523 [101523 , 180231]

Sez. G: Tubo40x40x4 L=83.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
83	1	-300	-20	-44	-0	-25	10	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
83	1	15086	4351	4351	204	204	139	98	5.2	>100	5.2

Asta : 110097 [110097 , 190097]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-679	-6	-107	-0	-63	3	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4354	4354	204	204	139	41	2.7	>100	2.7

Asta : 110098 [110098 , 190098]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-759	0	-120	-0	-70	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4354	4354	204	204	139	36	2.5	>100	2.5

Asta : 110099 [110099 , 190099]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-761	-2	-120	0	-70	1	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4355	4355	204	204	139	36	2.5	>100	2.5

Asta : 110101 [110101 , 190101]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-650	6	-104	0	-61	-4	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4355	4355	204	204	139	42	2.8	>100	2.8

Asta : 110107 [110107 , 190107]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-786	-15	-89	0	-52	8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4355	4355	204	204	139	49	2.9	>100	2.9

Asta : 110109 [110109 , 190109]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-862	14	-87	-0	-51	-8	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4354	4354	204	204	139	50	2.9	>100	2.9

Asta : 110113 [110113 , 190113]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-589	-52	-34	-0	-19	22	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4341	4341	204	204	139	84	4.1	>100	4.1

Asta : 110115 [110115 , 190115]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-568	-53	-25	-1	-14	24	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4337	4337	204	204	139	82	4.5	>100	4.5

Asta : 110123 [110123 , 190123]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-845	-52	22	-1	13	23	--	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4329	4329	204	204	139	83	4.3	>100	4.3

Asta : 110124 [110124 , 190124]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-728	-48	12	-1	13	20	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4335	4335	204	204	139	91	4.8	>100	4.8

Asta : 110137 [110137 , 190137]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-1822	-9	33	0	21	5	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4353	4353	204	204	139	>100	4.1	>100	4.1

Asta : 110139 [110139 , 190139]

Sez. G: Tubo40x40x4 L=90.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-793	57	23	1	14	-25	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	15086	4337	4337	204	204	139	77	4.1	>100	4.1

Asta : 110158 [180158 , 190158]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-346	412	-18	4	9	-59	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4243	4243	204	204	139	10	2.8	39	2.8

Asta : 110164 [180164 , 190164]

Sez. G: Tubo40x40x4 L=15.0 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-319	-428	-239	-2	-15	54	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	15086	4306	4306	204	204	139	10	2.8	88	2.8

VERIFICHE STATO LIMITE DI ESERCIZIO

Verifica spostamenti verticali delle aste in Acciaio più sollecitate secondo NTC 2008

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Travata: 8084 [10009 , 40019]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8085 [10039 , 40029]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8086 [10049 , 40059]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8087 [10079 , 40069]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8116 [10010 , 40020]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8117 [10040 , 40030]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8118 [10050 , 40060]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8119 [10080 , 40070]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8148 [10011 , 40021]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8149 [10041 , 40031]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8150 [10051 , 40061]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.21	>100

Travata: 8151 [10081 , 40071]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.21	>100

Travata: 8204 [10008 , 40018]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.21	>100

Travata: 8205 [10038 , 40028]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.21	>100

Travata: 8206 [10048 , 40058]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.21	>100

Travata: 8207 [10078 , 40068]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
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x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8236 [10007 , 40017]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8237 [10037 , 40027]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8238 [10047 , 40057]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8239 [10077 , 40067]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8268 [10006 , 40016]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8269 [10036 , 40026]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8270 [10046 , 40056]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8271 [10076 , 40066]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8300 [10005 , 40015]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8301 [10035 , 40025]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8302 [10045 , 40055]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8303 [10075 , 40065]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8332 [10004 , 40014]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8333 [10034 , 40024]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8334 [10044 , 40054]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8335 [10074 , 40064]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8384 [10011 , 40010]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8386 [10041 , 40040]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8388 [10051 , 40050]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8390 [10081 , 40080]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8392 [10021 , 40020]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
0.0	21	-0.00	5.21	>100

Travata: 8394 [10031 , 40030]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8396 [10061 , 40060]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8398 [10071 , 40070]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8400 [10008 , 40009]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8402 [10038 , 40039]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8404 [10048 , 40049]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8406 [10078 , 40079]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8408 [10028 , 40029]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8410 [10018 , 40019]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8412 [10058 , 40059]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8414 [10068 , 40069]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8416 [10007 , 40006]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8418 [10037 , 40036]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8420 [10047 , 40046]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8422 [10077 , 40076]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8424 [10017 , 40016]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8426 [10027 , 40026]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8428 [10057 , 40056]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8430 [10067 , 40066]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8432 [10004 , 40005]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8434 [10034 , 40035]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8436 [10044 , 40045]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8438 [10074 , 40075]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8440 [10014 , 40015]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8442 [10024 , 40025]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8444 [10054 , 40055]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8446 [10064 , 40065]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 401 [40009 , 40019]

L = 120.0cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
48.0	15	0.09	4.80	53

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
48.0	15	0.05	4.00	74

Travata: 405 [40010 , 40020]

L = 120.0cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
48.0	15	0.09	4.80	53

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
48.0	15	0.05	4.00	74

Travata: 409 [40011 , 40021]

L = 120.0cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
48.0	15	0.12	4.80	41

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
48.0	15	0.07	4.00	55

Travata: 413 [40008 , 40018]

L = 120.0cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
48.0	15	0.10	4.80	46

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
48.0	15	0.06	4.00	63

Travata: 417 [40007 , 40017]

L = 120.0cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
48.0	15	0.11	4.80	45

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
48.0	15	0.07	4.00	61

Travata: 421 [40006 , 40016]

$L = 120.0\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
48.0	15	0.09	4.80	54

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
48.0	15	0.05	4.00	76

Travata: 425 [40005 , 40015]

$L = 120.0\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
48.0	15	0.09	4.80	51

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
48.0	15	0.06	4.00	71

Travata: 429 [40004 , 40014]

$L = 120.0\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
48.0	15	0.10	4.80	46

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
48.0	15	0.06	4.00	64

Travata: 8041 [20779 , 70776]

$L = 138.1\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8042 [20776 , 70779]

$L = 138.1\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8043 [20834 , 70832]

$L = 138.1\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8044 [20832 , 70834]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8057 [20830 , 70828]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8058 [20828 , 70830]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8059 [20773 , 70770]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8060 [20770 , 70773]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
0.0	21	-0.00	4.60	>100

Travata: 8720 [20844 , 70821]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8721 [20821 , 70844]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8726 [20802 , 70782]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8734 [20782 , 70802]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8778 [20809 , 70790]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8783 [20790 , 70809]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	4.60	>100

Travata: 8788 [20847 , 70825]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	4.60	>100

Travata: 8795 [20825 , 70847]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	4.60	>100

Travata: 8674 [20862 , 70861]

L = 141.5cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
70.8	21	0.06	5.66	88

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	4.72	>100

Travata: 8675 [20860 , 70859]

L = 141.5cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
70.8	15	0.06	5.66	88

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	4.72	>100

Travata: 8676 [20858 , 70857]

L = 141.5cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
70.8	21	0.06	5.66	88

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.72	>100

Travata: 8677 [20856 , 70855]

L = 141.5cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.8	15	0.06	5.66	88

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.72	>100

Travata: 8680 [20855 , 70856]

L = 141.5cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.8	15	0.06	5.66	88

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.72	>100

Travata: 8681 [20857 , 70858]

L = 141.5cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.8	21	0.06	5.66	88

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.72	>100

Travata: 8682 [20859 , 70860]

L = 141.5cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.8	21	0.06	5.66	88

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.72	>100

Travata: 8683 [20861 , 70862]

L = 141.5cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.8	21	0.06	5.66	88

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.72	>100

Travata: 8079 [30707 , 90704]

$L = 135.5\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
67.7	21	0.06	5.42	98

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.52	>100

Travata: 8752 [30746 , 90722]

$L = 135.5\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
67.7	21	0.06	5.42	98

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.52	>100

Travata: 8817 [30786 , 90805]

$L = 135.5\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
67.7	21	0.06	5.42	98

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.52	>100

Travata: 701 [70779 , 70876]

$L = 156.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.15	6.24	40

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.11	5.20	48

Travata: 702 [70776 , 70874]

$L = 156.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.35	6.24	18

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.25	5.20	21

Travata: 703 [70773 , 70872]

$L = 156.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.34	6.24	19

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.24	5.20	22

Travata: 704 [70770 , 70870]

L = 156.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.14	6.24	43

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.10	5.20	51

Travata: 8045 [30713 , 100710]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	15	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8046 [30710 , 100713]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	15	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8047 [30644 , 100641]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	15	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8048 [30641 , 100644]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	15	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8061 [30704 , 100707]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8062 [30638 , 100635]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	15	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8063 [30635 , 100638]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	15	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 705 [70842 , 70843]

L = 775.4cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.8	15	1.05	31.02	29

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
70.8	15	0.75	25.85	35

Travata: 724 [70802 , 70877]

L = 122.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
61.2	15	0.81	4.89	6.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
61.2	15	0.58	4.08	7.1

Travata: 707 [70860 , 70009]

$L = 120.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
60.0	15	1.34	4.80	3.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.94	4.00	4.2

Travata: 708 [70861 , 70010]

$L = 120.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
60.0	15	1.33	4.80	3.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.94	4.00	4.3

Travata: 709 [70862 , 70011]

$L = 120.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
60.0	15	1.24	4.80	3.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.87	4.00	4.6

Travata: 710 [70863 , 70012]

$L = 120.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
60.0	15	0.76	4.80	6.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.53	4.00	7.5

Travata: 711 [70859 , 70008]

$L = 120.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
60.0	15	1.37	4.80	3.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.97	4.00	4.1

Travata: 712 [70858 , 70007]

$L = 120.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
60.0	15	1.38	4.80	3.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.97	4.00	4.1

Travata: 713 [70857 , 70006]

L = 120.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
60.0	15	1.34	4.80	3.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.95	4.00	4.2

Travata: 714 [70856 , 70005]

L = 120.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
60.0	15	1.40	4.80	3.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.99	4.00	4.1

Travata: 715 [70855 , 70004]

L = 120.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
60.0	15	0.98	4.80	4.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.69	4.00	5.8

Travata: 716 [70854 , 70003]

L = 120.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
60.0	15	0.58	4.80	8.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.0	15	0.41	4.00	9.8

Travata: 725 [70894 , 70002]

L = 84.9cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
46.7	15	0.13	3.40	25

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
46.7	15	0.09	2.83	30

Travata: 8716 [30718 , 100738]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8718 [30798 , 100765]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8722 [30765 , 100798]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	15	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8723 [30738 , 100718]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8727 [30722 , 100746]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8738 [30687 , 100653]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	4.79	>100

Travata: 8740 [30653 , 100687]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	4.79	>100

Travata: 718 [70863 , 70854]

L = 991.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
752.4	15	0.58	39.64	68

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
752.4	15	0.41	33.03	80

Travata: 719 [70821 , 70879]

L = 78.8cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
39.4	15	0.06	3.15	57

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
39.4	15	0.04	2.63	68

Travata: 720 [70844 , 70863]

L = 34.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
20.8	15	-0.05	1.38	26

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
20.8	15	-0.04	1.15	30

Travata: 728 [70895 , 70001]

L = 79.9cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
44.0	15	0.11	3.20	29

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
44.0	15	0.08	2.66	35

Travata: 721 [70847 , 70854]

L = 31.9cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
19.2	15	-0.03	1.28	37

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
19.2	15	-0.02	1.06	44

Travata: 722 [70825 , 70866]

L = 75.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
41.6	15	0.08	3.03	39

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
41.6	15	0.05	2.52	46

Travata: 723 [70809 , 70868]

L = 120.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
60.2	15	0.77	4.81	6.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
60.2	15	0.55	4.01	7.4

Travata: 8782 [30662 , 100695]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8784 [30731 , 100754]

L = 143.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8791 [30754 , 100731]

$L = 143.8\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8792 [30695 , 100662]

$L = 143.8\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8797 [30726 , 100750]

$L = 143.8\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
71.9	15	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8798 [30805 , 100786]

$L = 143.8\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 8802 [30750 , 100726]

$L = 143.8\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
71.9	21	0.06	5.75	92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.79	>100

Travata: 729 [70815 , 70812]

$L = 348.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
290.0	15	0.47	13.92	30

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
290.0	15	0.33	11.60	35

Travata: 730 [70896 , 70893]

L = 76.5cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
38.2	15	0.13	3.06	23

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
38.2	15	0.09	2.55	27

Travata: 731 [70893 , 70892]

L = 991.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
867.0	15	0.92	39.64	43

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
759.0	15	0.66	33.03	50

Travata: 732 [70892 , 70897]

L = 79.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
39.8	15	0.15	3.18	21

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
39.8	15	0.11	2.65	25

Travata: 733 [70907 , 70906]

L = 991.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
867.0	15	0.90	39.64	44

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
867.0	15	0.64	33.03	52

Travata: 8080 [40019 , 120009]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8081 [40029 , 120039]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8082 [120049 , 40059]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8083 [40069 , 120079]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8112 [40020 , 120010]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8113 [40030 , 120040]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8114 [120050 , 40060]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8115 [40070 , 120080]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8144 [40021 , 120011]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8145 [40031 , 120041]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8146 [120051 , 40061]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8147 [40071 , 120081]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8200 [40018 , 120008]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8201 [40028 , 120038]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8202 [120048 , 40058]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8203 [40068 , 120078]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8232 [40017 , 120007]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
0.0	21	-0.00	5.21	>100

Travata: 8233 [40027 , 120037]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8234 [120047 , 40057]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8235 [40067 , 120077]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8264 [40016 , 120006]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8265 [40026 , 120036]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8266 [120046 , 40056]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8267 [40066 , 120076]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8296 [40015 , 120005]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8297 [40025 , 120035]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8298 [120045 , 40055]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8299 [40065 , 120075]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8328 [40014 , 120004]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8329 [40024 , 120034]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8330 [120044 , 40054]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8331 [40064 , 120074]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8385 [40010 , 120011]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8387 [40040 , 120041]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8389 [40050 , 120051]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8391 [40080 , 120081]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8393 [40020 , 120021]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8395 [40030 , 120031]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8397 [40060 , 120061]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8399 [40070 , 120071]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8401 [40009 , 120008]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8403 [40039 , 120038]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8405 [40049 , 120048]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8407 [40079 , 120078]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8409 [40029 , 120028]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8411 [40019 , 120018]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8413 [40059 , 120058]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8415 [40069 , 120068]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8417 [40006 , 120007]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8419 [40036 , 120037]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8421 [40046 , 120047]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8423 [40076 , 120077]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8425 [40016 , 120017]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8427 [40026 , 120027]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8429 [40056 , 120057]

$L = 156.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8431 [40066 , 120067]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8433 [40005 , 120004]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8435 [40035 , 120034]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8437 [40045 , 120044]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8439 [40075 , 120074]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
0.0	21	-0.00	5.21	>100

Travata: 8441 [40015 , 120014]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	15	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8443 [40025 , 120024]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8445 [40055 , 120054]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 8447 [40065 , 120064]

L = 156.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.1	21	0.08	6.25	79

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.21	>100

Travata: 901 [90713 , 90779]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	18

Travata: 902 [90710 , 90776]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 903 [90707 , 90773]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 904 [90704 , 90770]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	19

Travata: 915 [90852 , 90894]

L = 91.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.18	3.65	20

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.6	15	0.13	3.04	24

Travata: 916 [90816 , 90850]

L = 91.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.26	3.65	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.6	15	0.18	3.04	17

Travata: 907 [90798 , 90844]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.26	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	16

Travata: 908 [90765 , 90821]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.41	3.60	8.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.29	3.00	10

Travata: 909 [90746 , 90802]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.37	3.60	9.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.26	3.00	12

Travata: 910 [90722 , 90782]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	19

Travata: 917 [90853 , 90895]

L = 91.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.18	3.65	20

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.6	15	0.13	3.04	24

Travata: 918 [90817 , 90851]

L = 91.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.26	3.65	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.6	15	0.18	3.04	17

Travata: 911 [90754 , 90809]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.36	3.60	9.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.26	3.00	12

Travata: 912 [90731 , 90790]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	19

Travata: 913 [90786 , 90825]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.40	3.60	9.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 914 [90805 , 90847]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.26	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	17

Travata: 1001 [100644 , 100713]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.29	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.20	3.00	15

Travata: 1002 [100641 , 100710]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 1003 [100638 , 100707]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 1004 [100635 , 100704]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.29	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.20	3.00	15

Travata: 8049 [60563 , 130560]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8050 [60560 , 130563]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8051 [60457 , 130453]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8052 [60453 , 130457]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8065 [60557 , 130554]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8066 [60554 , 130557]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8067 [60449 , 130445]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8068 [60445 , 130449]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 1015 [100818 , 100852]

$L = 91.3\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.18	3.65	20

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.6	15	0.13	3.04	24

Travata: 1016 [100762 , 100816]

$L = 91.3\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.32	3.65	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.6	15	0.22	3.04	14

Travata: 1007 [100738 , 100798]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.30	3.60	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.21	3.00	14

Travata: 1008 [100718 , 100765]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 1009 [100687 , 100746]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.40	3.60	9.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 1010 [100653 , 100722]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
45.0	15	0.29	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.20	3.00	15

Travata: 8724 [60603 , 130570]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8728 [60570 , 130603]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8729 [60683 , 130649]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8730 [60649 , 130683]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8735 [60576 , 130608]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
0.0	21	-0.00	4.70	>100

Travata: 8736 [60490 , 130527]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8742 [60608 , 130576]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8743 [60527 , 130490]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 1017 [100819 , 100853]

L = 90.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.3	15	0.17	3.62	21

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.3	15	0.12	3.02	25

Travata: 1018 [100764 , 100817]

L = 90.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.3	15	0.30	3.62	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.3	15	0.21	3.02	14

Travata: 8869 [60668 , 130622]

L = 140.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
70.4	21	0.06	5.63	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.69	>100

Travata: 8870 [60622 , 130668]

L = 140.8cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
70.4	15	0.06	5.63	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.69	>100

Travata: 8871 [60626 , 130672]

L = 141.0cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8872 [60672 , 130626]

L = 141.0cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 1011 [100695 , 100754]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.40	3.60	9.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 1012 [100662 , 100731]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.29	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.20	3.00	15

Travata: 1013 [100726 , 100786]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.40	3.60	9.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 8780 [60585 , 130617]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8790 [60499 , 130540]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8793 [60617 , 130585]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8794 [60540 , 130499]

L = 140.9cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8800 [60612 , 130580]

$L = 140.9\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8801 [60580 , 130612]

$L = 140.9\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8803 [60691 , 130658]

$L = 140.9\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
70.5	15	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 8804 [60658 , 130691]

$L = 140.9\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
70.5	21	0.06	5.64	94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.70	>100

Travata: 1014 [100750 , 100805]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.29	3.60	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.21	3.00	14

Travata: 1101 [110563 , 110644]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.33	3.60	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.23	3.00	13

Travata: 1103 [110560 , 110641]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1104 [110557 , 110638]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1105 [110554 , 110635]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.34	3.60	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.24	3.00	13

Travata: 1152 [110769 , 110818]

L = 90.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.3	15	0.17	3.62	21

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.3	15	0.12	3.02	26

Travata: 1153 [110734 , 110762]

L = 90.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.3	15	0.34	3.62	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.3	15	0.24	3.02	13

Travata: 1115 [110683 , 110738]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.35	3.60	10

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.25	3.00	12

Travata: 1117 [110649 , 110718]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1118 [110608 , 110687]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1119 [110576 , 110653]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.33	3.60	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.23	3.00	13

Travata: 1154 [110793 , 110819]

L = 91.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.18	3.65	21

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.6	15	0.12	3.04	25

Travata: 1155 [110735 , 110764]

$L = 91.2\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.36	3.65	10

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.6	15	0.25	3.04	12

Travata: 1127 [110617 , 110695]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1128 [110585 , 110662]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.34	3.60	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.24	3.00	13

Travata: 1130 [110658 , 110726]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1134 [110691 , 110750]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.34	3.60	10

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.24	3.00	12

Travata: 8053 [80357 , 160360]

$L = 139.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8054 [80270 , 160274]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8064 [80360 , 160357]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8069 [80354 , 160351]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8070 [80351 , 160354]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8071 [80266 , 160262]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
0.0	21	-0.00	4.64	>100

Travata: 8072 [80262 , 160266]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8078 [80274 , 160270]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8832 [80363 , 160378]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8833 [80279 , 160290]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8835 [80378 , 160363]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8836 [80290 , 160279]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8837 [80283 , 160294]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8839 [80294 , 160283]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8850 [80367 , 160389]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8852 [80389 , 160367]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8731 [80384 , 160418]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8732 [80481 , 160522]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8737 [80522 , 160481]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8739 [80303 , 160333]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8741 [80424 , 160392]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8744 [80392 , 160424]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8745 [80333 , 160303]

$L = 139.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8751 [80418 , 160384]

$L = 139.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8861 [80461 , 160518]

$L = 139.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8862 [80518 , 160461]

$L = 139.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8867 [80546 , 160597]

$L = 139.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8868 [80597 , 160546]

$L = 139.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8873 [80600 , 160550]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8874 [80550 , 160600]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8877 [80474 , 160532]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8878 [80532 , 160474]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8785 [80346 , 160312]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8787 [80437 , 160401]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8796 [80401 , 160437]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8799 [80495 , 160536]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8811 [80396 , 160429]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8813 [80429 , 160396]

L = 139.2cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8814 [80536 , 160495]

$L = 139.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	21	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 8818 [80312 , 160346]

$L = 139.2\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.6	15	0.06	5.57	95

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.64	>100

Travata: 1301 [130457 , 130563]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.37	3.60	9.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.26	3.00	12

Travata: 1302 [130453 , 130560]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1303 [130449 , 130557]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1304 [130445 , 130554]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
45.0	15	0.37	3.60	9.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.26	3.00	12

Travata: 1306 [130457 , 130445]

L = 348.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
290.0	15	0.14	13.92	98

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
290.0	15	0.10	11.60	>100

Travata: 1317 [130490 , 130457]

L = 137.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.2	15	0.11	5.50	50

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.2	15	0.08	4.59	60

Travata: 1318 [130445 , 130499]

L = 140.4cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
73.8	15	0.10	5.61	54

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
73.8	15	0.07	4.68	64

Travata: 1320 [130736 , 130769]

L = 91.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.17	3.65	21

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.6	15	0.12	3.04	25

Travata: 1321 [130676 , 130734]

L = 91.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.42	3.65	8.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
45.6	15	0.30	3.04	10

Travata: 1307 [130603 , 130683]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1308 [130570 , 130649]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1309 [130527 , 130608]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1310 [130490 , 130576]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.36	3.60	9.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.26	3.00	12

Travata: 1319 [130603 , 130570]

L = 138.4cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.8	15	0.14	5.53	38

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
68.8	15	0.10	4.61	46

Travata: 1590 [130736 , 130676]

L = 106.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
53.1	15	0.14	4.25	30

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
53.1	15	0.10	3.54	36

Travata: 1323 [130737 , 130793]

L = 89.9cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
44.9	15	0.19	3.59	19

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
44.9	15	0.13	3.00	23

Travata: 1324 [130682 , 130735]

L = 89.9cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
44.9	15	0.39	3.59	9.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
44.9	15	0.28	3.00	11

Travata: 1313 [130540 , 130617]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
45.0	15	0.27	3.00	11

Travata: 1314 [130499 , 130585]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
45.0	15	0.36	3.60	10

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
45.0	15	0.25	3.00	12

Travata: 1315 [130580 , 130658]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1316 [130612 , 130691]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1401 [140360 , 140457]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.22	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.15	3.00	19

Travata: 1402 [140357 , 140453]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1403 [140354 , 140449]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1404 [140351 , 140445]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	19

Travata: 1419 [140490 , 140457]

$L = 137.6\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
68.2	15	0.13	5.50	42

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.2	15	0.09	4.59	50

Travata: 1420 [140445 , 140499]

$L = 140.4\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
73.8	15	0.14	5.61	41

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
73.8	15	0.10	4.68	49

Travata: 1417 [140378 , 140486]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.22	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.15	3.00	20

Travata: 1418 [140363 , 140466]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.22	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.15	3.00	19

Travata: 1421 [140367 , 140470]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	19

Travata: 1422 [140389 , 140503]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.22	3.60	17

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.15	3.00	20

Travata: 1427 [140681 , 140736]

L = 90.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.3	15	0.17	3.62	22

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.3	15	0.12	3.02	26

Travata: 1428 [140621 , 140676]

L = 90.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.3	15	0.22	3.62	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.3	15	0.16	3.02	19

Travata: 1407 [140522 , 140603]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.22	3.60	17

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.15	3.00	20

Travata: 1408 [140481 , 140570]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1409 [140424 , 140527]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1410 [140392 , 140490]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.22	3.60	17

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.15	3.00	20

Travata: 1433 [140665 , 140717]

L = 79.9cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
40.0	15	0.12	3.20	27

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
40.0	15	0.08	2.66	33

Travata: 1591 [140736 , 140676]

L = 106.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
53.1	15	0.12	4.25	36

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
53.1	15	0.08	3.54	43

Travata: 1423 [140546 , 140622]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.22	3.60	17

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.15	3.00	20

Travata: 1424 [140597 , 140668]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	18

Travata: 1425 [140600 , 140672]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
44.0	15	0.37	3.60	9.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
44.0	15	0.26	3.00	11

Travata: 1426 [140550 , 140626]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	19

Travata: 1431 [140666 , 140730]

$L = 127.1\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
58.4	15	0.31	5.09	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
58.4	15	0.22	4.24	19

Travata: 1432 [140737 , 140667]

$L = 110.8\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
31.1	15	-0.04	4.43	99

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
31.1	15	-0.03	3.69	>100

Travata: 1413 [140437 , 140540]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1414 [140401 , 140499]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
45.0	15	0.21	3.60	17

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.15	3.00	20

Travata: 1415 [140495 , 140580]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1416 [140536 , 140612]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	19

Travata: 1593 [140703 , 140647]

L = 106.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
53.1	15	0.32	4.25	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
53.1	15	0.23	3.54	15

Travata: 1436 [140440 , 140700]

L = 617.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
546.5	15	0.59	24.71	42

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
546.5	15	0.42	20.59	49

Travata: 8039 [110150 , 180147]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
0.0	21	-0.00	4.60	>100

Travata: 8040 [110147 , 180150]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8055 [110201 , 180198]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8056 [110198 , 180201]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8074 [110195 , 180192]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8075 [110192 , 180195]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8076 [110146 , 180145]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8077 [110145 , 180146]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8828 [110217 , 180211]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8830 [110165 , 180154]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8831 [110154 , 180165]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8834 [110211 , 180217]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8838 [110214 , 180221]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8841 [110168 , 180162]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8842 [110221 , 180214]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8843 [110162 , 180168]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8717 [110248 , 180224]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8719 [110224 , 180248]

$L = 138.1\text{ cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{ cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8725 [110328 , 180299]

$L = 138.1\text{ cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{ cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8733 [110299 , 180328]

$L = 138.1\text{ cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{ cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8746 [110251 , 180228]

$L = 138.1\text{ cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{ cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8747 [110228 , 180251]

$L = 138.1\text{ cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{ cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8748 [110173 , 180189]

$L = 138.1\text{ cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{ cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8749 [110189 , 180173]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8853 [110382 , 180325]

L = 137.7cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.9	15	0.06	5.51	97

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.59	>100

Travata: 8854 [110325 , 180382]

L = 137.7cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.9	21	0.06	5.51	97

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.59	>100

Travata: 8857 [110433 , 180370]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8858 [110370 , 180433]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8776 [110176 , 180204]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8779 [110204 , 180176]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8786 [110234 , 180258]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8789 [110258 , 180234]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8812 [110339 , 180308]

L = 138.1cm

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8816 [110308 , 180339]

$L = 138.1\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8819 [110256 , 180232]

$L = 138.1\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	15	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 8820 [110232 , 180256]

$L = 138.1\text{cm}$

Crit.Prog: Acciaio_CompSemp $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
69.1	21	0.06	5.53	96

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	4.60	>100

Travata: 1601 [160274 , 160360]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.25	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	17

Travata: 1602 [160270 , 160357]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1603 [160266 , 160354]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1604 [160262 , 160351]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.26	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	17

Travata: 1615 [160290 , 160378]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.25	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	17

Travata: 1616 [160279 , 160363]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.25	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	17

Travata: 1617 [160283 , 160367]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.26	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	16

Travata: 1618 [160294 , 160389]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.25	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
45.0	15	0.17	3.00	17

Travata: 1623 [160630 , 160681]

L = 91.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.19	3.65	20

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.6	15	0.13	3.04	23

Travata: 1624 [160553 , 160621]

L = 91.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.6	15	0.28	3.65	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.6	15	0.19	3.04	16

Travata: 1607 [160418 , 160522]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.25	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	17

Travata: 1608 [160384 , 160481]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1609 [160333 , 160424]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1610 [160303 , 160392]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.25	3.60	15

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.17	3.00	17

Travata: 1626 [160592 , 160665]

L = 90.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.1	15	0.18	3.61	20

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.1	15	0.12	3.01	24

Travata: 1619 [160461 , 160546]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.26	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	17

Travata: 1620 [160518 , 160597]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.27	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.19	3.00	16

Travata: 1621 [160532 , 160600]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.44	3.60	8.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.31	3.00	9.7

Travata: 1622 [160474 , 160550]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.26	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	17

Travata: 1625 [160667 , 160592]

L = 91.5cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.8	15	0.13	3.66	29

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.8	15	0.09	3.05	35

Travata: 1611 [160346 , 160437]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1612 [160312 , 160401]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.24	3.60	15

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.17	3.00	18

Travata: 1613 [160396 , 160495]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.38	3.60	9.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1614 [160429 , 160536]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.25	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	17

Travata: 1701 [170201 , 170274]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.27	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.19	3.00	16

Travata: 1702 [170198 , 170270]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1703 [170195 , 170266]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 1704 [170192 , 170262]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.28	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.20	3.00	15

Travata: 1715 [170217 , 170290]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.28	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.20	3.00	15

Travata: 1716 [170211 , 170279]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.28	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.20	3.00	15

Travata: 1717 [170214 , 170283]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.29	3.60	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.20	3.00	15

Travata: 1718 [170221 , 170294]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.27	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.19	3.00	15

Travata: 1723 [170566 , 170630]

L = 90.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.3	15	0.12	3.62	30

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.3	15	0.08	3.02	36

Travata: 1724 [170480 , 170553]

L = 90.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.3	15	0.26	3.62	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.3	15	0.18	3.02	17

Travata: 1707 [170328 , 170418]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.29	3.60	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.21	3.00	14

Travata: 1708 [170299 , 170384]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 1709 [170251 , 170333]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1710 [170228 , 170303]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.27	3.60	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.19	3.00	16

Travata: 1721 [170442 , 170532]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
51.0	15	-0.08	3.60	48

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
51.0	15	-0.05	3.00	58

Travata: 1719 [170433 , 170518]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.31	3.60	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.22	3.00	14

Travata: 1720 [170370 , 170461]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.32	3.60	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.22	3.00	13

Travata: 1722 [170373 , 170474]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.26	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.18	3.00	16

Travata: 1725 [170592 , 170507]

$L = 97.3\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
48.7	15	0.12	3.89	33

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
48.7	15	0.08	3.24	41

Travata: 1726 [170507 , 170575]

$L = 89.9\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
44.9	15	0.09	3.60	40

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
44.9	15	0.06	3.00	49

Travata: 1711 [170258 , 170346]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.27	3.00	11

Travata: 1712 [170234 , 170312]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
45.0	15	0.27	3.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.19	3.00	16

Travata: 1713 [170308 , 170396]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.39	3.60	9.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.28	3.00	11

Travata: 1714 [170339 , 170429]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.30	3.60	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.21	3.00	14

Travata: 1801 [180150 , 180201]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.21	3.60	17

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.15	3.00	20

Travata: 1802 [180145 , 180192]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.22	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	19

Travata: 1803 [180146 , 180195]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.29	3.60	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
45.0	15	0.21	3.00	15

Travata: 1804 [180147 , 180198]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.29	3.60	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.21	3.00	15

Travata: 1815 [180165 , 180217]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.24	3.60	15

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.17	3.00	18

Travata: 1816 [180154 , 180211]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.23	3.60	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.16	3.00	19

Travata: 1817 [180168 , 180221]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.24	3.60	15

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.17	3.00	18

Travata: 1818 [180162 , 180214]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.24	3.60	15

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
45.0	15	0.17	3.00	18

Travata: 1824 [180465 , 180566]

L = 123.8cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
61.9	15	0.84	4.95	5.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
61.9	15	0.59	4.13	7.0

Travata: 1822 [180256 , 180404]

L = 230.5cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
157.6	15	0.74	9.22	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
157.6	15	0.52	7.68	15

Travata: 1829 [180287 , 180342]

L = 82.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
41.3	15	0.15	3.31	22

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
41.3	15	0.10	2.75	27

Travata: 1830 [180338 , 180355]

L = 106.8cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
58.1	15	0.31	4.27	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
58.1	15	0.22	3.56	16

Travata: 1823 [180231 , 180373]

L = 183.1cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
54.9	15	0.62	7.32	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
54.9	15	0.44	6.10	14

Travata: 1813 [180182 , 180339]

L = 219.5cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
60.4	15	1.21	8.78	7.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
60.4	15	0.86	7.32	8.6

Travata: 1825 [180376 , 180480]

L = 123.8cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
57.8	15	1.06	4.95	4.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
57.8	15	0.74	4.13	5.5

Travata: 1807 [180186 , 180328]

L = 193.8cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
51.9	15	0.63	7.75	12

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
51.9	15	0.45	6.46	15

Travata: 1808 [180173 , 180228]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.24	3.60	15

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
45.0	15	0.17	3.00	18

Travata: 1809 [180189 , 180251]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.33	3.60	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
45.0	15	0.23	3.00	13

Travata: 1810 [180141 , 180299]

L = 241.8cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.5	15	0.35	9.67	28

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
68.5	15	0.25	8.06	33

Travata: 1828 [180478 , 180404]

$L = 69.9\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
34.9	15	0.09	2.80	32

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
34.9	15	0.06	2.33	39

Travata: 1826 [180465 , 180186]

$L = 553.4\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
477.6	15	0.36	22.13	61

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
477.6	15	0.25	18.45	73

Travata: 1820 [180243 , 180370]

$L = 164.8\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
47.3	15	0.60	6.59	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
47.3	15	0.42	5.49	13

Travata: 1821 [180316 , 180433]

$L = 140.6\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
42.1	15	0.37	5.62	15

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
42.1	15	0.26	4.69	18

Travata: 1811 [180176 , 180234]

$L = 90.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.24	3.60	15

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.17	3.00	18

Travata: 1812 [180144 , 180308]

$L = 235.5\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
78.8	15	0.50	9.42	19

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
78.8	15	0.35	7.85	22

Travata: 1814 [180204 , 180258]

L = 90.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
45.0	15	0.33	3.60	11

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
45.0	15	0.23	3.00	13

Travata: 1831 [180209 , 180246]

L = 100.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
50.3	15	0.24	4.02	17

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
50.3	15	0.17	3.35	20

Travata: 1832 [180241 , 180288]

L = 92.1cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
55.3	15	0.04	3.68	87

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
55.3	15	0.03	3.07	>100

Travata: 1833 [180278 , 180366]

L = 122.4cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
77.6	15	0.10	4.90	48

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
77.6	15	0.07	4.08	58

Travata: 1834 [180509 , 180179]

L = 529.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
469.0	15	0.86	21.17	25

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
469.0	15	0.61	17.64	29

Travata: 1835 [180144 , 180185]

L = 101.9cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
51.0	15	0.12	4.08	33

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
51.0	15	0.09	3.40	40

Travata: 1836 [180185 , 180174]

L = 27.6cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
16.6	15	0.02	1.10	50

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
16.6	15	0.02	0.92	59

Travata: 1837 [180210 , 180241]

L = 116.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
58.0	15	0.49	4.64	9.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
58.0	15	0.34	3.87	11

Travata: 1838 [180184 , 180209]

L = 115.9cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
58.0	15	0.54	4.64	8.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
58.0	15	0.38	3.86	10

Travata: 1901 [190101 , 190150]

L = 125.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.5	15	1.60	5.00	3.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
62.5	15	1.13	4.17	3.7

Travata: 1902 [190097 , 190145]

$L = 125.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
62.5	15	1.66	5.00	3.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
62.5	15	1.17	4.17	3.6

Travata: 1903 [190098 , 190146]

$L = 125.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
62.5	15	1.85	5.00	2.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
62.5	15	1.30	4.17	3.2

Travata: 1904 [190099 , 190147]

$L = 125.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
62.5	15	1.85	5.00	2.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
62.5	15	1.30	4.17	3.2

Travata: 1906 [190105 , 190093]

$L = 1164.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
1095.0	15	5.13	46.56	9.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
1095.0	15	3.55	38.80	11

Travata: 1915 [190104 , 190165]

$L = 156.6\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
94.1	15	1.22	6.26	5.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
94.1	15	0.87	5.22	6.0

Travata: 1916 [190103 , 190154]

$L = 135.7\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
69.1	15	1.64	5.43	3.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
69.1	15	1.16	4.52	3.9

Travata: 1910 [190158 , 190107]

L = 445.5cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
58.0	15	0.43	17.82	41

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
58.0	15	0.31	14.85	48

Travata: 1917 [190095 , 190168]

L = 160.8cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
102.5	15	1.08	6.43	5.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
102.5	15	0.77	5.36	6.9

Travata: 1918 [190096 , 190162]

L = 138.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
72.1	15	1.69	5.55	3.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
72.1	15	1.20	4.62	3.9

Travata: 1911 [190109 , 190164]

L = 443.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
385.2	15	0.41	17.73	43

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
385.2	15	0.29	14.77	51

Travata: 1907 [190110 , 190189]

L = 199.1cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
70.4	15	-2.97	7.96	2.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
70.4	15	-2.06	6.64	3.2

Travata: 1908 [190141 , 190224]

L = 151.8cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
101.8	15	0.34	6.07	18

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
101.8	15	0.24	5.06	21

Travata: 1909 [190105 , 190173]

L = 183.4cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
55.5	15	-1.82	7.34	4.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
55.5	15	-1.26	6.11	4.9

Travata: 1919 [190106 , 190141]

L = 163.5cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
88.3	15	0.26	6.54	25

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
88.3	15	0.18	5.45	30

Travata: 1912 [190094 , 190176]

L = 187.9cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
59.8	15	-2.03	7.52	3.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
59.8	15	-1.40	6.26	4.5

Travata: 1913 [190144 , 190232]

L = 145.5cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
91.3	15	0.44	5.82	13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
91.3	15	0.31	4.85	15

Travata: 1914 [190116 , 190204]

L = 192.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
63.7	15	-2.40	7.68	3.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
63.7	15	-1.66	6.40	3.8

Travata: 1921 [190179 , 190184]

L = 1410.4cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
702.0	15	1.46	56.42	39

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
702.0	15	1.03	47.01	46

Travata: 1922 [190191 , 190210]

L = 1380.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
687.1	15	1.34	55.21	41

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
687.1	15	0.95	46.01	49

Travata: 1923 [190112 , 190127]

L = 116.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
58.1	15	0.53	4.65	8.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
58.1	15	0.37	3.87	10

Travata: 1924 [190126 , 190111]

L = 116.2cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
58.1	15	0.51	4.65	9.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
58.1	15	0.36	3.87	11

Verifica spostamenti laterali delle colonne in acciaio secondo NTC 2008

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Verifica spostamenti orizzontali relativi di piano (§4.2.4.2.2 - NTC 2008)

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup. mm	SpostY sup. mm	SpostX inf. mm	SpostY inf. mm	δ	h/300.00	Verifica
0-1	10009	9	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10039	39	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10049	49	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10079	79	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10010	10	14	-0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10040	40	14	-0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10050	50	14	-0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10080	80	14	-0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10011	11	14	0.01	0.00	0.00	0.00	0.01	0.40	Si
0-1	10021	21	14	0.01	0.00	0.00	0.00	0.01	0.40	Si
0-1	10031	31	14	0.01	-0.00	0.00	0.00	0.01	0.40	Si
0-1	10041	41	14	0.01	-0.00	0.00	0.00	0.01	0.40	Si
0-1	10051	51	14	0.01	-0.00	0.00	0.00	0.01	0.40	Si
0-1	10061	61	14	0.01	0.00	0.00	0.00	0.01	0.40	Si
0-1	10071	71	14	0.01	-0.00	0.00	0.00	0.01	0.40	Si
0-1	10081	81	14	0.01	0.00	0.00	0.00	0.01	0.40	Si
0-1	10008	8	14	-0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10018	18	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10028	28	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10038	38	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10048	48	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10058	58	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10068	68	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10078	78	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10007	7	14	0.01	0.00	0.00	0.00	0.01	0.40	Si
0-1	10017	17	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10027	27	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10037	37	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10047	47	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10057	57	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10067	67	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10077	77	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10006	6	14	-0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10036	36	14	-0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10046	46	14	-0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10076	76	14	-0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10005	5	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10035	35	14	0.00	-0.00	0.00	0.00	0.00	0.40	Si
0-1	10045	45	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10075	75	14	0.00	0.00	0.00	0.00	0.00	0.40	Si
0-1	10004	4	14	-0.01	0.00	0.00	0.00	0.01	0.40	Si
0-1	10014	14	14	-0.01	0.00	0.00	0.00	0.01	0.40	Si
0-1	10024	24	14	-0.01	-0.00	0.00	0.00	0.01	0.40	Si
0-1	10034	34	14	-0.01	-0.00	0.00	0.00	0.01	0.40	Si
0-1	10044	44	14	-0.01	-0.00	0.00	0.00	0.01	0.40	Si
0-1	10054	54	14	-0.01	0.00	0.00	0.00	0.01	0.40	Si
0-1	10064	64	14	-0.01	-0.00	0.00	0.00	0.01	0.40	Si
0-1	10074	74	14	-0.01	0.00	0.00	0.00	0.01	0.40	Si
1-4	40009	10009	14	0.06	0.08	0.00	0.00	0.09	3.33	Si
1-4	40039	10039	14	0.06	-0.06	0.00	-0.00	0.09	3.33	Si
1-4	40049	10049	14	0.06	0.06	0.00	-0.00	0.08	3.33	Si
1-4	40079	10079	14	0.06	-0.05	0.00	0.00	0.08	3.33	Si
1-4	40010	10010	14	-0.04	0.08	-0.00	0.00	0.09	3.33	Si
1-4	40040	10040	14	-0.04	-0.06	-0.00	-0.00	0.07	3.33	Si
1-4	40050	10050	14	-0.04	0.06	-0.00	0.00	0.07	3.33	Si
1-4	40080	10080	14	-0.04	-0.05	-0.00	0.00	0.07	3.33	Si
1-4	40011	10011	14	-0.04	0.07	0.01	0.00	0.09	3.33	Si
1-4	40041	10041	14	-0.04	-0.06	0.01	-0.00	0.08	3.33	Si
1-4	40051	10051	14	-0.04	0.05	0.01	-0.00	0.07	3.33	Si
1-4	40081	10081	14	-0.04	-0.05	0.01	0.00	0.07	3.33	Si
1-4	40008	10008	14	0.06	0.08	-0.00	0.00	0.10	3.33	Si
1-4	40038	10038	14	0.06	-0.06	0.00	-0.00	0.09	3.33	Si
1-4	40048	10048	14	0.06	0.06	0.00	-0.00	0.08	3.33	Si
1-4	40078	10078	14	0.06	-0.05	0.00	0.00	0.08	3.33	Si
1-4	40007	10007	14	-0.05	0.08	0.01	0.00	0.10	3.33	Si
1-4	40037	10037	14	-0.06	-0.06	0.00	-0.00	0.08	3.33	Si
1-4	40047	10047	14	-0.06	0.06	0.00	-0.00	0.08	3.33	Si
1-4	40077	10077	14	-0.05	-0.05	0.00	0.00	0.08	3.33	Si
1-4	40006	10006	14	-0.05	0.08	-0.00	0.00	0.09	3.33	Si
1-4	40036	10036	14	-0.06	-0.06	-0.00	-0.00	0.08	3.33	Si
1-4	40046	10046	14	-0.06	0.06	-0.00	-0.00	0.08	3.33	Si
1-4	40076	10076	14	-0.05	-0.05	-0.00	0.00	0.07	3.33	Si
1-4	40005	10005	14	0.03	0.08	0.00	0.00	0.08	3.33	Si
1-4	40035	10035	14	0.04	-0.06	0.00	-0.00	0.07	3.33	Si
1-4	40045	10045	14	0.04	0.06	0.00	0.00	0.07	3.33	Si

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Interp.	Nodo sup.	Nodo inf.	Comb.	SpостX sup.	SpостY sup.	SpостX inf.	SpостY inf.	δ	h/300.00	Verifica
1-4	40075	10075	14	0.03	-0.05	0.00	0.00	0.06	3.33	Si
1-4	40004	10004	14	0.03	0.06	-0.01	0.00	0.07	3.33	Si
1-4	40034	10034	14	0.04	-0.05	-0.01	-0.00	0.06	3.33	Si
1-4	40044	10044	14	0.04	0.04	-0.01	-0.00	0.06	3.33	Si
1-4	40074	10074	14	0.03	-0.04	-0.01	0.00	0.06	3.33	Si
1-4	40021	10021	14	-0.04	0.06	0.01	0.00	0.08	3.33	Si
1-4	40031	10031	14	-0.04	-0.06	0.01	-0.00	0.08	3.33	Si
1-4	40061	10061	14	-0.04	0.05	0.01	0.00	0.07	3.33	Si
1-4	40071	10071	14	-0.04	-0.05	0.01	-0.00	0.07	3.33	Si
1-4	40018	10018	14	0.06	0.07	0.00	0.00	0.09	3.33	Si
1-4	40028	10028	14	0.06	-0.06	0.00	-0.00	0.09	3.33	Si
1-4	40058	10058	14	0.06	0.06	0.00	0.00	0.08	3.33	Si
1-4	40068	10068	14	0.06	-0.05	0.00	-0.00	0.08	3.33	Si
1-4	40027	10027	14	-0.06	-0.06	0.00	-0.00	0.08	3.33	Si
1-4	40017	10017	14	-0.06	0.07	0.00	0.00	0.09	3.33	Si
1-4	40057	10057	14	-0.06	0.06	0.00	0.00	0.08	3.33	Si
1-4	40067	10067	14	-0.06	-0.05	0.00	-0.00	0.08	3.33	Si
1-4	40014	10014	14	0.04	0.05	-0.01	0.00	0.07	3.33	Si
1-4	40024	10024	14	0.04	-0.05	-0.01	-0.00	0.06	3.33	Si
1-4	40054	10054	14	0.04	0.04	-0.01	0.00	0.06	3.33	Si
1-4	40064	10064	14	0.04	-0.04	-0.01	-0.00	0.06	3.33	Si
0-4	40019	19	14	0.06	0.07	0.00	0.00	0.09	3.73	Si
0-4	40029	29	14	0.06	-0.06	0.00	0.00	0.09	3.73	Si
0-4	40059	59	14	0.06	0.06	0.00	0.00	0.09	3.73	Si
0-4	40069	69	14	0.06	-0.05	0.00	0.00	0.08	3.73	Si
0-4	40020	20	14	-0.04	0.07	0.00	0.00	0.08	3.73	Si
0-4	40030	30	14	-0.04	-0.06	0.00	0.00	0.08	3.73	Si
0-4	40060	60	14	-0.04	0.06	0.00	0.00	0.07	3.73	Si
0-4	40070	70	14	-0.04	-0.05	0.00	0.00	0.07	3.73	Si
0-4	40016	16	14	-0.06	0.07	0.00	0.00	0.09	3.73	Si
0-4	40026	26	14	-0.06	-0.06	0.00	0.00	0.08	3.73	Si
0-4	40056	56	14	-0.06	0.06	0.00	0.00	0.08	3.73	Si
0-4	40066	66	14	-0.06	-0.05	0.00	0.00	0.08	3.73	Si
0-4	40015	15	14	0.04	0.07	0.00	0.00	0.08	3.73	Si
0-4	40025	25	14	0.04	-0.06	0.00	0.00	0.07	3.73	Si
0-4	40055	55	14	0.04	0.06	0.00	0.00	0.07	3.73	Si
0-4	40065	65	14	0.04	-0.05	0.00	0.00	0.06	3.73	Si
5-6	60457	50457	14	0.01	-0.01	0.00	0.00	0.02	0.47	Si
5-6	60453	50453	14	0.00	-0.01	0.00	0.00	0.01	0.47	Si
5-6	60449	50449	14	-0.00	-0.01	0.00	0.00	0.01	0.47	Si
5-6	60445	50445	14	-0.01	-0.01	0.00	0.00	0.02	0.47	Si
5-6	60466	50466	14	-0.00	-0.00	0.00	0.00	0.00	0.47	Si
5-6	60486	50486	14	0.00	-0.00	0.00	0.00	0.00	0.47	Si
5-6	60470	50470	14	0.00	-0.00	0.00	0.00	0.00	0.47	Si
5-6	60503	50503	14	-0.00	-0.00	0.00	0.00	0.00	0.47	Si
5-6	60622	50622	14	0.00	0.00	0.00	0.00	0.00	0.47	Si
5-6	60676	50676	14	0.01	-0.01	0.00	0.00	0.01	0.47	Si
5-6	60626	50626	14	-0.00	-0.00	0.00	0.00	0.00	0.47	Si
5-6	60603	50603	14	0.01	-0.01	0.00	0.00	0.02	0.47	Si
5-6	60570	50570	14	0.00	-0.01	0.00	0.00	0.01	0.47	Si
5-6	60527	50527	14	0.00	-0.01	0.00	0.00	0.01	0.47	Si
5-6	60490	50490	14	-0.00	-0.01	0.00	0.00	0.02	0.47	Si
5-6	60682	50682	14	-0.01	-0.01	0.00	0.00	0.02	0.47	Si
5-6	60668	50668	14	0.01	0.00	0.00	0.00	0.01	0.47	Si
5-6	60672	50672	14	-0.01	0.00	0.00	0.00	0.01	0.47	Si
5-6	60540	50540	14	-0.00	-0.01	0.00	0.00	0.01	0.47	Si
5-6	60580	50580	14	-0.00	-0.01	0.00	0.00	0.01	0.47	Si
5-6	60612	50612	14	-0.01	-0.01	0.00	0.00	0.02	0.47	Si
5-6	60499	50499	14	0.00	-0.01	0.00	0.00	0.02	0.47	Si
0-7	70002	2	14	-0.00	0.12	0.00	0.00	0.12	5.17	Si
0-7	70001	1	14	0.00	0.10	0.00	0.00	0.10	5.17	Si
0-7	70012	12	14	0.00	0.12	0.00	0.00	0.12	5.17	Si
0-7	70003	3	14	0.00	0.11	0.00	0.00	0.11	5.17	Si
4-7	70009	40009	14	0.00	0.03	0.06	0.08	0.07	1.43	Si
4-7	70010	40010	14	0.00	0.03	-0.04	0.08	0.06	1.43	Si
4-7	70011	40011	14	-0.00	0.08	-0.04	0.07	0.04	1.43	Si
4-7	70008	40008	14	0.00	0.03	0.06	0.08	0.08	1.43	Si
4-7	70007	40007	14	0.00	0.03	-0.05	0.08	0.07	1.43	Si
4-7	70006	40006	14	0.00	0.02	-0.05	0.08	0.08	1.43	Si
4-7	70005	40005	14	0.00	0.04	0.03	0.08	0.05	1.43	Si
4-7	70004	40004	14	0.00	0.09	0.03	0.06	0.04	1.43	Si
2-7	70779	20779	14	-0.00	0.03	0.01	0.01	0.02	2.50	Si
2-7	70776	20776	14	-0.00	0.03	0.00	0.02	0.01	2.50	Si
2-7	70773	20773	14	0.00	0.03	-0.01	0.02	0.01	2.50	Si
2-7	70770	20770	14	0.00	0.04	-0.01	0.01	0.02	2.50	Si
2-7	70834	20834	14	0.01	0.04	0.01	0.02	0.02	2.50	Si
2-7	70832	20832	14	0.00	0.03	-0.00	0.03	0.00	2.50	Si
2-7	70830	20830	14	0.00	0.03	0.00	0.03	0.00	2.50	Si

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2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup.	SpostY sup.	SpostX inf.	SpostY inf.	δ	h/300.00	Verifica
2-7	70828	20828	14	-0.01	0.04	-0.01	0.02	0.02	2.50	Si
2-7	70782	20782	14	-0.00	0.04	-0.00	-0.01	0.04	2.50	Si
2-7	70844	20844	14	-0.02	0.11	0.02	0.04	0.08	2.50	Si
2-7	70821	20821	14	-0.02	0.08	0.02	0.01	0.08	2.50	Si
2-7	70802	20802	14	0.01	0.03	0.02	-0.05	0.08	2.50	Si
2-7	70790	20790	14	0.00	0.04	0.00	-0.01	0.05	2.50	Si
2-7	70809	20809	14	-0.01	0.03	-0.02	-0.05	0.08	2.50	Si
2-7	70825	20825	14	0.01	0.07	-0.02	0.00	0.08	2.50	Si
2-7	70847	20847	14	0.02	0.10	-0.02	0.03	0.07	2.50	Si
2-7	70863	20863	14	0.02	0.12	0.03	-0.11	0.23	2.50	Si
2-7	70862	20862	14	0.01	0.09	0.02	-0.27	0.36	2.50	Si
2-7	70861	20861	14	0.01	0.03	0.01	-0.31	0.34	2.50	Si
2-7	70860	20860	14	0.01	0.04	0.01	-0.33	0.36	2.50	Si
2-7	70859	20859	14	0.00	0.03	-0.00	-0.35	0.38	2.50	Si
2-7	70858	20858	14	0.00	0.04	0.01	-0.36	0.39	2.50	Si
2-7	70857	20857	14	-0.00	0.03	0.00	-0.33	0.35	2.50	Si
2-7	70856	20856	14	-0.00	0.04	-0.02	-0.36	0.40	2.50	Si
2-7	70855	20855	14	-0.01	0.09	-0.03	-0.22	0.32	2.50	Si
2-7	70854	20854	14	-0.01	0.11	-0.03	-0.12	0.23	2.50	Si
7-8	80274	70274	14	0.01	-0.00	0.00	0.00	0.01	0.43	Si
7-8	80270	70270	14	0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80266	70266	14	0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80262	70262	14	-0.01	-0.00	0.00	0.00	0.01	0.43	Si
7-8	80290	70290	14	0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80279	70279	14	-0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80283	70283	14	0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80294	70294	14	-0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80553	70553	14	0.00	-0.00	0.00	0.00	0.00	0.43	Si
7-8	80418	70418	14	0.01	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80384	70384	14	0.01	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80333	70333	14	0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80303	70303	14	-0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80461	70461	14	0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80518	70518	14	0.01	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80532	70532	14	-0.01	-0.01	0.00	0.00	0.02	0.43	Si
7-8	80474	70474	14	-0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80346	70346	14	-0.00	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80396	70396	14	-0.01	-0.01	0.00	0.00	0.01	0.43	Si
7-8	80429	70429	14	-0.01	-0.00	0.00	0.00	0.01	0.43	Si
7-8	80312	70312	14	0.00	-0.01	0.00	0.00	0.01	0.43	Si
3-9	90713	30713	14	-0.00	0.02	0.01	0.01	0.02	2.33	Si
3-9	90710	30710	14	-0.00	0.02	0.01	0.00	0.02	2.33	Si
3-9	90707	30707	14	-0.00	0.02	-0.01	0.00	0.02	2.33	Si
3-9	90704	30704	14	-0.01	0.03	-0.01	0.01	0.02	2.33	Si
3-9	90798	30798	14	-0.00	0.04	0.01	0.02	0.03	2.33	Si
3-9	90765	30765	14	-0.00	0.03	0.01	0.01	0.02	2.33	Si
3-9	90746	30746	14	-0.01	0.05	-0.00	0.01	0.04	2.33	Si
3-9	90722	30722	14	-0.00	0.02	-0.01	0.00	0.02	2.33	Si
3-9	90816	30816	14	-0.00	0.04	-0.01	0.01	0.04	2.33	Si
3-9	90817	30817	14	-0.00	0.04	0.01	0.00	0.04	2.33	Si
3-9	90754	30754	14	0.01	0.05	0.00	0.01	0.04	2.33	Si
3-9	90731	30731	14	-0.00	0.02	0.01	0.00	0.03	2.33	Si
3-9	90786	30786	14	0.00	0.04	-0.01	0.01	0.03	2.33	Si
3-9	90805	30805	14	-0.00	0.04	-0.02	0.02	0.03	2.33	Si
7-9	90779	70779	14	0.00	0.02	-0.00	0.03	0.01	0.50	Si
7-9	90776	70776	14	0.00	0.02	-0.00	0.03	0.01	0.50	Si
7-9	90773	70773	14	-0.00	0.02	0.00	0.03	0.01	0.50	Si
7-9	90770	70770	14	-0.00	0.02	0.00	0.04	0.01	0.50	Si
7-9	90782	70782	14	0.00	0.02	-0.00	0.04	0.01	0.50	Si
7-9	90894	70894	14	-0.04	0.07	-0.02	0.11	0.04	0.50	Si
7-9	90895	70895	14	0.02	0.05	0.01	0.10	0.04	0.50	Si
7-9	90850	70850	14	-0.00	0.04	-0.02	0.11	0.07	0.50	Si
7-9	90844	70844	14	-0.00	0.04	-0.02	0.11	0.07	0.50	Si
7-9	90821	70821	14	0.00	0.03	-0.02	0.08	0.05	0.50	Si
7-9	90802	70802	14	-0.01	0.05	0.01	0.03	0.03	0.50	Si
7-9	90851	70851	14	-0.00	0.04	0.02	0.10	0.06	0.50	Si
7-9	90790	70790	14	-0.00	0.02	0.00	0.04	0.02	0.50	Si
7-9	90809	70809	14	0.01	0.06	-0.01	0.03	0.03	0.50	Si
7-9	90825	70825	14	0.00	0.04	0.01	0.07	0.04	0.50	Si
7-9	90847	70847	14	-0.00	0.04	0.02	0.10	0.06	0.50	Si
3-10	100644	30644	14	0.00	0.01	0.01	-0.00	0.01	2.83	Si
3-10	100641	30641	14	-0.00	0.01	-0.00	-0.01	0.02	2.83	Si
3-10	100638	30638	14	0.00	0.01	0.00	-0.01	0.02	2.83	Si
3-10	100635	30635	14	-0.00	0.01	-0.01	-0.00	0.01	2.83	Si
3-10	100738	30738	14	0.01	0.02	0.01	0.00	0.01	2.83	Si
3-10	100718	30718	14	-0.00	0.01	0.00	-0.00	0.02	2.83	Si
3-10	100687	30687	14	-0.00	0.02	0.00	-0.00	0.02	2.83	Si
3-10	100653	30653	14	-0.00	0.01	-0.00	-0.00	0.01	2.83	Si

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup.	SpostY sup.	SpostX inf.	SpostY inf.	δ	h/300.00	Verifica
3-10	100762	30762	14	0.01	0.02	-0.00	0.00	0.02	2.83	Si
3-10	100764	30764	14	-0.00	0.02	0.00	-0.00	0.02	2.83	Si
3-10	100695	30695	14	0.00	0.02	-0.00	0.00	0.02	2.83	Si
3-10	100662	30662	14	0.00	0.01	0.00	-0.00	0.01	2.83	Si
3-10	100726	30726	14	0.00	0.02	-0.00	-0.00	0.02	2.83	Si
3-10	100750	30750	14	-0.01	0.02	-0.01	0.00	0.01	2.83	Si
9-10	100713	90713	14	0.00	0.01	-0.00	0.02	0.01	0.50	Si
9-10	100710	90710	14	-0.00	0.02	-0.00	0.02	0.01	0.50	Si
9-10	100707	90707	14	0.00	0.01	-0.00	0.02	0.01	0.50	Si
9-10	100704	90704	14	0.00	0.01	-0.01	0.03	0.01	0.50	Si
9-10	100852	90852	14	-0.05	0.06	-0.03	0.08	0.03	0.50	Si
9-10	100853	90853	14	0.03	0.04	0.01	0.06	0.03	0.50	Si
9-10	100816	90816	14	0.01	0.02	-0.00	0.04	0.03	0.50	Si
9-10	100798	90798	14	0.00	0.02	-0.00	0.04	0.02	0.50	Si
9-10	100765	90765	14	-0.00	0.02	-0.00	0.03	0.01	0.50	Si
9-10	100746	90746	14	0.00	0.03	-0.01	0.05	0.03	0.50	Si
9-10	100722	90722	14	0.01	0.01	-0.00	0.02	0.01	0.50	Si
9-10	100817	90817	14	0.00	0.02	-0.00	0.04	0.02	0.50	Si
9-10	100731	90731	14	-0.00	0.01	-0.00	0.02	0.01	0.50	Si
9-10	100754	90754	14	0.00	0.03	0.01	0.05	0.03	0.50	Si
9-10	100786	90786	14	0.00	0.02	0.00	0.04	0.02	0.50	Si
9-10	100805	90805	14	0.00	0.02	-0.00	0.04	0.02	0.50	Si
6-11	110563	60563	14	0.00	0.01	0.01	-0.01	0.02	2.17	Si
6-11	110560	60560	14	0.00	0.01	-0.00	-0.00	0.01	2.17	Si
6-11	110557	60557	14	-0.00	0.01	0.00	-0.00	0.01	2.17	Si
6-11	110554	60554	14	-0.00	0.01	-0.01	-0.01	0.02	2.17	Si
6-11	110683	60683	14	0.01	0.02	0.01	-0.00	0.02	2.17	Si
6-11	110649	60649	14	0.00	0.02	0.00	0.00	0.02	2.17	Si
6-11	110608	60608	14	0.00	0.02	0.01	0.00	0.02	2.17	Si
6-11	110576	60576	14	0.00	0.01	0.00	-0.01	0.02	2.17	Si
6-11	110734	60734	14	0.00	0.03	0.01	-0.00	0.03	2.17	Si
6-11	110735	60735	14	-0.00	0.03	-0.01	-0.00	0.03	2.17	Si
6-11	110617	60617	14	-0.00	0.02	-0.01	0.00	0.02	2.17	Si
6-11	110585	60585	14	-0.00	0.01	-0.00	-0.01	0.02	2.17	Si
6-11	110658	60658	14	-0.00	0.02	-0.00	-0.00	0.02	2.17	Si
6-11	110691	60691	14	-0.01	0.02	-0.01	-0.00	0.02	2.17	Si
10-11	110644	100644	14	-0.00	0.01	0.00	0.01	0.00	0.50	Si
10-11	110641	100641	14	-0.00	0.01	-0.00	0.01	0.00	0.50	Si
10-11	110638	100638	14	0.00	0.01	0.00	0.01	0.00	0.50	Si
10-11	110635	100635	14	0.00	0.01	-0.00	0.01	0.00	0.50	Si
10-11	110818	100818	14	-0.06	0.06	-0.04	0.07	0.03	0.50	Si
10-11	110819	100819	14	0.03	0.03	0.02	0.05	0.03	0.50	Si
10-11	110762	100762	14	-0.01	0.01	0.01	0.02	0.02	0.50	Si
10-11	110738	100738	14	-0.00	0.01	0.01	0.02	0.01	0.50	Si
10-11	110718	100718	14	-0.00	0.01	-0.00	0.01	0.00	0.50	Si
10-11	110687	100687	14	-0.00	0.02	-0.00	0.02	0.00	0.50	Si
10-11	110653	100653	14	0.00	0.01	-0.00	0.01	0.00	0.50	Si
10-11	110764	100764	14	0.01	0.01	-0.00	0.02	0.01	0.50	Si
10-11	110750	100750	14	0.01	0.01	-0.01	0.02	0.01	0.50	Si
10-11	110662	100662	14	-0.00	0.01	0.00	0.01	0.00	0.50	Si
10-11	110695	100695	14	0.00	0.02	0.00	0.02	0.00	0.50	Si
10-11	110726	100726	14	0.00	0.01	0.00	0.02	0.00	0.50	Si
7-12	120009	70009	14	0.00	-0.01	0.00	0.03	0.04	1.90	Si
7-12	120010	70010	14	0.00	-0.01	0.00	0.03	0.04	1.90	Si
7-12	120011	70011	14	0.01	-0.01	-0.00	0.08	0.10	1.90	Si
7-12	120012	70012	14	0.01	-0.07	0.00	0.12	0.20	1.90	Si
7-12	120008	70008	14	0.00	-0.01	0.00	0.03	0.04	1.90	Si
7-12	120007	70007	14	0.01	-0.01	0.00	0.03	0.05	1.90	Si
7-12	120006	70006	14	0.01	-0.01	0.00	0.02	0.03	1.90	Si
7-12	120005	70005	14	0.01	-0.01	0.00	0.04	0.05	1.90	Si
7-12	120004	70004	14	0.01	-0.01	0.00	0.09	0.10	1.90	Si
7-12	120003	70003	14	0.00	-0.02	0.00	0.11	0.13	1.90	Si
4-12	120019	40019	14	0.01	-0.00	0.06	0.07	0.09	3.33	Si
4-12	120029	40029	14	0.00	-0.00	0.06	-0.06	0.08	3.33	Si
4-12	120039	40039	14	0.01	-0.00	0.06	-0.06	0.08	3.33	Si
4-12	120049	40049	14	0.01	-0.00	0.06	0.06	0.09	3.33	Si
4-12	120059	40059	14	0.00	-0.01	0.06	0.06	0.09	3.33	Si
4-12	120069	40069	14	0.00	-0.00	0.06	-0.05	0.07	3.33	Si
4-12	120079	40079	14	0.01	0.00	0.06	-0.05	0.08	3.33	Si
4-12	120020	40020	14	0.01	-0.00	-0.04	0.07	0.09	3.33	Si
4-12	120030	40030	14	0.01	-0.00	-0.04	-0.06	0.08	3.33	Si
4-12	120040	40040	14	0.01	-0.00	-0.04	-0.06	0.08	3.33	Si
4-12	120050	40050	14	0.01	-0.00	-0.04	0.06	0.08	3.33	Si
4-12	120060	40060	14	0.01	-0.01	-0.04	0.06	0.08	3.33	Si
4-12	120070	40070	14	0.01	-0.00	-0.04	-0.05	0.07	3.33	Si
4-12	120080	40080	14	0.01	0.01	-0.04	-0.05	0.07	3.33	Si
4-12	120021	40021	14	0.01	-0.01	-0.04	0.06	0.09	3.33	Si
4-12	120031	40031	14	0.01	-0.01	-0.04	-0.06	0.08	3.33	Si

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup.	SpostY sup.	SpostX inf.	SpostY inf.	δ	h/300.00	Verifica
4-12	120041	40041	14	0.01	-0.01	-0.04	-0.06	0.08	3.33	Si
4-12	120051	40051	14	0.01	-0.01	-0.04	0.05	0.08	3.33	Si
4-12	120061	40061	14	0.01	-0.01	-0.04	0.05	0.08	3.33	Si
4-12	120071	40071	14	0.01	-0.01	-0.04	-0.05	0.07	3.33	Si
4-12	120081	40081	14	0.01	-0.00	-0.04	-0.05	0.07	3.33	Si
4-12	120018	40018	14	0.01	-0.01	0.06	0.07	0.09	3.33	Si
4-12	120028	40028	14	0.01	-0.01	0.06	-0.06	0.08	3.33	Si
4-12	120038	40038	14	0.01	-0.01	0.06	-0.06	0.08	3.33	Si
4-12	120048	40048	14	0.01	-0.01	0.06	0.06	0.08	3.33	Si
4-12	120058	40058	14	0.01	-0.01	0.06	0.06	0.09	3.33	Si
4-12	120068	40068	14	0.01	-0.01	0.06	-0.05	0.07	3.33	Si
4-12	120078	40078	14	0.01	0.00	0.06	-0.05	0.08	3.33	Si
4-12	120017	40017	14	0.01	-0.01	-0.06	0.07	0.10	3.33	Si
4-12	120027	40027	14	0.01	-0.01	-0.06	-0.06	0.09	3.33	Si
4-12	120037	40037	14	0.01	-0.01	-0.06	-0.06	0.09	3.33	Si
4-12	120047	40047	14	0.01	-0.01	-0.06	0.06	0.09	3.33	Si
4-12	120057	40057	14	0.01	-0.01	-0.06	0.06	0.09	3.33	Si
4-12	120067	40067	14	0.01	-0.01	-0.06	-0.05	0.08	3.33	Si
4-12	120077	40077	14	0.01	0.00	-0.05	-0.05	0.08	3.33	Si
4-12	120016	40016	14	0.01	-0.00	-0.06	0.07	0.10	3.33	Si
4-12	120026	40026	14	0.01	-0.00	-0.06	-0.06	0.09	3.33	Si
4-12	120036	40036	14	0.01	-0.00	-0.06	-0.06	0.09	3.33	Si
4-12	120046	40046	14	0.01	-0.00	-0.06	0.06	0.09	3.33	Si
4-12	120056	40056	14	0.01	-0.01	-0.06	0.06	0.09	3.33	Si
4-12	120066	40066	14	0.01	-0.00	-0.06	-0.05	0.08	3.33	Si
4-12	120076	40076	14	0.01	0.00	-0.05	-0.05	0.08	3.33	Si
4-12	120015	40015	14	0.01	-0.00	0.04	0.07	0.08	3.33	Si
4-12	120025	40025	14	0.01	-0.00	0.04	-0.06	0.06	3.33	Si
4-12	120035	40035	14	0.01	-0.00	0.04	-0.06	0.06	3.33	Si
4-12	120045	40045	14	0.01	-0.00	0.04	0.06	0.07	3.33	Si
4-12	120055	40055	14	0.01	-0.00	0.04	0.06	0.07	3.33	Si
4-12	120065	40065	14	0.01	-0.00	0.04	-0.05	0.05	3.33	Si
4-12	120075	40075	14	0.01	0.01	0.03	-0.05	0.06	3.33	Si
4-12	120014	40014	14	0.00	-0.01	0.04	0.05	0.06	3.33	Si
4-12	120024	40024	14	0.00	-0.01	0.04	-0.05	0.05	3.33	Si
4-12	120034	40034	14	0.00	-0.01	0.04	-0.05	0.05	3.33	Si
4-12	120044	40044	14	0.00	-0.01	0.04	0.04	0.06	3.33	Si
4-12	120054	40054	14	0.00	-0.01	0.04	0.04	0.06	3.33	Si
4-12	120064	40064	14	0.00	-0.01	0.04	-0.04	0.05	3.33	Si
4-12	120074	40074	14	0.00	-0.00	0.03	-0.04	0.05	3.33	Si
0-12	120089	89	14	0.01	0.01	0.00	0.00	0.02	7.07	Si
0-12	120090	90	14	0.01	0.01	0.00	0.00	0.02	7.07	Si
0-12	120091	91	14	0.02	0.01	0.00	0.00	0.02	7.07	Si
0-12	120092	92	14	0.02	-0.06	0.00	0.00	0.06	7.07	Si
0-12	120088	88	14	0.01	0.01	0.00	0.00	0.02	7.07	Si
0-12	120087	87	14	0.01	0.01	0.00	0.00	0.02	7.07	Si
0-12	120086	86	14	0.01	0.01	0.00	0.00	0.02	7.07	Si
0-12	120085	85	14	0.01	0.01	0.00	0.00	0.02	7.07	Si
0-12	120084	84	14	0.01	0.01	0.00	0.00	0.01	7.07	Si
0-12	120083	83	14	0.01	-0.01	0.00	0.00	0.01	7.07	Si
0-12	120022	22	14	0.02	-0.07	0.00	0.00	0.07	7.07	Si
0-12	120032	32	14	0.02	-0.07	0.00	0.00	0.07	7.07	Si
0-12	120042	42	14	0.02	-0.07	0.00	0.00	0.07	7.07	Si
0-12	120052	52	14	0.02	-0.07	0.00	0.00	0.07	7.07	Si
0-12	120062	62	14	0.02	-0.07	0.00	0.00	0.07	7.07	Si
0-12	120072	72	14	0.02	-0.07	0.00	0.00	0.07	7.07	Si
0-12	120082	82	14	0.02	-0.06	0.00	0.00	0.06	7.07	Si
0-12	120013	13	14	-0.00	-0.02	0.00	0.00	0.02	7.07	Si
0-12	120023	23	14	-0.00	-0.02	0.00	0.00	0.02	7.07	Si
0-12	120033	33	14	-0.00	-0.02	0.00	0.00	0.02	7.07	Si
0-12	120043	43	14	-0.00	-0.02	0.00	0.00	0.02	7.07	Si
0-12	120053	53	14	-0.00	-0.02	0.00	0.00	0.02	7.07	Si
0-12	120063	63	14	-0.00	-0.01	0.00	0.00	0.01	7.07	Si
0-12	120073	73	14	-0.00	-0.01	0.00	0.00	0.01	7.07	Si
6-13	130457	60457	14	0.00	0.01	0.01	-0.01	0.02	2.67	Si
6-13	130453	60453	14	-0.00	0.00	0.00	-0.01	0.02	2.67	Si
6-13	130449	60449	14	0.00	0.00	-0.00	-0.01	0.02	2.67	Si
6-13	130445	60445	14	-0.00	0.00	-0.01	-0.01	0.02	2.67	Si
6-13	130466	60466	14	-0.00	0.02	-0.00	-0.00	0.02	2.67	Si
6-13	130486	60486	14	-0.00	0.02	0.00	-0.00	0.02	2.67	Si
6-13	130470	60470	14	0.01	0.03	0.00	-0.00	0.03	2.67	Si
6-13	130503	60503	14	0.00	0.02	-0.00	-0.00	0.02	2.67	Si
6-13	130622	60622	14	-0.01	0.02	0.00	0.00	0.02	2.67	Si
6-13	130676	60676	14	0.01	0.00	0.01	-0.01	0.01	2.67	Si
6-13	130626	60626	14	0.01	0.02	-0.00	-0.00	0.03	2.67	Si
6-13	130603	60603	14	0.00	0.00	0.01	-0.01	0.02	2.67	Si
6-13	130570	60570	14	-0.00	0.00	0.00	-0.01	0.01	2.67	Si
6-13	130527	60527	14	0.00	0.01	0.00	-0.01	0.02	2.67	Si

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup.	SpostY sup.	SpostX inf.	SpostY inf.	δ	h/300.00	Verifica
6-13	130490	60490	14	-0.00	0.00	-0.00	-0.01	0.02	2.67	Si
6-13	130668	60668	14	-0.00	0.03	0.01	0.00	0.03	2.67	Si
6-13	130672	60672	14	0.01	0.04	-0.01	0.00	0.04	2.67	Si
6-13	130682	60682	14	-0.00	0.01	-0.01	-0.01	0.03	2.67	Si
6-13	130540	60540	14	0.00	0.01	-0.00	-0.01	0.02	2.67	Si
6-13	130499	60499	14	0.00	0.00	0.00	-0.01	0.02	2.67	Si
6-13	130580	60580	14	0.00	0.00	-0.00	-0.01	0.01	2.67	Si
6-13	130612	60612	14	-0.00	0.00	-0.01	-0.01	0.02	2.67	Si
11-13	130563	110563	14	0.00	0.01	0.00	0.01	0.00	0.50	Si
11-13	130560	110560	14	-0.00	0.01	0.00	0.01	0.00	0.50	Si
11-13	130557	110557	14	0.00	0.01	-0.00	0.01	0.00	0.50	Si
11-13	130554	110554	14	-0.00	0.01	-0.00	0.01	0.00	0.50	Si
11-13	130769	110769	14	-0.06	0.06	-0.04	0.08	0.03	0.50	Si
11-13	130793	110793	14	0.03	0.03	0.01	0.05	0.03	0.50	Si
11-13	130734	110734	14	0.01	0.00	0.00	0.03	0.03	0.50	Si
11-13	130683	110683	14	0.01	0.01	0.01	0.02	0.01	0.50	Si
11-13	130649	110649	14	0.00	0.01	0.00	0.02	0.01	0.50	Si
11-13	130608	110608	14	0.00	0.01	0.00	0.02	0.01	0.50	Si
11-13	130576	110576	14	0.00	0.01	0.00	0.01	0.00	0.50	Si
11-13	130735	110735	14	0.00	0.01	-0.00	0.03	0.02	0.50	Si
11-13	130617	110617	14	-0.00	0.01	-0.00	0.02	0.01	0.50	Si
11-13	130658	110658	14	-0.00	0.01	-0.00	0.02	0.01	0.50	Si
11-13	130691	110691	14	-0.00	0.01	-0.01	0.02	0.01	0.50	Si
11-13	130585	110585	14	-0.00	0.01	-0.00	0.01	0.00	0.50	Si
5-13	130736	50736	14	-0.05	0.07	0.00	0.00	0.09	3.13	Si
5-13	130737	50737	14	0.01	0.04	0.00	0.00	0.04	3.13	Si
5-14	140717	50717	14	0.05	0.07	0.00	0.00	0.09	3.63	Si
8-14	140360	80360	14	0.00	0.02	0.01	0.00	0.02	2.07	Si
8-14	140357	80357	14	-0.00	0.01	0.00	-0.00	0.01	2.07	Si
8-14	140354	80354	14	-0.00	0.01	-0.00	-0.00	0.01	2.07	Si
8-14	140351	80351	14	-0.00	0.02	-0.01	0.00	0.02	2.07	Si
8-14	140378	80378	14	0.00	0.01	0.01	0.00	0.01	2.07	Si
8-14	140363	80363	14	-0.00	0.01	-0.00	0.00	0.01	2.07	Si
8-14	140367	80367	14	-0.00	0.01	-0.00	0.00	0.01	2.07	Si
8-14	140389	80389	14	-0.00	0.01	-0.01	0.00	0.01	2.07	Si
8-14	140621	80621	14	-0.00	0.03	-0.01	-0.00	0.03	2.07	Si
8-14	140522	80522	14	0.00	0.01	0.02	0.00	0.02	2.07	Si
8-14	140481	80481	14	0.00	0.01	0.01	-0.00	0.01	2.07	Si
8-14	140424	80424	14	0.00	0.01	0.00	-0.00	0.02	2.07	Si
8-14	140392	80392	14	-0.00	0.01	-0.01	-0.00	0.02	2.07	Si
8-14	140546	80546	14	0.00	0.01	0.00	-0.00	0.02	2.07	Si
8-14	140597	80597	14	0.01	0.02	0.01	-0.00	0.02	2.07	Si
8-14	140600	80600	14	-0.01	0.02	-0.01	-0.01	0.03	2.07	Si
8-14	140550	80550	14	-0.01	0.01	0.00	-0.01	0.02	2.07	Si
8-14	140437	80437	14	-0.00	0.01	-0.00	-0.00	0.02	2.07	Si
8-14	140401	80401	14	-0.00	0.01	0.01	-0.00	0.02	2.07	Si
8-14	140495	80495	14	-0.01	0.01	-0.01	-0.00	0.01	2.07	Si
8-14	140536	80536	14	-0.01	0.01	-0.02	0.00	0.02	2.07	Si
13-14	140457	130457	14	-0.00	0.01	0.00	0.01	0.01	0.50	Si
13-14	140453	130453	14	-0.00	0.01	-0.00	0.00	0.01	0.50	Si
13-14	140449	130449	14	0.00	0.01	0.00	0.00	0.01	0.50	Si
13-14	140445	130445	14	0.00	0.02	-0.00	0.00	0.01	0.50	Si
13-14	140466	130466	14	-0.00	0.01	-0.00	0.02	0.01	0.50	Si
13-14	140486	130486	14	-0.00	0.01	-0.00	0.02	0.01	0.50	Si
13-14	140470	130470	14	0.00	0.01	0.01	0.03	0.02	0.50	Si
13-14	140503	130503	14	0.00	0.01	0.00	0.02	0.01	0.50	Si
13-14	140622	130622	14	-0.00	0.01	-0.01	0.02	0.01	0.50	Si
13-14	140736	130736	14	-0.07	0.06	-0.05	0.07	0.02	0.50	Si
13-14	140737	130737	14	0.06	0.06	0.01	0.04	0.06	0.50	Si
13-14	140676	130676	14	-0.01	0.01	0.01	0.00	0.02	0.50	Si
13-14	140626	130626	14	0.01	0.01	0.01	0.02	0.02	0.50	Si
13-14	140603	130603	14	-0.00	0.01	0.00	0.00	0.01	0.50	Si
13-14	140570	130570	14	-0.00	0.01	-0.00	0.00	0.00	0.50	Si
13-14	140527	130527	14	-0.00	0.01	0.00	0.01	0.00	0.50	Si
13-14	140490	130490	14	-0.00	0.01	-0.00	0.00	0.01	0.50	Si
13-14	140682	130682	14	0.02	0.03	-0.00	0.01	0.03	0.50	Si
13-14	140668	130668	14	-0.01	0.01	-0.00	0.03	0.02	0.50	Si
13-14	140672	130672	14	0.01	0.01	0.01	0.04	0.03	0.50	Si
13-14	140540	130540	14	0.00	0.01	0.00	0.01	0.00	0.50	Si
13-14	140580	130580	14	0.00	0.01	0.00	0.00	0.00	0.50	Si
13-14	140612	130612	14	0.01	0.01	-0.00	0.00	0.01	0.50	Si
13-14	140499	130499	14	0.00	0.01	0.00	0.00	0.01	0.50	Si
12-15	150009	120009	14	0.00	0.01	0.00	-0.01	0.02	1.03	Si
12-15	150019	120019	14	0.01	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150029	120029	14	0.01	0.00	0.00	-0.00	0.01	1.03	Si
12-15	150039	120039	14	0.01	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150049	120049	14	0.01	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150059	120059	14	0.01	-0.00	0.00	-0.01	0.01	1.03	Si

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup.	SpostY sup.	SpostX inf.	SpostY inf.	δ	h/300.00	Verifica
12-15	150069	120069	14	0.01	-0.00	0.00	-0.00	0.01	1.03	Si
12-15	150089	120089	14	0.02	-0.01	0.01	0.01	0.03	1.03	Si
12-15	150079	120079	14	0.01	-0.01	0.01	0.00	0.01	1.03	Si
12-15	150010	120010	14	0.00	0.01	0.00	-0.01	0.02	1.03	Si
12-15	150020	120020	14	0.01	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150030	120030	14	0.01	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150040	120040	14	0.01	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150050	120050	14	0.01	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150060	120060	14	0.01	0.00	0.01	-0.01	0.01	1.03	Si
12-15	150070	120070	14	0.01	-0.00	0.01	-0.00	0.00	1.03	Si
12-15	150090	120090	14	0.02	-0.01	0.01	0.01	0.03	1.03	Si
12-15	150080	120080	14	0.01	-0.01	0.01	0.01	0.01	1.03	Si
12-15	150011	120011	14	-0.00	0.01	0.01	-0.01	0.02	1.03	Si
12-15	150021	120021	14	0.00	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150031	120031	14	0.00	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150041	120041	14	0.00	-0.01	0.01	-0.01	0.01	1.03	Si
12-15	150051	120051	14	0.00	-0.01	0.01	-0.01	0.01	1.03	Si
12-15	150061	120061	14	0.00	-0.01	0.01	-0.01	0.01	1.03	Si
12-15	150071	120071	14	0.00	-0.01	0.01	-0.01	0.01	1.03	Si
12-15	150091	120091	14	0.01	-0.02	0.02	0.01	0.03	1.03	Si
12-15	150081	120081	14	0.00	-0.01	0.01	-0.00	0.01	1.03	Si
12-15	150012	120012	14	-0.01	-0.06	0.01	-0.07	0.02	1.03	Si
12-15	150022	120022	14	-0.00	-0.07	0.02	-0.07	0.02	1.03	Si
12-15	150032	120032	14	-0.00	-0.07	0.02	-0.07	0.03	1.03	Si
12-15	150042	120042	14	-0.00	-0.07	0.02	-0.07	0.02	1.03	Si
12-15	150052	120052	14	-0.00	-0.06	0.02	-0.07	0.03	1.03	Si
12-15	150062	120062	14	-0.00	-0.06	0.02	-0.07	0.02	1.03	Si
12-15	150072	120072	14	-0.00	-0.06	0.02	-0.07	0.02	1.03	Si
12-15	150092	120092	14	0.01	-0.07	0.02	-0.06	0.02	1.03	Si
12-15	150082	120082	14	-0.00	-0.07	0.02	-0.06	0.02	1.03	Si
12-15	150008	120008	14	0.01	0.01	0.00	-0.01	0.02	1.03	Si
12-15	150018	120018	14	0.01	0.00	0.01	-0.01	0.01	1.03	Si
12-15	150028	120028	14	0.01	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150038	120038	14	0.01	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150048	120048	14	0.01	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150058	120058	14	0.01	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150068	120068	14	0.01	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150088	120088	14	0.02	-0.01	0.01	0.01	0.03	1.03	Si
12-15	150078	120078	14	0.01	-0.01	0.01	0.00	0.01	1.03	Si
12-15	150007	120007	14	0.01	0.01	0.01	-0.01	0.02	1.03	Si
12-15	150017	120017	14	0.01	0.00	0.01	-0.01	0.01	1.03	Si
12-15	150027	120027	14	0.01	0.00	0.01	-0.01	0.01	1.03	Si
12-15	150037	120037	14	0.01	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150047	120047	14	0.01	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150057	120057	14	0.01	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150067	120067	14	0.01	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150087	120087	14	0.02	-0.01	0.01	0.01	0.03	1.03	Si
12-15	150077	120077	14	0.01	-0.01	0.01	0.00	0.01	1.03	Si
12-15	150006	120006	14	0.01	0.01	0.01	-0.01	0.02	1.03	Si
12-15	150016	120016	14	0.02	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150026	120026	14	0.02	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150036	120036	14	0.02	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150046	120046	14	0.02	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150056	120056	14	0.02	-0.00	0.01	-0.01	0.01	1.03	Si
12-15	150066	120066	14	0.02	-0.00	0.01	-0.00	0.01	1.03	Si
12-15	150086	120086	14	0.02	-0.01	0.01	0.01	0.03	1.03	Si
12-15	150076	120076	14	0.02	-0.01	0.01	0.00	0.01	1.03	Si
12-15	150005	120005	14	0.02	0.01	0.01	-0.01	0.02	1.03	Si
12-15	150015	120015	14	0.02	0.00	0.01	-0.00	0.02	1.03	Si
12-15	150025	120025	14	0.02	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150035	120035	14	0.02	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150045	120045	14	0.02	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150055	120055	14	0.02	0.00	0.01	-0.00	0.01	1.03	Si
12-15	150065	120065	14	0.02	-0.00	0.01	-0.00	0.01	1.03	Si
12-15	150085	120085	14	0.02	-0.01	0.01	0.01	0.03	1.03	Si
12-15	150075	120075	14	0.02	-0.01	0.01	0.01	0.02	1.03	Si
12-15	150004	120004	14	0.03	0.00	0.01	-0.01	0.03	1.03	Si
12-15	150014	120014	14	0.04	-0.00	0.00	-0.01	0.03	1.03	Si
12-15	150024	120024	14	0.04	-0.00	0.00	-0.01	0.03	1.03	Si
12-15	150034	120034	14	0.04	-0.00	0.00	-0.01	0.03	1.03	Si
12-15	150044	120044	14	0.04	-0.00	0.00	-0.01	0.03	1.03	Si
12-15	150054	120054	14	0.03	-0.00	0.00	-0.01	0.03	1.03	Si
12-15	150064	120064	14	0.03	-0.01	0.00	-0.01	0.03	1.03	Si
12-15	150084	120084	14	0.02	-0.01	0.01	0.01	0.03	1.03	Si
12-15	150074	120074	14	0.03	-0.01	0.00	-0.00	0.03	1.03	Si
12-15	150003	120003	14	0.03	-0.01	0.00	-0.02	0.03	1.03	Si
12-15	150013	120013	14	0.04	-0.02	-0.00	-0.02	0.04	1.03	Si
12-15	150023	120023	14	0.04	-0.02	-0.00	-0.02	0.04	1.03	Si

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup.	SpostY sup.	SpostX inf.	SpostY inf.	δ	h/300.00	Verifica
12-15	150033	120033	14	0.04	-0.02	-0.00	-0.02	0.04	1.03	Si
12-15	150043	120043	14	0.04	-0.01	-0.00	-0.02	0.04	1.03	Si
12-15	150053	120053	14	0.04	-0.01	-0.00	-0.02	0.04	1.03	Si
12-15	150063	120063	14	0.04	-0.01	-0.00	-0.01	0.04	1.03	Si
12-15	150083	120083	14	0.02	-0.02	0.01	-0.01	0.02	1.03	Si
12-15	150073	120073	14	0.03	-0.02	-0.00	-0.01	0.04	1.03	Si
8-16	160274	80274	14	0.00	0.00	0.01	-0.00	0.01	2.57	Si
8-16	160270	80270	14	-0.00	0.00	0.00	-0.01	0.01	2.57	Si
8-16	160266	80266	14	0.00	0.00	0.00	-0.01	0.01	2.57	Si
8-16	160262	80262	14	-0.00	0.00	-0.01	-0.00	0.01	2.57	Si
8-16	160290	80290	14	0.00	0.00	0.00	-0.01	0.01	2.57	Si
8-16	160279	80279	14	-0.00	0.00	-0.00	-0.01	0.01	2.57	Si
8-16	160283	80283	14	0.00	0.00	0.00	-0.01	0.01	2.57	Si
8-16	160294	80294	14	-0.00	0.00	-0.00	-0.01	0.01	2.57	Si
8-16	160553	80553	14	0.00	0.01	0.00	-0.00	0.02	2.57	Si
8-16	160418	80418	14	0.01	-0.00	0.01	-0.01	0.01	2.57	Si
8-16	160384	80384	14	0.00	-0.00	0.01	-0.01	0.01	2.57	Si
8-16	160333	80333	14	0.00	0.00	0.00	-0.01	0.01	2.57	Si
8-16	160303	80303	14	-0.00	-0.00	-0.00	-0.01	0.01	2.57	Si
8-16	160461	80461	14	0.00	-0.01	0.00	-0.01	0.00	2.57	Si
8-16	160518	80518	14	0.01	-0.00	0.01	-0.01	0.00	2.57	Si
8-16	160532	80532	14	-0.01	0.00	-0.01	-0.01	0.02	2.57	Si
8-16	160474	80474	14	-0.00	-0.00	-0.00	-0.01	0.01	2.57	Si
8-16	160312	80312	14	0.00	-0.00	0.00	-0.01	0.01	2.57	Si
8-16	160346	80346	14	-0.00	0.00	-0.00	-0.01	0.01	2.57	Si
8-16	160396	80396	14	-0.00	-0.00	-0.01	-0.01	0.01	2.57	Si
8-16	160429	80429	14	-0.01	-0.00	-0.01	-0.00	0.01	2.57	Si
14-16	160360	140360	14	-0.00	0.01	0.00	0.02	0.01	0.50	Si
14-16	160357	140357	14	-0.00	0.01	-0.00	0.01	0.00	0.50	Si
14-16	160354	140354	14	0.00	0.01	-0.00	0.01	0.00	0.50	Si
14-16	160351	140351	14	-0.00	0.01	-0.00	0.02	0.01	0.50	Si
14-16	160378	140378	14	0.00	0.00	0.00	0.01	0.01	0.50	Si
14-16	160363	140363	14	0.00	0.01	-0.00	0.01	0.01	0.50	Si
14-16	160367	140367	14	-0.00	0.01	-0.00	0.01	0.01	0.50	Si
14-16	160389	140389	14	-0.00	0.00	-0.00	0.01	0.01	0.50	Si
14-16	160681	140681	14	-0.06	0.07	-0.04	0.08	0.03	0.50	Si
14-16	160621	140621	14	-0.00	0.01	-0.00	0.03	0.01	0.50	Si
14-16	160522	140522	14	0.00	0.00	0.00	0.01	0.01	0.50	Si
14-16	160481	140481	14	0.00	0.01	0.00	0.01	0.01	0.50	Si
14-16	160424	140424	14	0.00	0.01	0.00	0.01	0.01	0.50	Si
14-16	160392	140392	14	0.00	0.01	-0.00	0.01	0.01	0.50	Si
14-16	160546	140546	14	0.01	-0.00	0.00	0.01	0.01	0.50	Si
14-16	160597	140597	14	0.01	0.00	0.01	0.02	0.02	0.50	Si
14-16	160600	140600	14	-0.00	0.01	-0.01	0.02	0.02	0.50	Si
14-16	160550	140550	14	-0.01	0.00	-0.01	0.01	0.01	0.50	Si
14-16	160665	140665	14	0.04	0.06	0.02	0.09	0.03	0.50	Si
14-16	160437	140437	14	-0.00	0.01	-0.00	0.01	0.01	0.50	Si
14-16	160495	140495	14	-0.00	0.01	-0.01	0.01	0.01	0.50	Si
14-16	160536	140536	14	-0.01	0.00	-0.01	0.01	0.01	0.50	Si
14-16	160401	140401	14	-0.00	0.01	-0.00	0.01	0.01	0.50	Si
7-16	160630	70630	14	-0.05	0.08	0.00	0.00	0.10	3.00	Si
7-16	160592	70592	14	0.02	0.07	0.00	0.00	0.07	3.00	Si
11-17	170201	110201	14	0.00	0.01	0.01	0.01	0.01	2.00	Si
11-17	170198	110198	14	0.00	0.01	0.00	0.01	0.00	2.00	Si
11-17	170195	110195	14	0.00	0.01	0.00	0.01	0.00	2.00	Si
11-17	170192	110192	14	-0.00	0.01	-0.01	0.01	0.01	2.00	Si
11-17	170217	110217	14	0.01	0.00	0.01	0.00	0.00	2.00	Si
11-17	170211	110211	14	0.00	0.01	-0.00	0.01	0.00	2.00	Si
11-17	170214	110214	14	0.00	0.00	0.00	0.01	0.00	2.00	Si
11-17	170221	110221	14	-0.00	0.00	-0.01	0.00	0.00	2.00	Si
11-17	170328	110328	14	0.01	-0.01	0.01	0.01	0.02	2.00	Si
11-17	170299	110299	14	0.01	-0.00	0.01	-0.00	0.00	2.00	Si
11-17	170251	110251	14	0.01	0.00	0.00	-0.00	0.00	2.00	Si
11-17	170228	110228	14	0.00	-0.00	-0.00	-0.00	0.01	2.00	Si
11-17	170370	110370	14	0.02	-0.03	-0.01	0.02	0.05	2.00	Si
11-17	170433	110433	14	0.02	-0.02	-0.00	0.02	0.05	2.00	Si
11-17	170373	110373	14	-0.00	0.00	0.02	0.01	0.02	2.00	Si
11-17	170234	110234	14	-0.00	-0.00	0.01	-0.01	0.01	2.00	Si
11-17	170258	110258	14	-0.00	0.00	-0.00	-0.00	0.00	2.00	Si
11-17	170308	110308	14	-0.01	-0.01	-0.00	-0.00	0.01	2.00	Si
11-17	170339	110339	14	-0.01	-0.01	-0.00	0.01	0.03	2.00	Si
16-17	170274	160274	14	-0.00	0.00	0.00	0.00	0.00	0.50	Si
16-17	170270	160270	14	-0.00	0.00	-0.00	0.00	0.00	0.50	Si
16-17	170266	160266	14	0.00	0.00	0.00	0.00	0.00	0.50	Si
16-17	170262	160262	14	0.00	0.01	-0.00	0.00	0.00	0.50	Si
16-17	170290	160290	14	0.00	-0.00	0.00	0.00	0.00	0.50	Si
16-17	170279	160279	14	0.00	0.00	-0.00	0.00	0.00	0.50	Si
16-17	170283	160283	14	-0.00	0.00	0.00	0.00	0.00	0.50	Si

COMUNE DI ANDRIA
RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup.	SpostY sup.	SpostX inf.	SpostY inf.	δ	h/300.00	Verifica
16-17	170294	160294	14	-0.00	-0.00	-0.00	0.00	0.00	0.50	Si
16-17	170630	160630	14	-0.08	0.07	-0.05	0.08	0.03	0.50	Si
16-17	170553	160553	14	-0.02	0.02	0.00	0.01	0.02	0.50	Si
16-17	170418	160418	14	0.00	-0.01	0.01	-0.00	0.01	0.50	Si
16-17	170384	160384	14	0.00	-0.01	0.00	-0.00	0.01	0.50	Si
16-17	170333	160333	14	0.00	-0.00	0.00	0.00	0.00	0.50	Si
16-17	170303	160303	14	0.00	-0.00	-0.00	-0.00	0.00	0.50	Si
16-17	170461	160461	14	0.01	-0.03	0.00	-0.01	0.02	0.50	Si
16-17	170518	160518	14	0.01	-0.03	0.01	-0.00	0.03	0.50	Si
16-17	170532	160532	14	0.05	0.07	-0.01	0.00	0.09	0.50	Si
16-17	170474	160474	14	0.00	-0.00	-0.00	-0.00	0.01	0.50	Si
16-17	170592	160592	14	0.07	0.08	0.02	0.07	0.05	0.50	Si
16-17	170346	160346	14	-0.00	-0.00	-0.00	0.00	0.00	0.50	Si
16-17	170396	160396	14	-0.00	-0.01	-0.00	-0.00	0.01	0.50	Si
16-17	170429	160429	14	-0.00	-0.02	-0.01	-0.00	0.02	0.50	Si
16-17	170312	160312	14	-0.00	-0.00	0.00	-0.00	0.00	0.50	Si
11-18	180150	110150	14	0.00	0.01	0.01	0.00	0.01	2.50	Si
11-18	180147	110147	14	-0.00	0.01	-0.00	0.00	0.01	2.50	Si
11-18	180146	110146	14	0.00	0.01	0.00	0.00	0.01	2.50	Si
11-18	180145	110145	14	-0.00	0.01	-0.01	0.00	0.01	2.50	Si
11-18	180154	110154	14	-0.01	0.01	-0.01	0.00	0.01	2.50	Si
11-18	180165	110165	14	-0.00	-0.00	0.00	-0.00	0.01	2.50	Si
11-18	180168	110168	14	0.00	-0.00	-0.00	-0.00	0.01	2.50	Si
11-18	180162	110162	14	0.01	0.01	0.01	-0.00	0.01	2.50	Si
11-18	180158	110158	14	0.02	-0.01	0.00	0.00	0.02	2.50	Si
11-18	180224	110224	14	-0.00	-0.01	-0.00	-0.01	0.00	2.50	Si
11-18	180248	110248	14	0.00	0.00	0.00	0.00	0.00	2.50	Si
11-18	180173	110173	14	-0.01	-0.01	-0.01	-0.01	0.00	2.50	Si
11-18	180189	110189	14	-0.00	-0.01	0.00	-0.01	0.01	2.50	Si
11-18	180325	110325	14	-0.01	0.02	-0.01	0.01	0.01	2.50	Si
11-18	180382	110382	14	-0.00	0.01	-0.00	0.01	0.00	2.50	Si
11-18	180322	110322	14	0.01	0.01	0.01	0.01	0.01	2.50	Si
11-18	180164	110164	14	-0.05	-0.01	0.00	0.00	0.05	2.50	Si
11-18	180256	110256	14	-0.00	-0.00	-0.00	0.01	0.01	2.50	Si
11-18	180176	110176	14	0.01	-0.01	0.01	-0.01	0.00	2.50	Si
11-18	180232	110232	14	0.00	-0.01	0.00	-0.01	0.00	2.50	Si
11-18	180204	110204	14	0.00	-0.01	-0.00	-0.01	0.01	2.50	Si
17-18	180201	170201	14	0.00	0.01	0.00	0.01	0.01	0.50	Si
17-18	180198	170198	14	-0.00	0.02	0.00	0.01	0.01	0.50	Si
17-18	180195	170195	14	0.00	0.02	0.00	0.01	0.01	0.50	Si
17-18	180192	170192	14	0.00	0.01	-0.00	0.01	0.01	0.50	Si
17-18	180217	170217	14	0.00	0.00	0.01	0.00	0.00	0.50	Si
17-18	180211	170211	14	0.00	0.01	0.00	0.01	0.01	0.50	Si
17-18	180214	170214	14	0.00	0.01	0.00	0.00	0.01	0.50	Si
17-18	180221	170221	14	-0.00	0.00	-0.00	0.00	0.00	0.50	Si
17-18	180566	170566	14	-0.01	-0.00	-0.06	0.10	0.11	0.50	Si
17-18	180480	170480	14	0.03	-0.04	-0.01	0.03	0.08	0.50	Si
17-18	180328	170328	14	0.00	0.01	0.01	-0.01	0.02	0.50	Si
17-18	180299	170299	14	0.00	-0.00	0.01	-0.00	0.01	0.50	Si
17-18	180251	170251	14	0.01	0.00	0.01	0.00	0.00	0.50	Si
17-18	180228	170228	14	0.01	-0.00	0.00	-0.00	0.00	0.50	Si
17-18	180414	170414	14	0.03	0.06	0.03	0.06	0.00	0.50	Si
17-18	180370	170370	14	-0.01	0.03	0.02	-0.03	0.06	0.50	Si
17-18	180433	170433	14	-0.00	0.02	0.02	-0.02	0.05	0.50	Si
17-18	180373	170373	14	0.01	0.02	-0.00	0.00	0.02	0.50	Si
17-18	180507	170507	14	0.09	0.11	0.03	0.08	0.06	0.50	Si
17-18	180258	170258	14	-0.00	0.00	-0.00	0.00	0.00	0.50	Si
17-18	180308	170308	14	0.00	0.00	-0.01	-0.01	0.01	0.50	Si
17-18	180339	170339	14	0.00	0.01	-0.01	-0.01	0.03	0.50	Si
17-18	180234	170234	14	-0.00	-0.00	-0.00	-0.00	0.00	0.50	Si
11-19	190097	110097	14	-0.01	-0.18	0.00	0.00	0.18	3.00	Si
11-19	190098	110098	14	-0.01	-0.20	0.00	0.00	0.21	3.00	Si
11-19	190099	110099	14	-0.01	-0.20	0.00	0.00	0.20	3.00	Si
11-19	190101	110101	14	-0.01	-0.18	0.00	0.00	0.18	3.00	Si
11-19	190107	110107	14	-0.01	-0.18	0.00	0.00	0.18	3.00	Si
11-19	190113	110113	14	-0.02	-0.16	0.00	0.00	0.16	3.00	Si
11-19	190115	110115	14	-0.01	-0.15	0.00	0.00	0.15	3.00	Si
11-19	190109	110109	14	-0.01	-0.18	0.00	0.00	0.18	3.00	Si
11-19	190137	110137	14	-0.02	-0.15	0.00	0.00	0.15	3.00	Si
11-19	190123	110123	14	-0.02	-0.15	0.00	0.00	0.15	3.00	Si
11-19	190124	110124	14	-0.00	-0.14	0.00	0.00	0.14	3.00	Si
11-19	190139	110139	14	-0.00	-0.14	0.00	0.00	0.14	3.00	Si
18-19	190145	180145	14	-0.01	-0.19	-0.00	0.01	0.20	0.50	Si
18-19	190146	180146	14	-0.00	-0.21	0.00	0.01	0.22	0.50	Si
18-19	190147	180147	14	0.00	-0.21	-0.00	0.01	0.22	0.50	Si
18-19	190150	180150	14	0.01	-0.18	0.00	0.01	0.20	0.50	Si
18-19	190165	180165	14	0.02	-0.15	-0.00	-0.00	0.15	0.50	Si
18-19	190154	180154	14	0.02	-0.18	-0.01	0.01	0.19	0.50	Si

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup.	SpostY sup.	SpostX inf.	SpostY inf.	δ	h/300.00	Verifica
18-19	190162	180162	14	-0.02	-0.18	0.01	0.01	0.19	0.50	Si
18-19	190168	180168	14	-0.02	-0.15	0.00	-0.00	0.15	0.50	Si
18-19	190173	180173	14	0.02	-0.13	-0.01	-0.01	0.12	0.50	Si
18-19	190189	180189	14	0.03	-0.13	-0.00	-0.01	0.12	0.50	Si
18-19	190224	180224	14	-0.00	-0.05	-0.00	-0.01	0.04	0.50	Si
18-19	190176	180176	14	-0.02	-0.13	0.01	-0.01	0.12	0.50	Si
18-19	190204	180204	14	-0.03	-0.13	0.00	-0.01	0.13	0.50	Si
18-19	190232	180232	14	0.01	-0.05	0.00	-0.01	0.04	0.50	Si
18-19	190158	180158	14	-0.06	-0.06	0.02	-0.01	0.09	0.50	Si
18-19	190164	180164	14	0.04	-0.04	-0.05	-0.01	0.09	0.50	Si

Verifica spostamenti orizzontali in sommità (§4.2.4.2.2 - NTC 2008)

Nodo	Comb.	SpostX mm	SpostY mm	Δ mm	H/500.00 mm	Verifica
190145 (Nodo_190145)	14	-0.01	-0.19	0.19	5.80	Si
190146 (Nodo_190146)	14	-0.00	-0.21	0.21	5.80	Si
190147 (Nodo_190147)	14	0.00	-0.21	0.21	5.80	Si
190150 (Nodo_190150)	14	0.01	-0.18	0.18	5.80	Si
190165 (Nodo_190165)	14	0.02	-0.15	0.15	5.80	Si
190154 (Nodo_190154)	14	0.02	-0.18	0.18	5.80	Si
190162 (Nodo_190162)	14	-0.02	-0.18	0.19	5.80	Si
190168 (Nodo_190168)	14	-0.02	-0.15	0.15	5.80	Si
190173 (Nodo_190173)	14	0.02	-0.13	0.14	5.80	Si
190189 (Nodo_190189)	14	0.03	-0.13	0.13	5.80	Si
190224 (Nodo_190224)	14	-0.00	-0.05	0.05	5.80	Si
190176 (Nodo_190176)	14	-0.02	-0.13	0.13	5.80	Si
190204 (Nodo_190204)	14	-0.03	-0.13	0.13	5.80	Si
190232 (Nodo_190232)	14	0.01	-0.05	0.05	5.80	Si
190158 (Nodo_190158)	14	-0.06	-0.06	0.08	5.80	Si
190164 (Nodo_190164)	14	0.04	-0.04	0.05	5.80	Si

STRUTTURA GRATTICCIA

TABULATI DI INPUT

Dati generali

Nome struttura	Graticcia
Numero di frequenze	100
% Filtro masse libere	0.1
% Coefficiente di smorzamento viscoso	5
Spostamenti modali con segno	Si
Deformabilità a taglio delle aste	Si
Spostamento ammissibile impalcati	0.0050*h

Impalcati

N°	Quota	Rigido	Incr.Soll.Pil	Inc.Soll.Par.
	mm			
0	0	No	1.000	1.000
1	1550	Si	1.000	1.000

Percentuali Spostamento masse impalcati

Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Combinazioni del Sisma in X e Y e Verticale

Comb	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
1	1	2	1	0.3	0
2	1	2	0.3	1	0
3	1	4	1	0.3	0
4	1	4	0.3	1	0
5	3	2	1	0.3	0
6	3	2	0.3	1	0
7	3	4	1	0.3	0
8	3	4	0.3	1	0

Comb. = Numero di combinazione dei sismi

Pos. SismaX = Posizione in cui viene scelto il sisma in direzione X

Pos. SismaY = Posizione in cui viene scelto il sisma in direzione Y

Fx = Fattore con cui il sisma X partecipa

Fy = Fattore con cui il sisma Y partecipa

Fz = Fattore con cui il sisma Verticale partecipa (quando richiesto)

Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz.

Spettri di risposta

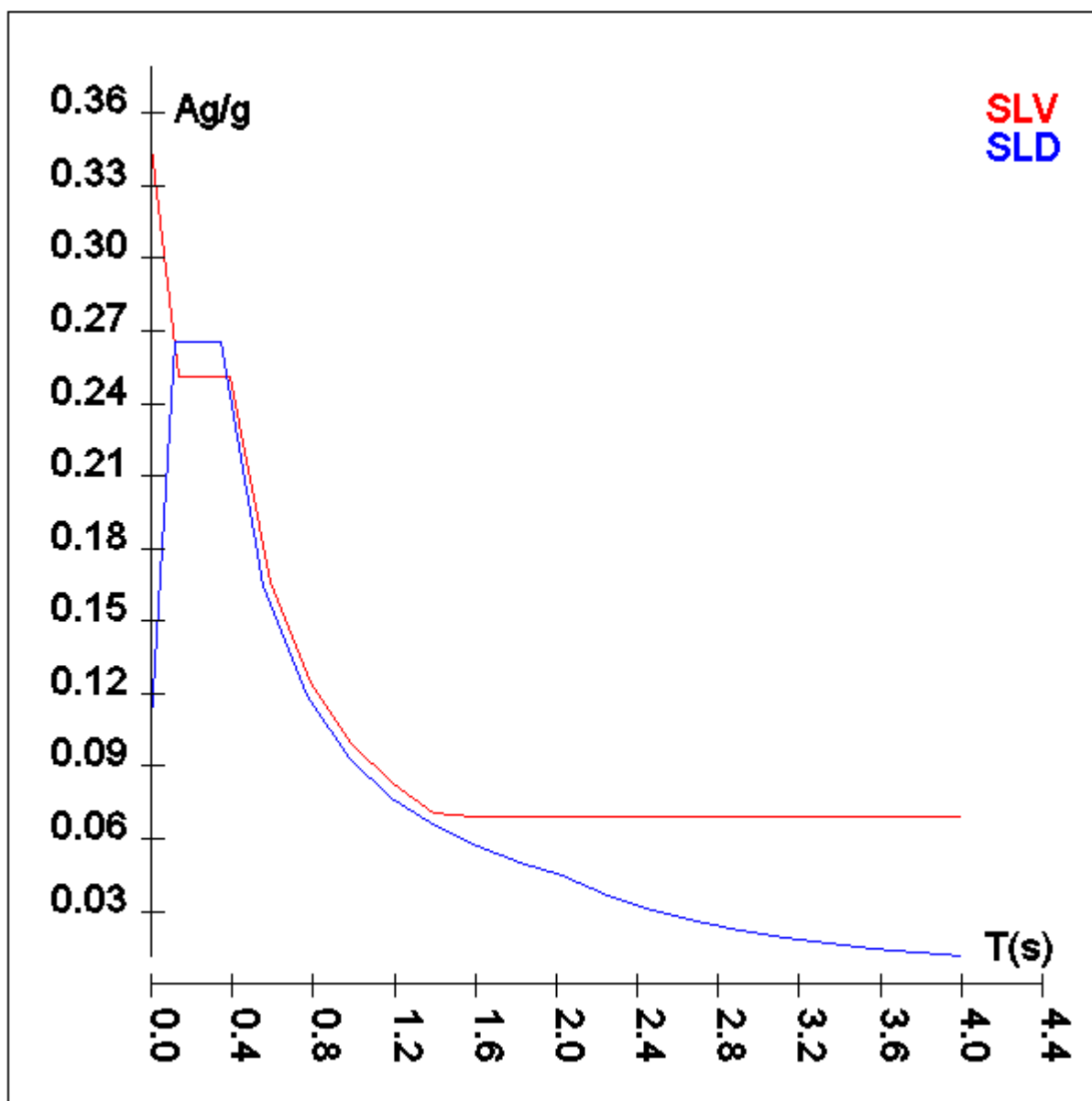
Spettro :SpettroNT

Il calcolo degli spettri e del fattore di struttura sono stati calcolati per la seguente tipologia di terreno e struttura

Vita della struttura	
Tipo	Opere ordinarie (50-100) 50 - 100 anni
Vita nominale(anni)	100.0
Classe d'uso	Classe IV
Coefficiente d'uso	2.000
Periodo di riferimento(anni)	200.000
Stato limite di esercizio - SLD	PVR=63.0%
Stato limite ultimo - SLV	PVR=10.0%
Periodo di ritorno SLD(anni)	TR=201.0
Periodo di ritorno SLV(anni)	TR=1898.2
Parametri del sito	
Comune	Andria - (BT)
Longitudine	16.2825
Latitudine	41.2216
Id reticolo del sito	31233-31455-31456-31234
Valori di riferimento del sito	
A _g /g(TR=201.0) SLD	0.1078
F ₀ (TR=201.0) SLD	2.4612
T [*] C(TR=201.0) SLD	0.344
A _g /g(TR=1898.2) SLV	0.3465
F ₀ (TR=1898.2) SLV	2.3179
T [*] C(TR=1898.2) SLV	0.392
Coefficiente Amplificazione Topografica	St=1.000
Categoria terreno A	
stato limite SLV	
	S=1.00
	TB=0.13
	TC=0.39
	TD=2.99
stato limite SLD	
	S=1.00
	TB=0.11
	TC=0.34
	TD=2.03
Fattore di struttura (SLV)	
Classe duttilità	B
Tipo struttura	Acciaio
Struttura non regolare in altezza	Kr=0.800000
	Kw=1.000
Regolare in pianta	SI
Tipologia : Strutture a telaio	Ce=4.000
Fattore di struttura q=Kw*Kr*Ce	3.200

TSLV [s]	SLV[a/g]	TSLD [s]	SLD[a/g]
0.00000	0.34645	0.00000	0.10785
0.13062	0.25095	0.11479	0.26544
0.39186	0.25095	0.34437	0.26544
0.59140	0.16628	0.55525	0.16463
0.79093	0.12433	0.76613	0.11932
0.99047	0.09929	0.97701	0.09356
1.19000	0.08264	1.18788	0.07695
1.38954	0.07077	1.39876	0.06535
1.58907	0.06929	1.60964	0.05679
1.78861	0.06929	1.82052	0.05021
1.98814	0.06929	2.03140	0.04500
2.18768	0.06929	2.25013	0.03668
2.38721	0.06929	2.46886	0.03046

2.58675	0.06929	2.68760	0.02571
2.78628	0.06929	2.90633	0.02198
2.98582	0.06929	3.12507	0.01901
3.23936	0.06929	3.34380	0.01661
3.49291	0.06929	3.56253	0.01463
3.74645	0.06929	3.78127	0.01299
4.00000	0.06929	4.00000	0.01161



Materiali

Materiale: Acciaio

Peso specifico	kg/mc	7850
Modulo di Young E	kg/cm ²	2E06
Modulo di Poisson ν		0.30
Coefficiente di dilatazione termica λ	1/°C	1.2e-005

Nodi - Geometria e vincoli

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
			Coordinate [mm]						Vincoli	
2	250	0	0	0	0	0	0	0	0	0
4	1400	0	0	0	0	0	0	0	0	0
5	3175	0	0	0	0	0	0	0	0	0
6	4950	0	0	0	0	0	0	0	0	0
7	6725	0	0	0	0	0	0	0	0	0
8	8500	0	0	0	0	0	0	0	0	0
9	9650	0	0	0	0	0	0	0	0	0
11	250	1106	0	0	0	0	0	0	0	0
12	1400	1106	0	0	0	0	0	0	0	0
13	3175	1106	0	0	0	0	0	0	0	0
14	4950	1106	0	0	0	0	0	0	0	0
15	6725	1106	0	0	0	0	0	0	0	0
16	8500	1106	0	0	0	0	0	0	0	0
17	9650	1106	0	0	0	0	0	0	0	0
18	250	2213	0	0	0	0	0	0	0	0
19	1400	2213	0	0	0	0	0	0	0	0
20	3175	2213	0	0	0	0	0	0	0	0
21	4950	2213	0	0	0	0	0	0	0	0
22	6725	2213	0	0	0	0	0	0	0	0
23	8500	2213	0	0	0	0	0	0	0	0
24	9650	2213	0	0	0	0	0	0	0	0
25	250	3319	0	0	0	0	0	0	0	0
26	1400	3319	0	0	0	0	0	0	0	0
27	3175	3319	0	0	0	0	0	0	0	0
28	4950	3319	0	0	0	0	0	0	0	0
29	6725	3319	0	0	0	0	0	0	0	0
30	8500	3319	0	0	0	0	0	0	0	0
31	9650	3319	0	0	0	0	0	0	0	0
33	250	4425	0	0	0	0	0	0	0	0
34	1400	4425	0	0	0	0	0	0	0	0
35	3175	4425	0	0	0	0	0	0	0	0
36	4950	4425	0	0	0	0	0	0	0	0
37	6725	4425	0	0	0	0	0	0	0	0
38	8500	4425	0	0	0	0	0	0	0	0
39	9650	4425	0	0	0	0	0	0	0	0
41	250	5531	0	0	0	0	0	0	0	0
42	1400	5531	0	0	0	0	0	0	0	0
43	3175	5531	0	0	0	0	0	0	0	0
44	4950	5531	0	0	0	0	0	0	0	0
45	6725	5531	0	0	0	0	0	0	0	0
46	8500	5531	0	0	0	0	0	0	0	0
47	9650	5531	0	0	0	0	0	0	0	0
48	250	6638	0	0	0	0	0	0	0	0
49	1400	6638	0	0	0	0	0	0	0	0
50	3175	6638	0	0	0	0	0	0	0	0
51	4950	6638	0	0	0	0	0	0	0	0
52	6725	6638	0	0	0	0	0	0	0	0
53	8500	6638	0	0	0	0	0	0	0	0
54	9650	6638	0	0	0	0	0	0	0	0
55	250	7744	0	0	0	0	0	0	0	0
56	1400	7744	0	0	0	0	0	0	0	0
57	3175	7744	0	0	0	0	0	0	0	0
58	4950	7744	0	0	0	0	0	0	0	0
59	6725	7744	0	0	0	0	0	0	0	0
60	8500	7744	0	0	0	0	0	0	0	0
61	9650	7744	0	0	0	0	0	0	0	0
63	250	8850	0	0	0	0	0	0	0	0
64	1400	8850	0	0	0	0	0	0	0	0
65	3175	8850	0	0	0	0	0	0	0	0
66	4950	8850	0	0	0	0	0	0	0	0
67	6725	8850	0	0	0	0	0	0	0	0

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
68	8500	8850	0	0	0	0	0	0	0	0
69	9650	8850	0	0	0	0	0	0	0	0
101	0	0	1550	1	1	1	1	1	1	1
102	250	0	1550	0	0	0	0	0	0	1
103	410	0	1550	0	0	0	0	0	0	1
104	1400	0	1550	0	0	0	0	0	0	1
105	3175	0	1550	0	0	0	0	0	0	1
106	4950	0	1550	0	0	0	0	0	0	1
107	6725	0	1550	0	0	0	0	0	0	1
108	8500	0	1550	0	0	0	0	0	0	1
109	9650	0	1550	0	0	0	0	0	0	1
110	9900	0	1550	1	1	1	1	1	1	1
132	0	4425	1550	1	1	1	1	1	1	1
133	250	4425	1550	0	0	0	0	0	0	1
134	1400	4425	1550	0	0	0	0	0	0	1
135	3175	4425	1550	0	0	0	0	0	0	1
136	4950	4425	1550	0	0	0	0	0	0	1
137	6725	4425	1550	0	0	0	0	0	0	1
138	8500	4425	1550	0	0	0	0	0	0	1
139	9650	4425	1550	0	0	0	0	0	0	1
140	9900	4425	1550	1	1	1	1	1	1	1
162	0	8850	1550	1	1	1	1	1	1	1
163	250	8850	1550	0	0	0	0	0	0	1
164	1400	8850	1550	0	0	0	0	0	0	1
165	3175	8850	1550	0	0	0	0	0	0	1
166	4950	8850	1550	0	0	0	0	0	0	1
167	6725	8850	1550	0	0	0	0	0	0	1
168	8500	8850	1550	0	0	0	0	0	0	1
169	9650	8850	1550	0	0	0	0	0	0	1
170	9900	8850	1550	1	1	1	1	1	1	1

Nodi - Carichi

N°	C.Car.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
				kg			kg*m			mm			mmrad	°C
11	QFissi Travi	0	0	500	0	0	0							
12	QFissi Travi	0	0	500	0	0	0							
13	QFissi Travi	0	0	500	0	0	0							
14	QFissi Travi	0	0	500	0	0	0							
15	QFissi Travi	0	0	500	0	0	0							
16	QFissi Travi	0	0	500	0	0	0							
17	QFissi Travi	0	0	500	0	0	0							
18	QFissi Travi	0	0	500	0	0	0							
19	QFissi Travi	0	0	500	0	0	0							
20	QFissi Travi	0	0	500	0	0	0							
21	QFissi Travi	0	0	500	0	0	0							
22	QFissi Travi	0	0	500	0	0	0							
23	QFissi Travi	0	0	500	0	0	0							
24	QFissi Travi	0	0	500	0	0	0							
25	QFissi Travi	0	0	500	0	0	0							
26	QFissi Travi	0	0	500	0	0	0							
27	QFissi Travi	0	0	500	0	0	0							
28	QFissi Travi	0	0	500	0	0	0							
29	QFissi Travi	0	0	500	0	0	0							
30	QFissi Travi	0	0	500	0	0	0							
31	QFissi Travi	0	0	500	0	0	0							
41	QFissi Travi	0	0	500	0	0	0							
42	QFissi Travi	0	0	500	0	0	0							
43	QFissi Travi	0	0	500	0	0	0							
44	QFissi Travi	0	0	500	0	0	0							
45	QFissi Travi	0	0	500	0	0	0							
46	QFissi Travi	0	0	500	0	0	0							
47	QFissi Travi	0	0	500	0	0	0							
48	QFissi Travi	0	0	500	0	0	0							
49	QFissi Travi	0	0	500	0	0	0							
50	QFissi Travi	0	0	500	0	0	0							
51	QFissi Travi	0	0	500	0	0	0							
52	QFissi Travi	0	0	500	0	0	0							
53	QFissi Travi	0	0	500	0	0	0							
54	QFissi Travi	0	0	500	0	0	0							
55	QFissi Travi	0	0	500	0	0	0							
56	QFissi Travi	0	0	500	0	0	0							
57	QFissi Travi	0	0	500	0	0	0							
58	QFissi Travi	0	0	500	0	0	0							
59	QFissi Travi	0	0	500	0	0	0							
60	QFissi Travi	0	0	500	0	0	0							

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

N°	C.Car.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
61	QFissi Travi	0	0	500	0	0	0							

Input - Aste - Tabella sezioni tipo

Tipo	Nome	Area	Ix	Iy	It	Fx	Fy	Lx	Lx
G		mq	m ⁴	m ⁴	m ⁴			cm	cm
	Tubo100x100x8	0.0	4.184E-06	4.184E-06	6.511E-06	2.286	2.286	10	10

Aste - Geometria e vincoli

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
							°							cm			cm
701	101	102	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	25	25
701	102	104	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
701	104	105	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
701	105	106	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
701	106	107	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
701	107	108	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
701	108	109	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
701	109	110	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	25	25
702	132	133	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	25	25
702	133	134	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
702	134	135	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
702	135	136	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
702	136	137	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
702	137	138	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
702	138	139	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
702	139	140	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	25	25
703	162	163	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	25	25
703	163	164	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
703	164	165	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
703	165	166	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
703	166	167	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
703	167	168	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
703	168	169	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
703	169	170	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	25	25
704	103	133	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	443	443
704	133	163	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	443	443
705	109	139	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	443	443
705	139	169	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	443	443
8000	2	4	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
8000	4	5	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
8000	5	6	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
8000	6	7	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
8000	7	8	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
8000	8	9	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
8014	33	34	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
8014	34	35	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
8014	35	36	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
8014	36	37	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
8014	37	38	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
8014	38	39	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
8028	63	64	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
8028	64	65	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
8028	65	66	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	177	177
8028	66	67	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
8028	67	68	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	178	178
8028	68	69	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	115	115
8042	2	11	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8042	11	18	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8042	18	25	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8042	25	33	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8042	33	41	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8042	41	48	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8042	48	55	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8042	55	63	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8043	4	12	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8043	12	19	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8043	19	26	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8043	26	34	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8043	34	42	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8043	42	49	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
8043	49	56	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8043	56	64	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8044	5	13	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8044	13	20	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8044	20	27	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8044	27	35	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8044	35	43	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8044	43	50	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8044	50	57	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8044	57	65	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8045	6	14	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8045	14	21	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8045	21	28	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8045	28	36	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8045	36	44	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8045	44	51	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8045	51	58	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8045	58	66	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8046	7	15	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8046	15	22	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8046	22	29	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8046	29	37	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8046	37	45	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8046	45	52	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8046	52	59	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8046	59	67	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8047	8	16	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8047	16	23	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8047	23	30	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8047	30	38	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8047	38	46	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8047	46	53	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8047	53	60	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8047	60	68	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8048	9	17	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8048	17	24	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8048	24	31	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8048	31	39	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8048	39	47	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8048	47	54	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8048	54	61	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8048	61	69	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Trave	111	111
8001	2	102	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8002	4	104	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8003	5	105	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8004	6	106	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8005	7	107	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8006	8	108	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8007	9	109	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8008	2	104	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	193	193
8009	4	105	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8010	5	106	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8011	7	106	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8012	8	107	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8013	9	108	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	193	193
8015	33	133	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8016	34	134	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8017	35	135	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8018	36	136	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8019	37	137	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8020	38	138	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8021	39	139	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8022	33	134	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	193	193
8023	34	135	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8024	35	136	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8025	37	136	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8026	38	137	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8027	39	138	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	193	193
8029	63	163	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8030	64	164	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8031	65	165	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8032	66	166	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8033	67	167	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8034	68	168	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8035	69	169	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	155	155
8036	63	164	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	193	193
8037	64	165	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8038	65	166	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8039	67	166	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
8040	68	167	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	236	236
8041	69	168	I-I	Tubo100x100x8	Acciaio	Acciaio_Svergolamento	0	5050	0	0	0	0	0	0	Gen.	193	193

Aste - Carichi

Descrizione carichi aste

UnifG	Uniforme globale
UnifL	Uniforme locale
VarG	Variabile lineare globale
VarL	Variabile lineare locale
PolG	Poligonale globale
Termico	Distorsione termica
Torcente	Carico torcente
Precomp.	Carico da precompressione
PolL	Poligonale locale

Piloni da installare												
Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					cm	car. dist. kg/m coppie torc. kg*m/m			cm	car. dist. kg/m coppie torc. kg*m/m		
Trave 701												
Tubo100x100x8	101	102	Peso Proprio	UnifG	0	0	0	23	25	0	0	23
Tubo100x100x8	102	104	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Tubo100x100x8	104	105	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	105	106	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	106	107	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	107	108	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	108	109	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Tubo100x100x8	109	110	Peso Proprio	UnifG	0	0	0	23	25	0	0	23
Trave 702												
Tubo100x100x8	132	133	Peso Proprio	UnifG	0	0	0	23	25	0	0	23
Tubo100x100x8	133	134	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Tubo100x100x8	134	135	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	135	136	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	136	137	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	137	138	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	138	139	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Tubo100x100x8	139	140	Peso Proprio	UnifG	0	0	0	23	25	0	0	23
Trave 703												
Tubo100x100x8	162	163	Peso Proprio	UnifG	0	0	0	23	25	0	0	23
Tubo100x100x8	163	164	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Tubo100x100x8	164	165	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	165	166	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	166	167	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	167	168	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	168	169	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Tubo100x100x8	169	170	Peso Proprio	UnifG	0	0	0	23	25	0	0	23
Trave 704												
Tubo100x100x8	103	133	Peso Proprio	UnifG	0	0	0	23	443	0	0	23
Tubo100x100x8	133	163	Peso Proprio	UnifG	0	0	0	23	443	0	0	23
Trave 705												
Tubo100x100x8	109	139	Peso Proprio	UnifG	0	0	0	23	443	0	0	23
Tubo100x100x8	139	169	Peso Proprio	UnifG	0	0	0	23	443	0	0	23
Trave 8000												
Tubo100x100x8	2	4	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Tubo100x100x8	4	5	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	5	6	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	6	7	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	7	8	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	8	9	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Trave 8014												
Tubo100x100x8	33	34	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Tubo100x100x8	34	35	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	35	36	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	36	37	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	37	38	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	38	39	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Trave 8028												
Tubo100x100x8	63	64	Peso Proprio	UnifG	0	0	0	23	115	0	0	23
Tubo100x100x8	64	65	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	65	66	Peso Proprio	UnifG	0	0	0	23	177	0	0	23
Tubo100x100x8	66	67	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	67	68	Peso Proprio	UnifG	0	0	0	23	178	0	0	23
Tubo100x100x8	68	69	Peso Proprio	UnifG	0	0	0	23	115	0	0	23

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Trave 8042												
Tubo100x100x8	2	11	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	11	18	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	18	25	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	25	33	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	33	41	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	41	48	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	48	55	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	55	63	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Trave 8043												
Tubo100x100x8	4	12	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	12	19	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	19	26	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	26	34	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	34	42	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	42	49	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	49	56	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	56	64	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Trave 8044												
Tubo100x100x8	5	13	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	13	20	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	20	27	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	27	35	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	35	43	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	43	50	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	50	57	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	57	65	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Trave 8045												
Tubo100x100x8	6	14	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	14	21	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	21	28	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	28	36	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	36	44	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	44	51	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	51	58	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	58	66	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Trave 8046												
Tubo100x100x8	7	15	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	15	22	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	22	29	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	29	37	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	37	45	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	45	52	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	52	59	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	59	67	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Trave 8047												
Tubo100x100x8	8	16	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	16	23	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	23	30	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	30	38	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	38	46	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	46	53	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	53	60	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	60	68	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Trave 8048												
Tubo100x100x8	9	17	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	17	24	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	24	31	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	31	39	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	39	47	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	47	54	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	54	61	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Tubo100x100x8	61	69	Peso Proprio	UnifG	0	0	0	23	111	0	0	23
Generica 8001												
Tubo100x100x8	2	102	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8002												
Tubo100x100x8	4	104	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8003												
Tubo100x100x8	5	105	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8004												
Tubo100x100x8	6	106	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8005												
Tubo100x100x8	7	107	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8006												
Tubo100x100x8	8	108	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8007												
Tubo100x100x8	9	109	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8008												

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Tubo100x100x8	2	104	Peso Proprio	UnifG	0	0	0	23	193	0	0	23
Generica 8009												
Tubo100x100x8	4	105	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8010												
Tubo100x100x8	5	106	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8011												
Tubo100x100x8	7	106	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8012												
Tubo100x100x8	8	107	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8013												
Tubo100x100x8	9	108	Peso Proprio	UnifG	0	0	0	23	193	0	0	23
Generica 8015												
Tubo100x100x8	33	133	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8016												
Tubo100x100x8	34	134	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8017												
Tubo100x100x8	35	135	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8018												
Tubo100x100x8	36	136	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8019												
Tubo100x100x8	37	137	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8020												
Tubo100x100x8	38	138	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8021												
Tubo100x100x8	39	139	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8022												
Tubo100x100x8	33	134	Peso Proprio	UnifG	0	0	0	23	193	0	0	23
Generica 8023												
Tubo100x100x8	34	135	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8024												
Tubo100x100x8	35	136	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8025												
Tubo100x100x8	37	136	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8026												
Tubo100x100x8	38	137	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8027												
Tubo100x100x8	39	138	Peso Proprio	UnifG	0	0	0	23	193	0	0	23
Generica 8029												
Tubo100x100x8	63	163	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8030												
Tubo100x100x8	64	164	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8031												
Tubo100x100x8	65	165	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8032												
Tubo100x100x8	66	166	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8033												
Tubo100x100x8	67	167	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8034												
Tubo100x100x8	68	168	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8035												
Tubo100x100x8	69	169	Peso Proprio	UnifG	0	0	0	23	155	0	0	23
Generica 8036												
Tubo100x100x8	63	164	Peso Proprio	UnifG	0	0	0	23	193	0	0	23
Generica 8037												
Tubo100x100x8	64	165	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8038												
Tubo100x100x8	65	166	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8039												
Tubo100x100x8	67	166	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8040												
Tubo100x100x8	68	167	Peso Proprio	UnifG	0	0	0	23	236	0	0	23
Generica 8041												
Tubo100x100x8	69	168	Peso Proprio	UnifG	0	0	0	23	193	0	0	23

TABULATI DI VERIFICA

Centri di rigidezza e Centri di massa

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Centri rigidezze

Piano	Kx	Ky	Kxy	K ϕ	X	Y	r/ls
	kg/cm	kg/cm	kg/cm	kg*cm/rad	cm	cm	
0	7.570673E05	8.997818E03	1.623975E-02	1.009464E11	510	442	0.980

Ellissi delle rigidezze

Piano	K $_{\xi}$	K $_{\eta}$	alfa	r $_{\xi}$	r $_{\eta}$
	kg/cm	kg/cm	°	cm	cm
0	7.570673E05	8.997818E03	-0	3349	365

Baricentri masse per posizione masse

Piano	Pos.Masse	X	Y	Peso Sism.
		cm	cm	kg
0	1	495	398	23920
0	2	542	442	23920
0	3	495	487	23920
0	4	448	442	23920
1	1	495	398	1932
1	2	542	442	1932
1	3	495	487	1932
1	4	448	442	1932

Risultati Analisi Dinamica - Baricentri masse e masse

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Combinazione masse 1

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	23920	495	398	0
1	Si	1932	495	398	155

Combinazione masse 2

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	23920	542	442	0
1	Si	1932	542	442	155

Combinazione masse 3

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	23920	495	487	0
1	Si	1932	495	487	155

Combinazione masse 4

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	23920	448	442	0
1	Si	1932	448	442	155

Taglianti di piano

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

I taglianti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(I,II) Pm=posizione masse(1,2,...)

Azioni compressive, riferite al sistema WCS, con origine in (0,0,0), i momenti sono comprensivi dei momenti di trasporto $\Theta = Fz \cdot dr / (Fh \cdot H)$ con: Fz=forza verticale, dr=spost medio del piano rispetto al piano inferiore, Fh=tagliante, H=altezza del piano

Combinazione 12-I-1 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	4584	-9	-23073	-33	500	758	4950	4425	0	--
1	-4584	9	24747	50	6606	-758	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	4584	-9
1	0	0	0	0	0	0	-4584	9

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 12-I-2 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	4231	7	-22910	-34	116	-100	4950	4425	0	--
1	-4231	-7	24583	28	6442	99	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	4231	7
1	0	0	0	0	0	0	-4231	-7

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 12-I-3 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	4589	14	-23106	-53	600	-901	4950	4425	0	--
1	-4589	-14	24780	56	6513	886	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	4589	14
1	0	0	0	0	0	0	-4589	-14

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 12-I-4 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	4232	-1	-23250	8	97	-33	4950	4425	0	--
1	-4232	1	24924	-4	6462	34	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	4232	-1
1	0	0	0	0	0	0	-4232	1

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 13-I-1 (SISMAY_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-48	4629	-22918	-857	-61	-426	4950	4425	0	--
1	48	-4629	24592	-6375	-14	423	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	-48	4629
1	0	0	0	0	0	0	48	-4629

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 13-I-2 (SISMAY_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-1	4642	-23038	-343	-14	2064	4950	4425	0	--
1	1	-4642	24712	-6848	13	-1985	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	-1	4642
1	0	0	0	0	0	0	1	-4642

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 13-I-3 (SISMAY_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	50	4637	-23249	-866	81	-408	4950	4425	0	--
1	-50	-4637	24922	-6378	-3	405	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	50	4637
1	0	0	0	0	0	0	-50	-4637

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 13-I-4 (SISMAY_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	1	4632	-23121	-458	-41	-2321	4950	4425	0	--
1	-1	-4632	24795	-6777	43	2293	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	1	4632
1	0	0	0	0	0	0	-1	-4632

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 28-I-1 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	4827	-9	-23073	-36	533	794	4950	4425	0	--
1	-4827	9	24746	53	6949	-794	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	4827	-9
1	0	0	0	0	0	0	-4827	9

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 28-I-2 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	4454	7	-22902	-38	133	-103	4950	4425	0	--
1	-4454	-7	24575	31	6770	102	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	4454	7
1	0	0	0	0	0	0	-4454	-7

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 28-I-3 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	4833	15	-23108	-57	640	-945	4950	4425	0	--
1	-4833	-15	24781	60	6850	929	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	4833	15
1	0	0	0	0	0	0	-4833	-15

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 28-I-4 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
-------	----	----	----	----	----	----	---	---	---	---

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	4454	-6	-23258	14	112	-28	4950	4425	0	--
1	-4454	6	24931	-4	6792	31	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	4454	-6
1	0	0	0	0	0	0	-4454	6

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 29-I-1 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-47	4337	-22927	-811	-63	-401	4950	4425	0	--
1	47	-4337	24601	-5976	-11	397	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	-47	4337
1	0	0	0	0	0	0	47	-4337

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 29-I-2 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-0	4347	-23036	-306	-20	1905	4950	4425	0	--
1	0	-4347	24710	-6438	20	-1826	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	-0	4347
1	0	0	0	0	0	0	0	-4347

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Combinazione 29-I-3 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	48	4344	-23241	-819	79	-385	4950	4425	0	--
1	-48	-4344	24914	-5980	-3	382	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	48	4344
1	0	0	0	0	0	0	-48	-4344

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
1	--	--	--

Combinazione 29-I-4 (SISMAX_SLD)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	1	4332	-23124	-377	-46	-2165	4950	4425	0	--
1	-1	-4332	24797	-6361	48	2088	4950	4425	1550	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	0	0	0	0	0	0	1	4332
1	0	0	0	0	0	0	-1	-4332

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

Periodi di vibrazione e Masse modali

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Posizione masse 1

Numero di Frequenze calcolate =100, filtrate=31

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
				kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.4629	0.109	45.565	0	20360	0.00	78.81
2(3)	0.2932	-2.468	1.544	60	23	0.23	0.09
3(6)	0.1956	-0.022	-19.787	0	3839	0.00	14.86
4(9)	0.1803	-0.002	5.922	0	344	0.00	1.33
5(10)	0.1762	2.842	0.129	79	0	0.31	0.00
6(12)	0.1746	-5.833	0.200	334	0	1.29	0.00
7(13)	0.1721	-0.132	2.468	0	60	0.00	0.23
8(14)	0.1704	-4.384	-0.073	188	0	0.73	0.00
9(15)	0.1642	-4.365	0.163	187	0	0.72	0.00
10(18)	0.1599	3.417	0.066	114	0	0.44	0.00
11(19)	0.1581	26.945	-0.023	7120	0	27.56	0.00
12(24)	0.1404	-13.915	0.026	1899	0	7.35	0.00
13(28)	0.1378	9.026	0.037	799	0	3.09	0.00
14(29)	0.1348	-8.997	-0.035	794	0	3.07	0.00
15(30)	0.1348	2.958	-0.039	86	0	0.33	0.00
16(32)	0.1331	-28.521	0.001	7977	0	30.88	0.00
17(33)	0.1323	11.048	-0.008	1197	0	4.63	0.00
18(36)	0.0891	-0.004	-3.718	0	136	0.00	0.52
19(38)	0.0781	0.015	-1.965	0	38	0.00	0.15
20(42)	0.0645	0.002	-3.351	0	110	0.00	0.43
21(46)	0.0617	0.004	1.896	0	35	0.00	0.14
22(74)	0.0358	7.701	-0.003	582	0	2.25	0.00
23(75)	0.0354	5.430	0.005	289	0	1.12	0.00
24(78)	0.0350	2.909	-0.001	83	0	0.32	0.00
25(79)	0.0349	2.298	0.005	52	0	0.20	0.00
26(80)	0.0348	-2.932	-0.003	84	0	0.33	0.00
27(87)	0.0313	0.008	-1.890	0	35	0.00	0.14
28(89)	0.0305	-5.392	-0.001	285	0	1.10	0.00
29(90)	0.0302	5.649	0.005	313	0	1.21	0.00
30(94)	0.0298	-2.342	-0.002	54	0	0.21	0.00
31(95)	0.0296	2.658	-0.001	69	0	0.27	0.00
Somma delle Masse Modali [kgm*g]				22645	24981		
Masse strutturali libere [kgm*g]				25835	25835		
Percentuale				87.65	96.70	87.65	96.70

Posizione masse 2

Numero di Frequenze calcolate =100, filtrate=36

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
				kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
1(1)	0.4629	0.058	45.657	0	20442	0.00	79.13
2(2)	0.2607	0.388	-3.537	1	123	0.01	0.48
3(3)	0.2460	-0.804	2.988	6	88	0.02	0.34
4(5)	0.2400	1.374	2.123	19	44	0.07	0.17
5(6)	0.1935	-0.006	12.132	0	1443	0.00	5.59
6(7)	0.1919	0.154	-14.714	0	2123	0.00	8.22
7(9)	0.1858	0.004	-2.162	0	46	0.00	0.18
8(10)	0.1801	-0.002	-5.025	0	248	0.00	0.96
9(15)	0.1621	-7.543	0.002	558	0	2.16	0.00
10(16)	0.1593	14.002	-0.042	1923	0	7.44	0.00
11(19)	0.1549	7.923	-0.045	616	0	2.38	0.00
12(21)	0.1520	-12.819	-0.047	1611	0	6.24	0.00
13(22)	0.1499	19.341	-0.023	3669	0	14.20	0.00
14(24)	0.1466	-15.095	-0.019	2235	0	8.65	0.00
15(27)	0.1426	-18.422	0.014	3328	0	12.88	0.00
16(29)	0.1360	-10.529	0.625	1087	4	4.21	0.01
17(30)	0.1359	-6.899	-1.213	467	14	1.81	0.06
18(31)	0.1352	-12.323	0.158	1489	0	5.76	0.00
19(32)	0.1303	-1.723	-0.066	29	0	0.11	0.00
20(33)	0.1283	15.449	-0.054	2341	0	9.06	0.00
21(34)	0.1265	12.171	0.069	1453	0	5.62	0.00
22(36)	0.0859	0.009	-4.285	0	180	0.00	0.70
23(41)	0.0667	0.020	1.632	0	26	0.00	0.10
24(43)	0.0642	-0.001	2.219	0	48	0.00	0.19
25(61)	0.0531	0.004	-2.107	0	44	0.00	0.17
26(75)	0.0358	1.753	0.053	30	0	0.12	0.00
27(76)	0.0358	6.007	-0.018	354	0	1.37	0.00
28(79)	0.0350	-5.261	0.023	271	0	1.05	0.00
29(80)	0.0345	-2.692	0.004	71	0	0.28	0.00
30(82)	0.0341	-5.192	-0.000	264	0	1.02	0.00
31(84)	0.0332	3.841	-0.002	145	0	0.56	0.00
32(86)	0.0328	3.208	0.004	101	0	0.39	0.00
33(88)	0.0320	4.321	0.000	183	0	0.71	0.00
34(92)	0.0307	4.404	-0.000	190	0	0.74	0.00
35(97)	0.0294	-3.965	0.064	154	0	0.60	0.00
36(98)	0.0289	0.224	3.014	0	89	0.00	0.34
Somma delle Masse Modali [kgm*g]				22595	24963		
Masse strutturali libere [kgm*g]				25835	25835		
Percentuale				87.46	96.62	87.46	96.62

Posizione masse 3

Numero di Frequenze calcolate =100, filtrate=32

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
				kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.4627	0.062	45.599	0	20391	0.00	78.93
2(3)	0.2512	1.648	-1.274	27	16	0.10	0.06
3(6)	0.1953	-0.078	19.708	0	3809	0.00	14.74
4(9)	0.1802	-0.036	-5.997	0	353	0.00	1.36
5(10)	0.1761	2.949	-0.036	85	0	0.33	0.00
6(12)	0.1746	5.798	0.048	330	0	1.28	0.00
7(13)	0.1721	-0.013	-2.570	0	65	0.00	0.25
8(14)	0.1704	-4.371	0.033	187	0	0.73	0.00
9(15)	0.1641	4.513	-0.156	200	0	0.77	0.00
10(18)	0.1598	3.480	-0.063	119	0	0.46	0.00
11(19)	0.1581	26.942	0.017	7118	0	27.55	0.00
12(24)	0.1404	14.041	-0.059	1933	0	7.48	0.00
13(28)	0.1378	8.972	-0.019	789	0	3.06	0.00
14(29)	0.1348	-8.115	-0.057	646	0	2.50	0.00
15(30)	0.1348	-5.057	-0.010	251	0	0.97	0.00
16(32)	0.1331	-28.522	-0.003	7978	0	30.88	0.00
17(33)	0.1323	10.994	0.015	1185	0	4.59	0.00
18(36)	0.0890	0.017	-3.727	0	136	0.00	0.53
19(38)	0.0782	0.016	1.933	0	37	0.00	0.14
20(42)	0.0644	0.007	-3.361	0	111	0.00	0.43
21(46)	0.0617	-0.008	-1.809	0	32	0.00	0.12
22(48)	0.0611	0.019	-1.748	0	30	0.00	0.12
23(74)	0.0358	-7.699	0.003	581	0	2.25	0.00
24(75)	0.0354	-5.460	0.001	292	0	1.13	0.00
25(78)	0.0350	2.892	0.004	82	0	0.32	0.00
26(79)	0.0349	-2.401	0.007	57	0	0.22	0.00
27(80)	0.0348	-2.824	-0.006	78	0	0.30	0.00
28(87)	0.0312	0.007	1.665	0	27	0.00	0.11
29(89)	0.0305	-5.387	0.005	285	0	1.10	0.00
30(90)	0.0302	5.639	0.001	312	0	1.21	0.00
31(94)	0.0298	-2.329	-0.002	53	0	0.21	0.00
32(95)	0.0296	-2.688	-0.008	71	0	0.27	0.00

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
Somma delle Masse Modali [kgm*g]				22659	25006		
Masse strutturali libere [kgm*g]				25835	25835		
Percentuale				87.71	96.79	87.71	96.79

Posizione masse 4

Numero di Frequenze calcolate =100, filtrate=35

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
				kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.4643	0.116	45.675	0	20459	0.00	79.19
2(3)	0.2980	-2.485	1.513	61	22	0.23	0.09
3(4)	0.2549	-0.251	4.368	1	187	0.00	0.72
4(6)	0.1935	-0.098	-10.179	0	1016	0.00	3.93
5(7)	0.1921	0.084	-16.164	0	2562	0.00	9.92
6(9)	0.1858	-0.031	1.826	0	33	0.00	0.13
7(10)	0.1801	0.040	4.917	0	237	0.00	0.92
8(15)	0.1622	-7.170	0.200	504	0	1.95	0.00
9(16)	0.1594	14.187	-0.004	1974	0	7.64	0.00
10(19)	0.1549	8.007	0.097	629	0	2.43	0.00
11(21)	0.1520	-12.860	-0.009	1622	0	6.28	0.00
12(22)	0.1499	19.308	-0.002	3656	0	14.15	0.00
13(24)	0.1466	15.090	0.001	2233	0	8.64	0.00
14(27)	0.1426	-18.440	-0.004	3335	0	12.91	0.00
15(29)	0.1360	13.388	-0.003	1758	0	6.80	0.00
16(30)	0.1358	0.040	1.793	0	32	0.00	0.12
17(31)	0.1352	11.447	-0.002	1285	0	4.97	0.00
18(32)	0.1303	1.760	-0.000	30	0	0.12	0.00
19(33)	0.1283	15.543	0.001	2369	0	9.17	0.00
20(34)	0.1264	12.046	0.001	1423	0	5.51	0.00
21(36)	0.0860	0.008	-4.295	0	181	0.00	0.70
22(43)	0.0642	-0.002	2.167	0	46	0.00	0.18
23(61)	0.0531	-0.001	2.143	0	45	0.00	0.17
24(75)	0.0358	2.768	0.046	75	0	0.29	0.00
25(76)	0.0358	5.590	-0.031	306	0	1.19	0.00
26(78)	0.0350	-2.102	0.162	43	0	0.17	0.00
27(79)	0.0350	4.884	0.085	234	0	0.91	0.00
28(80)	0.0345	2.745	0.001	74	0	0.29	0.00
29(82)	0.0341	-5.175	-0.001	263	0	1.02	0.00
30(84)	0.0332	3.851	0.001	145	0	0.56	0.00
31(86)	0.0328	-3.195	-0.002	100	0	0.39	0.00
32(88)	0.0320	4.313	0.001	182	0	0.71	0.00
33(92)	0.0307	-4.419	0.001	191	0	0.74	0.00
34(97)	0.0294	3.962	0.124	154	0	0.60	0.00
35(98)	0.0289	-0.472	2.920	2	84	0.01	0.32
Somma delle Masse Modali [kgm*g]				22650	24905		
Masse strutturali libere [kgm*g]				25835	25835		
Percentuale				87.67	96.40	87.67	96.40

Risultati Analisi Dinamica - Spostamenti massimi - Nodi

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	mrads	mrads	mrads
2	-0.28(1)	5.32(13-I-4)	-0.34(1)	-5.10(13-II-4)	0.23(1)	2.29(13-I-4)
4	-0.24(1)	8.72(13-I-4)	-0.78(1)	-6.46(13-II-4)	0.34(1)	3.34(13-I-4)
5	-0.15(12-II-1)	14.91(13-I-4)	-1.29(1)	-8.41(1)	0.19(1)	2.56(13-I-2)
6	-0.06(12-II-1)	16.98(13-I-3)	-1.50(1)	-9.33(1)	0.01(12-II-1)	-0.42(13-I-4)
7	0.15(12-I-1)	14.62(13-I-2)	-1.29(1)	-8.33(1)	-0.18(1)	-2.68(13-I-4)
8	0.24(1)	8.16(13-I-2)	-0.78(1)	-6.30(13-II-2)	-0.34(1)	-3.43(13-I-2)
9	0.28(1)	-4.78(13-II-2)	-0.34(1)	-4.98(13-II-2)	-0.22(1)	-2.25(13-I-2)
11	-1.61(12-II-4)	5.34(13-I-4)	-6.46(1)	-5.50(1)	0.30(1)	1.35(12-II-4)
12	-1.76(13-I-4)	8.73(13-I-4)	-8.53(1)	-6.15(1)	0.46(1)	1.34(12-II-4)
13	-1.31(13-I-2)	14.91(13-I-4)	-10.88(1)	-6.86(1)	0.25(1)	1.13(12-II-1)
14	1.02(12-I-1)	16.99(13-I-3)	-11.72(1)	-7.11(1)	0.01(12-II-4)	1.03(12-II-1)
15	1.36(13-I-4)	14.62(13-I-2)	-10.82(1)	-6.83(1)	-0.25(1)	-1.11(12-I-2)
16	1.80(13-I-2)	8.16(13-I-2)	-8.43(1)	-6.09(1)	-0.46(1)	-1.33(12-I-2)
17	1.58(12-I-2)	-4.77(13-II-2)	-6.43(1)	-5.48(1)	-0.30(1)	-1.33(12-I-2)
18	-2.47(12-II-4)	5.35(13-I-4)	-9.53(1)	1.58(13-II-4)	0.38(1)	1.08(13-II-4)

COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
19	-2.39(12-II-4)	8.73(13-I-4)	-11.68(1)	1.53(13-II-4)	0.57(1)	1.54(13-II-4)
20	-1.96(12-II-1)	14.92(13-I-4)	-14.09(1)	1.62(13-II-4)	0.31(1)	1.18(13-II-2)
21	1.68(12-I-1)	16.99(13-I-3)	-14.97(1)	1.59(13-II-1)	-0.01(12-I-4)	0.19(13-I-4)
22	1.93(12-I-2)	14.63(13-I-2)	-14.02(1)	1.61(13-II-2)	-0.31(1)	-1.19(13-II-4)
23	2.40(12-I-2)	8.17(13-I-2)	-11.55(1)	1.51(13-II-2)	-0.57(1)	-1.55(13-II-2)
24	2.43(12-I-2)	-4.76(13-II-2)	-9.48(1)	1.55(13-II-2)	-0.38(1)	-1.08(13-II-2)
25	-1.63(12-II-4)	5.36(13-I-4)	-5.50(1)	5.63(1)	0.45(1)	1.32(12-I-4)
26	-1.56(12-II-4)	8.73(13-I-4)	-7.03(1)	6.24(1)	0.69(1)	1.24(12-I-4)
27	-1.26(12-II-1)	14.92(13-I-4)	-8.75(1)	6.89(1)	0.37(1)	1.08(12-I-4)
28	-0.99(12-II-3)	17.00(13-I-3)	-9.42(1)	7.09(1)	-0.01(12-I-4)	1.02(12-I-1)
29	1.23(12-I-1)	14.63(13-I-2)	-8.70(1)	6.86(1)	-0.37(1)	-1.07(12-II-2)
30	1.56(13-II-2)	8.17(13-I-2)	-6.93(1)	6.18(1)	-0.69(1)	-1.23(12-II-2)
31	1.60(12-I-2)	-4.75(13-II-2)	-5.45(1)	5.62(1)	-0.46(1)	-1.34(12-II-2)
33	-0.71(1)	5.37(13-I-4)	-0.82(1)	1.85(13-I-4)	0.53(1)	-1.77(13-II-4)
34	-0.61(1)	8.73(13-I-4)	-1.91(1)	1.08(13-I-4)	0.81(1)	-2.80(13-II-4)
35	-0.34(12-II-4)	14.92(13-I-4)	-3.20(1)	0.47(13-I-4)	0.43(1)	-2.10(13-II-2)
36	0.09(12-I-4)	16.99(13-I-3)	-3.75(1)	0.26(13-I-3)	-0.01(12-I-4)	-0.33(13-I-4)
37	0.34(12-I-2)	14.62(13-I-2)	-3.19(1)	0.45(13-I-2)	-0.43(1)	-2.17(13-I-4)
38	0.61(1)	8.17(13-I-2)	-1.90(1)	1.00(13-I-2)	-0.81(1)	-2.85(13-I-2)
39	0.71(1)	4.76(13-I-2)	-0.81(1)	1.76(13-I-2)	-0.54(1)	-1.74(13-I-2)
41	-1.59(12-II-4)	5.38(13-I-4)	-5.46(1)	-5.66(1)	0.45(1)	-1.34(12-I-4)
42	-1.55(12-II-4)	8.74(13-I-4)	-6.89(1)	-6.19(1)	0.69(1)	-1.24(12-I-4)
43	-1.24(12-II-3)	14.92(13-I-4)	-8.65(1)	-6.85(1)	0.37(1)	-1.08(12-I-4)
44	1.00(12-I-1)	17.00(13-I-3)	-9.37(1)	-7.06(1)	-0.01(12-I-4)	1.03(12-II-1)
45	1.25(12-I-3)	14.63(13-I-2)	-8.67(1)	-6.85(1)	-0.37(1)	1.09(12-II-2)
46	1.57(13-I-2)	8.18(13-I-2)	-6.92(1)	-6.18(1)	-0.69(1)	1.25(12-II-2)
47	1.61(12-I-2)	4.77(13-I-2)	-5.45(1)	-5.62(1)	-0.46(1)	1.34(12-II-2)
48	-2.42(12-II-4)	5.39(13-I-4)	-9.56(1)	-1.66(13-I-4)	0.38(1)	-1.08(13-I-4)
49	-2.40(12-II-4)	8.74(13-I-4)	-11.55(1)	-1.58(13-I-4)	0.57(1)	-1.53(13-I-4)
50	-1.95(12-II-3)	14.92(13-I-4)	-13.99(1)	-1.64(13-I-4)	0.31(1)	-1.16(13-I-2)
51	-1.67(12-II-1)	17.00(13-I-3)	-14.91(1)	-1.60(13-I-3)	-0.01(12-I-4)	0.19(13-I-4)
52	1.95(12-I-3)	14.63(13-I-2)	-13.99(1)	-1.62(13-I-2)	-0.31(1)	1.22(13-I-4)
53	2.40(12-I-2)	8.18(13-I-2)	-11.54(1)	-1.51(13-I-2)	-0.57(1)	1.57(13-I-2)
54	2.43(12-I-2)	4.78(13-I-2)	-9.48(1)	-1.56(13-I-2)	-0.38(1)	1.09(13-I-2)
55	-1.57(12-II-4)	5.40(13-I-4)	-6.53(1)	5.50(1)	0.30(1)	-1.32(12-II-4)
56	-1.78(13-II-4)	8.75(13-I-4)	-8.48(1)	6.08(1)	0.46(1)	-1.34(12-II-4)
57	-1.33(13-II-2)	14.92(13-I-4)	-10.82(1)	6.81(1)	0.25(1)	-1.12(12-II-4)
58	-1.02(12-II-3)	17.00(13-I-3)	-11.68(1)	7.08(1)	-0.01(12-I-4)	1.02(12-I-3)
59	1.34(13-II-4)	14.63(13-I-2)	-10.80(1)	6.82(1)	-0.25(1)	1.13(12-I-2)
60	1.79(13-II-2)	8.19(13-I-2)	-8.43(1)	6.09(1)	-0.46(1)	1.34(12-I-2)
61	1.57(12-I-2)	4.79(13-I-2)	-6.43(1)	5.47(1)	-0.30(1)	1.33(12-I-2)
63	-0.28(1)	5.41(13-I-4)	-0.34(1)	5.36(13-I-4)	0.22(1)	-2.23(13-II-4)
64	-0.24(1)	8.75(13-I-4)	-0.78(1)	6.54(13-I-4)	0.34(1)	-3.37(13-II-4)
65	-0.15(12-II-3)	14.91(13-I-4)	-1.29(1)	8.35(1)	0.18(1)	-2.60(13-II-2)
66	0.06(12-I-3)	17.00(13-I-3)	-1.51(1)	9.29(1)	0.00(12-II-3)	-0.42(13-I-4)
67	0.15(12-I-3)	14.62(13-I-2)	-1.29(1)	8.31(1)	-0.18(1)	2.63(13-II-4)
68	0.24(1)	8.19(13-I-2)	-0.78(1)	6.30(13-I-2)	-0.34(1)	3.40(13-II-2)
69	0.28(1)	4.80(13-I-2)	-0.34(1)	4.99(13-I-2)	-0.22(1)	2.22(13-II-2)
101	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
102	0.01(12-I-1)	0.41(13-I-4)	-0.24(1)	2.37(13-I-4)	0.76(1)	2.76(13-I-4)
103	-11.38(13-II-4)	-0.67(13-II-4)	-28.07(13-I-4)	7.70(13-I-4)	2.03(1)	-3.11(13-II-4)
104	0.05(12-I-1)	7.13(13-I-4)	-0.71(1)	-4.05(13-II-4)	0.24(1)	6.67(13-I-4)
105	0.07(12-I-1)	18.95(13-I-4)	-1.25(1)	-6.68(13-II-4)	0.18(1)	5.07(13-I-2)
106	-0.04(12-II-1)	23.54(13-I-1)	-1.48(1)	-7.49(13-II-3)	0.00(12-II-1)	-0.38(13-I-4)
107	-0.07(12-II-1)	18.58(13-I-2)	-1.25(1)	-6.53(13-II-2)	-0.18(1)	-5.23(13-I-4)
108	-0.05(12-II-1)	6.57(13-I-2)	-0.72(1)	-3.78(13-II-2)	-0.24(1)	-6.59(13-I-2)
109	-0.01(12-II-1)	0.27(13-I-2)	-0.25(1)	1.68(13-I-2)	-0.79(1)	-2.02(13-I-2)
110	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
132	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
133	0.02(1)	-0.26(13-II-4)	-0.59(1)	2.27(13-I-4)	1.85(1)	-1.59(13-II-4)
134	0.12(1)	-4.48(13-II-4)	-1.75(1)	3.40(13-I-4)	0.61(1)	4.49(13-I-4)
135	0.14(12-I-4)	12.51(13-I-4)	-3.10(1)	1.95(13-I-4)	0.49(1)	3.76(13-I-2)
136	-0.06(12-II-2)	15.70(13-I-3)	-3.68(1)	0.88(13-I-2)	-0.01(12-I-4)	-0.41(13-II-4)
137	-0.15(12-II-2)	12.34(13-I-2)	-3.09(1)	1.82(13-I-2)	-0.49(1)	-3.80(13-I-4)
138	-0.12(1)	4.17(13-I-2)	-1.74(1)	2.98(13-I-2)	-0.62(1)	-4.42(13-I-2)
139	-0.02(1)	0.18(13-I-2)	-0.58(1)	1.27(13-I-2)	-1.81(1)	-1.15(13-I-2)
140	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
162	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)
163	0.01(12-I-3)	-0.31(13-II-4)	-0.25(1)	-1.72(13-II-4)	0.78(1)	-2.12(13-II-4)
164	0.05(12-I-3)	-6.63(13-II-4)	-0.72(1)	4.12(13-I-4)	0.24(1)	-6.55(13-II-4)
165	0.07(12-I-3)	-18.46(13-II-4)	-1.25(1)	6.72(13-I-4)	0.18(1)	-5.13(13-II-2)
166	0.04(12-I-3)	-23.22(13-II-3)	-1.48(1)	7.49(13-I-1)	0.00(12-II-4)	-0.32(13-I-4)
167	-0.07(12-II-3)	-18.40(13-II-2)	-1.25(1)	6.54(13-I-2)	-0.18(1)	5.15(13-II-4)
168	-0.05(12-II-3)	-6.52(13-II-2)	-0.72(1)	3.80(13-I-2)	-0.24(1)	6.54(13-II-2)
169	-0.01(12-II-3)	-0.27(13-II-2)	-0.25(1)	-1.68(13-II-2)	-0.79(1)	2.00(13-II-2)
170	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)	0.00(1)

Risultati Analisi Dinamica - Reazioni massime - Nodi

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Nodo	Rx kg	Ry kg	Rz kg	Mx kg*m	My kg*m	Mz kg*m
101	-2371(12-I-1)	-1635(13-I-4)	3775(1)	-498(13-I-4)	-739(1)	-1172(13-I-4)
110	2395(12-II-1)	1186(13-II-2)	3854(1)	-354(13-I-2)	758(1)	765(13-I-2)
132	-5481(1)	1720(13-II-4)	9205(1)	-477(13-I-4)	-1801(1)	770(13-II-4)
140	5458(1)	-966(13-I-2)	9101(1)	-266(13-I-2)	1773(1)	525(13-I-2)
162	-2402(12-I-3)	1099(13-II-4)	3824(1)	363(13-II-4)	-753(1)	881(13-II-4)
170	2392(12-II-3)	-1188(13-I-2)	3850(1)	353(13-II-2)	757(1)	-761(13-II-2)

VERIFICHE STATO LIMITE ULTIMO

Verifica Stabilità aste Metalliche

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Asta : 701 [102 , 104]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1868	-66	784	80960	2800	2800	31	31	0.965	0.965	--	0.583	0.297	0.350	0.494

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1868	39	232	74419	2667	2667	(12+13)-VIII-1	7.9
1	Z	1868	23	387	74419	2667	2667	(12+13)-VIII-1	5.6

Asta : 701 [104 , 105]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
162	26	-331	80960	2800	2800	47	47	0.911	0.911	--	0.400	0.243	0.240	0.405

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	162	10	80	70211	2667	2667	(12+13)-VIII-1	27
1	Z	162	6	134	70211	2667	2667	(12+13)-VIII-1	18

Asta : 701 [105 , 106]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1500	-12	-322	80960	2800	2800	47	47	0.911	0.911	--	0.403	0.516	0.242	0.861

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1500	5	166	70211	2667	2667	(12+13)-IV-3	12
1	Z	1500	3	277	70211	2667	2667	(12+13)-IV-3	7.9

Asta : 701 [106 , 107]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1497	-12	-327	80960	2800	2800	47	47	0.911	0.911	--	0.403	0.508	0.242	0.847

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1497	5	166	70211	2667	2667	(12+13)-II-1	12
1	Z	1497	3	277	70211	2667	2667	(12+13)-II-1	7.9

Asta : 701 [107 , 108]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
165	27	-329	80960	2800	2800	47	47	0.911	0.911	--	0.400	0.240	0.240	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	165	11	79	70211	2667	2667	(12+13)-VI-3	28
1	Z	165	6	132	70211	2667	2667	(12+13)-VI-3	18

Asta : 701 [108 , 109]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1892	-73	818	80960	2800	2800	31	31	0.965	0.965	--	0.572	0.326	0.343	0.543

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1892	42	266	74419	2667	2667	(12+13)-VIII-3	7.1
1	Z	1892	25	444	74419	2667	2667	(12+13)-VIII-3	5.0

Asta : 701 [101 , 102]

Sez. G: Tubo100x100x8 L=25.0 cm Ln1=25.0 cm Ln2=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=30.160

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
2000	620	1168	80960	2800	2800	7	7	1.000	1.000	--	0.485	0.514	0.291	0.856

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2000	300	600	77105	2667	2667	(12+13)-IV-1	2.8
1	Z	2000	180	1000	77105	2667	2667	(12+13)-IV-1	2.1

Asta : 701 [109 , 110]

Sez. G: Tubo100x100x8 L=25.0 cm Ln1=25.0 cm Ln2=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=30.160

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
2069	644	767	80960	2800	2800	7	7	1.000	1.000	--	0.486	0.560	0.292	0.933

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2069	313	429	77105	2667	2667	(12+13)-VI-3	3.3
1	Z	2069	188	715	77105	2667	2667	(12+13)-VI-3	2.7

Asta : 702 [133 , 134]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
4333	-152	542	80960	2800	2800	31	31	0.965	0.965	--	0.592	0.329	0.355	0.548

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4333	90	178	74419	2667	2667	(12+13)-VIII-1	6.3
1	Z	4333	54	297	74419	2667	2667	(12+13)-VIII-1	5.3

Asta : 702 [134 , 135]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
415	51	-208	80960	2800	2800	47	47	0.911	0.911	--	0.401	0.241	0.240	0.401

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	415	20	50	70211	2667	2667	(12+13)-VIII-1	31
1	Z	415	12	84	70211	2667	2667	(12+13)-VIII-1	24

Asta : 702 [135 , 136]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-3518	-31	-228	80960	2800	2800	47	47	0.911	0.911	--	0.530	0.544	0.318	0.906

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3518	17	124	70211	2667	2667	(12+13)-VIII-3	9.7
1	Z	3518	10	206	70211	2667	2667	(12+13)-VIII-3	7.6

Asta : 702 [136 , 137]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-3512	-31	225	80960	2800	2800	47	47	0.911	0.911	--	0.528	0.539	0.317	0.899

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3512	17	122	70211	2667	2667	(12+13)-II-2	9.8
1	Z	3512	10	203	70211	2667	2667	(12+13)-II-2	7.7

Asta : 702 [137 , 138]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
433	50	197	80960	2800	2800	47	47	0.911	0.911	--	0.401	0.241	0.241	0.401

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	433	20	47	70211	2667	2667	(12+13)-VI-4	32
1	Z	433	12	79	70211	2667	2667	(12+13)-VI-4	25

Asta : 702 [138 , 139]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
4316	-138	542	80960	2800	2800	31	31	0.965	0.965	--	0.604	0.336	0.362	0.561

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4316	83	182	74419	2667	2667	(12+13)-II-3	6.3
1	Z	4316	50	304	74419	2667	2667	(12+13)-II-3	5.2

Asta : 702 [132 , 133]

Sez. G: Tubo100x100x8 L=25.0 cm Ln1=25.0 cm Ln2=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=30.160

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
4447	1380	-766	80960	2800	2800	7	7	1.000	1.000	--	0.488	0.461	0.293	0.768

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4447	674	353	77105	2667	2667	(12+13)-VIII-2	2.3
1	Z	4447	404	588	77105	2667	2667	(12+13)-VIII-2	2.3

Asta : 702 [139 , 140]

Sez. G: Tubo100x100x8 L=25.0 cm Ln1=25.0 cm Ln2=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=30.160

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
4528	1383	-521	80960	2800	2800	7	7	1.000	1.000	--	0.486	0.487	0.291	0.812

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4528	672	254	77105	2667	2667	(12+13)-II-4	2.5
1	Z	4528	403	423	77105	2667	2667	(12+13)-II-4	2.7

Asta : 703 [163 , 164]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1886	-73	-805	80960	2800	2800	31	31	0.965	0.965	--	0.572	0.324	0.343	0.540

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1886	42	261	74419	2667	2667	(12+13)-II-2	7.2

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Z	1886	25	435	74419	2667	2667	(12+13)-II-2	5.1

Asta : 703 [164 , 165]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
161	27	330	80960	2800	2800	47	47	0.911	0.911	--	0.400	0.240	0.240	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	161	11	79	70211	2667	2667	(12+13)-IV-2	28
1	Z	161	6	132	70211	2667	2667	(12+13)-IV-2	18

Asta : 703 [165 , 166]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1498	-12	324	80960	2800	2800	47	47	0.911	0.911	--	0.403	0.512	0.242	0.853

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1498	5	166	70211	2667	2667	(12+13)-VIII-4	12
1	Z	1498	3	277	70211	2667	2667	(12+13)-VIII-4	7.9

Asta : 703 [166 , 167]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1503	-12	325	80960	2800	2800	47	47	0.911	0.911	--	0.403	0.510	0.242	0.851

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1503	5	166	70211	2667	2667	(12+13)-VI-2	12
1	Z	1503	3	276	70211	2667	2667	(12+13)-VI-2	7.9

Asta : 703 [167 , 168]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
161	27	329	80960	2800	2800	47	47	0.911	0.911	--	0.400	0.240	0.240	0.400

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	161	11	79	70211	2667	2667	(12+13)-II-4	28
1	Z	161	6	132	70211	2667	2667	(12+13)-II-4	18

Asta : 703 [168 , 169]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1886	-73	-812	80960	2800	2800	31	31	0.965	0.965	--	0.572	0.325	0.343	0.542

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1886	42	264	74419	2667	2667	(12+13)-IV-4	7.1
1	Z	1886	25	440	74419	2667	2667	(12+13)-IV-4	5.0

Asta : 703 [162 , 163]

Sez. G: Tubo100x100x8 L=25.0 cm Ln1=25.0 cm Ln2=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=30.160

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
2097	645	-878	80960	2800	2800	7	7	1.000	1.000	--	0.486	0.522	0.292	0.870

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2097	314	459	77105	2667	2667	(12+13)-VIII-2	3.2
1	Z	2097	188	765	77105	2667	2667	(12+13)-VIII-2	2.6

Asta : 703 [169 , 170]

Sez. G: Tubo100x100x8 L=25.0 cm Ln1=25.0 cm Ln2=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

SF_λ=30.160

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
2088	646	-758	80960	2800	2800	7	7	1.000	1.000	--	0.486	0.561	0.292	0.934

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2088	314	425	77105	2667	2667	(12+13)-VI-4	3.3
1	Z	2088	188	709	77105	2667	2667	(12+13)-VI-4	2.8

Asta : 704 [103 , 133]

Sez. G: Tubo100x100x8 L=442.8 cm Ln1=442.8 cm Ln2=442.8 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=1.703

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	299	-88	80960	2800	2800	117	117	0.442	0.442	--	0.600	0.360	0.360	0.600

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	179	32	34058	2667	2667	(12+13)-IV-1	13
1	Z	0	108	53	34058	2667	2667	(12+13)-IV-1	17

Asta : 704 [133 , 163]

Sez. G: Tubo100x100x8 L=442.5 cm Ln1=442.5 cm Ln2=442.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=1.704

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1217	259	-120	80960	2800	2800	117	117	0.442	0.442	--	0.411	0.252	0.247	0.420

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1217	107	30	34094	2667	2667	(12+13)-IV-1	11
1	Z	1217	64	50	34094	2667	2667	(12+13)-IV-1	13

Asta : 705 [109 , 139]

Sez. G: Tubo100x100x8 L=442.5 cm Ln1=442.5 cm Ln2=442.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=1.704

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1239	226	206	80960	2800	2800	117	117	0.442	0.442	--	0.412	0.252	0.247	0.420

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1239	93	52	34094	2667	2667	(12+13)-VI-1	11
1	Z	1239	56	86	34094	2667	2667	(12+13)-VI-1	11

Asta : 705 [139 , 169]

Sez. G: Tubo100x100x8 L=442.5 cm Ln1=442.5 cm Ln2=442.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=1.704

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1233	226	204	80960	2800	2800	117	117	0.442	0.442	--	0.412	0.252	0.247	0.420

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1233	93	52	34094	2667	2667	(12+13)-II-2	11
1	Z	1233	56	86	34094	2667	2667	(12+13)-II-2	11

Asta : 8000 [2 , 4]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
1573	37	-304	80960	2800	2800	31	31	0.965	0.965	--	0.401	0.241	0.241	0.401

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1573	15	73	74419	2667	2667	(12+13)-VIII-4	19
1	Z	1573	9	122	74419	2667	2667	(12+13)-VIII-4	14

Asta : 8000 [4 , 5]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
2907	-9	366	80960	2800	2800	47	47	0.911	0.911	--	0.406	0.245	0.243	0.408

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2907	4	90	70211	2667	2667	(12+13)-IV-4	13
1	Z	2907	2	149	70211	2667	2667	(12+13)-IV-4	10

Asta : 8000 [5 , 6]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3645	-11	257	80960	2800	2800	47	47	0.911	0.911	--	0.407	0.362	0.244	0.604

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3645	4	93	70211	2667	2667	(12+13)-II-4	11
1	Z	3645	3	155	70211	2667	2667	(12+13)-II-4	9.0

Asta : 8000 [6 , 7]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3647	-11	259	80960	2800	2800	47	47	0.911	0.911	--	0.407	0.365	0.244	0.608

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3647	5	95	70211	2667	2667	(12+13)-IV-2	11
1	Z	3647	3	158	70211	2667	2667	(12+13)-IV-2	8.9

Asta : 8000 [7 , 8]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3132	-9	369	80960	2800	2800	47	47	0.911	0.911	--	0.406	0.245	0.244	0.409

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3132	4	90	70211	2667	2667	(12+13)-II-2	13
1	Z	3132	2	151	70211	2667	2667	(12+13)-II-2	9.8

Asta : 8000 [8 , 9]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1687	47	243	80960	2800	2800	31	31	0.965	0.965	--	0.401	0.304	0.241	0.507

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1687	19	74	74419	2667	2667	(12+13)-VI-3	17
1	Z	1687	11	123	74419	2667	2667	(12+13)-VI-3	14

Asta : 8001 [2 , 102]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cmq: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
3770	628	129	80960	2800	2800	41	41	0.932	0.932	--	0.480	0.244	0.407

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3770	301	32	71883	2667	2667	1	5.6
1	Z	3770	181	53	71883	2667	2667	1	7.1

Asta : 8002 [4 , 104]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
2085	568	-33	80960	2800	2800	41	41	0.932	0.932	--	0.578	0.242	0.404

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2085	329	8	71883	2667	2667	(12+13)-IV-1	6.4
1	Z	2085	197	13	71883	2667	2667	(12+13)-IV-1	9.3

Asta : 8003 [5 , 105]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
1223	337	-18	80960	2800	2800	41	41	0.932	0.932	--	0.634	0.241	0.402

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1223	213	4	71883	2667	2667	(12+13)-IV-1	10
1	Z	1223	128	7	71883	2667	2667	(12+13)-IV-1	15

Asta : 8004 [6 , 106]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
697	267	-1	80960	2800	2800	41	41	0.932	0.932	--	0.545	0.241	0.401

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	697	145	0	71883	2667	2667	(12+13)-VIII-3	16
1	Z	697	87	0	71883	2667	2667	(12+13)-VIII-3	24

Asta : 8005 [7 , 107]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
1224	343	18	80960	2800	2800	41	41	0.932	0.932	--	0.628	0.241	0.402

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1224	216	4	71883	2667	2667	(12+13)-II-3	10
1	Z	1224	129	7	71883	2667	2667	(12+13)-II-3	15

Asta : 8006 [8 , 108]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
2471	496	39	80960	2800	2800	41	41	0.932	0.932	--	0.624	0.243	0.405

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2471	310	10	71883	2667	2667	1	6.5
1	Z	2471	186	16	71883	2667	2667	1	9.1

Asta : 8007 [9 , 109]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3778	618	-135	80960	2800	2800	41	41	0.932	0.932	--	0.464	0.244	0.278	0.407

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3778	287	33	71883	2667	2667	1	5.8
1	Z	3778	172	55	71883	2667	2667	1	7.3

Asta : 8008 [2 , 104]

Sez. G: Tubo100x100x8 L=193.0 cm Ln1=193.0 cm Ln2=193.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.907

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-3363	8	192	80960	2800	2800	51	51	0.894	0.894	--	0.408	0.370	0.245	0.617

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3363	3	71	68921	2667	2667	1	13
1	Z	3363	2	118	68921	2667	2667	1	11

Asta : 8009 [4 , 105]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2386	-12	83	80960	2800	2800	63	63	0.838	0.838	--	0.543	0.395	0.326	0.658

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2386	6	33	64626	2667	2667	1	19
1	Z	2386	4	54	64626	2667	2667	1	17

Asta : 8010 [5 , 106]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-742	-9	-153	80960	2800	2800	63	63	0.838	0.838	--	0.937	0.429	0.562	0.716

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	742	9	66	64626	2667	2667	(12+13)-II-1	25
1	Z	742	5	109	64626	2667	2667	(12+13)-II-1	18

Asta : 8011 [7 , 106]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-743	-9	150	80960	2800	2800	63	63	0.838	0.838	--	0.936	0.423	0.562	0.706

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	743	9	63	64626	2667	2667	(12+13)-IV-3	26
1	Z	743	5	106	64626	2667	2667	(12+13)-IV-3	19

Asta : 8012 [8 , 107]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2385	-12	-90	80960	2800	2800	63	63	0.838	0.838	--	0.536	0.391	0.322	0.651

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	2385	6	35	64626	2667	2667	1	19
1	Z	2385	4	58	64626	2667	2667	1	17

Asta : 8013 [9 , 108]

Sez. G: Tubo100x100x8 L=193.0 cm Ln1=193.0 cm Ln2=193.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.907

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3371	8	-195	80960	2800	2800	51	51	0.894	0.894	--	0.408	0.370	0.617

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3371	3	72	68921	2667	2667	1	13
1	Z	3371	2	120	68921	2667	2667	1	11

Asta : 8014 [33 , 34]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
4023	113	453	80960	2800	2800	31	31	0.965	0.965	--	0.403	0.241	0.402

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4023	45	109	74419	2667	2667	(12+13)-VIII-1	8.9
1	Z	4023	27	182	74419	2667	2667	(12+13)-VIII-1	7.5

Asta : 8014 [34 , 35]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
7620	-33	-443	80960	2800	2800	47	47	0.911	0.911	--	0.415	0.253	0.421

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7620	14	112	70211	2667	2667	(12+13)-VIII-1	6.4
1	Z	7620	8	186	70211	2667	2667	(12+13)-VIII-1	5.5

Asta : 8014 [35 , 36]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
8854	-32	-235	80960	2800	2800	47	47	0.911	0.911	--	0.477	0.391	0.652

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	8854	15	92	70211	2667	2667	(12+13)-IV-1	6.0
1	Z	8854	9	153	70211	2667	2667	(12+13)-IV-1	5.3

Asta : 8014 [36 , 37]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
8854	-32	-306	80960	2800	2800	47	47	0.911	0.911	--	0.477	0.278	0.463

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	8854	15	85	70211	2667	2667	(12+13)-IV-3	6.1
1	Z	8854	9	142	70211	2667	2667	(12+13)-IV-3	5.5

Asta : 8014 [37 , 38]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
8854	-32	-306	80960	2800	2800	47	47	0.911	0.911	--	0.477	0.278	0.463

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
7612	-33	450	80960	2800	2800	47	47	0.911	0.911	--	0.415	0.253	0.249	0.421

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7612	14	114	70211	2667	2667	(12+13)-II-4	6.4
1	Z	7612	8	189	70211	2667	2667	(12+13)-II-4	5.5

Asta : 8014 [38 , 39]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3978	110	457	80960	2800	2800	31	31	0.965	0.965	--	0.403	0.241	0.242	0.402

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3978	45	110	74419	2667	2667	(12+13)-VI-3	9.0
1	Z	3978	27	184	74419	2667	2667	(12+13)-VI-3	7.6

Asta : 8015 [33 , 133]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
7072	518	240	80960	2800	2800	41	41	0.932	0.932	--	0.411	0.248	0.246	0.414

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7072	213	60	71883	2667	2667	(12+13)-IV-2	5.0
1	Z	7072	128	99	71883	2667	2667	(12+13)-IV-2	5.4

Asta : 8016 [34 , 134]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
4912	337	-70	80960	2800	2800	41	41	0.932	0.932	--	0.525	0.246	0.315	0.409

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4912	177	17	71883	2667	2667	(12+13)-VIII-1	7.1
1	Z	4912	106	29	71883	2667	2667	(12+13)-VIII-1	8.4

Asta : 8017 [35 , 135]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3098	215	46	80960	2800	2800	41	41	0.932	0.932	--	0.514	0.244	0.308	0.406

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3098	111	11	71883	2667	2667	(12+13)-VIII-1	11
1	Z	3098	66	19	71883	2667	2667	(12+13)-VIII-1	13

Asta : 8018 [36 , 136]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1946	148	-2	80960	2800	2800	41	41	0.932	0.932	--	0.403	0.242	0.242	0.404

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1946	60	0	71883	2667	2667	(12+13)-IV-3	20
1	Z	1946	36	1	71883	2667	2667	(12+13)-IV-3	25

Asta : 8019 [37 , 137]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
3080	211	-46	80960	2800	2800	41	41	0.932	0.932	--	0.499	0.244	0.406

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3080	105	11	71883	2667	2667	(12+13)-VI-3	12
1	Z	3080	63	19	71883	2667	2667	(12+13)-VI-3	14

Asta : 8020 [38 , 138]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
4882	321	70	80960	2800	2800	41	41	0.932	0.932	--	0.498	0.246	0.409

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4882	160	17	71883	2667	2667	(12+13)-II-3	7.4
1	Z	4882	96	29	71883	2667	2667	(12+13)-II-3	8.7

Asta : 8021 [39 , 139]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
7096	500	-238	80960	2800	2800	41	41	0.932	0.932	--	0.411	0.248	0.414

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7096	205	59	71883	2667	2667	(12+13)-VI-4	5.1
1	Z	7096	123	98	71883	2667	2667	(12+13)-VI-4	5.5

Asta : 8022 [33 , 134]

Sez. G: Tubo100x100x8 L=193.0 cm Ln1=193.0 cm Ln2=193.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.907

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-8220	19	-17	80960	2800	2800	51	51	0.894	0.894	--	0.419	0.385	0.641

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	8220	8	6	68921	2667	2667	1	8.0
1	Z	8220	5	11	68921	2667	2667	1	8.0

Asta : 8023 [34 , 135]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6082	-20	5	80960	2800	2800	63	63	0.838	0.838	--	0.420	0.259	0.432

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6082	8	1	64626	2667	2667	1	10
1	Z	6082	5	2	64626	2667	2667	1	10

Asta : 8024 [35 , 136]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1713	-17	124	80960	2800	2800	63	63	0.838	0.838	--	0.565	0.423	0.705

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1713	10	53	64626	2667	2667	(12+13)-II-2	20
1	Z	1713	6	88	64626	2667	2667	(12+13)-II-2	16

Asta : 8025 [37 , 136]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1721	-17	126	80960	2800	2800	63	63	0.838	0.838	--	0.567	0.423	0.340	0.705

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1721	10	53	64626	2667	2667	(12+13)-VIII-3	20
1	Z	1721	6	89	64626	2667	2667	(12+13)-VIII-3	16

Asta : 8026 [38 , 137]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-6091	-20	1	80960	2800	2800	63	63	0.838	0.838	--	0.420	0.339	0.252	0.565

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6091	8	0	64626	2667	2667	1	10
1	Z	6091	5	1	64626	2667	2667	1	10

Asta : 8027 [39 , 138]

Sez. G: Tubo100x100x8 L=193.0 cm Ln1=193.0 cm Ln2=193.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.907

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-8206	18	0	80960	2800	2800	51	51	0.894	0.894	--	0.419	0.385	0.251	0.641

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	8206	7	0	68921	2667	2667	1	8.2
1	Z	8206	4	0	68921	2667	2667	1	8.3

Asta : 8028 [63 , 64]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1680	47	-228	80960	2800	2800	31	31	0.965	0.965	--	0.401	0.316	0.241	0.527

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1680	19	72	74419	2667	2667	(12+13)-II-2	18
1	Z	1680	11	120	74419	2667	2667	(12+13)-II-2	14

Asta : 8028 [64 , 65]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3123	-9	-364	80960	2800	2800	47	47	0.911	0.911	--	0.406	0.245	0.244	0.409

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3123	4	89	70211	2667	2667	(12+13)-VIII-3	13
1	Z	3123	2	149	70211	2667	2667	(12+13)-VIII-3	9.9

Asta : 8028 [65 , 66]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3653	-11	-252	80960	2800	2800	47	47	0.911	0.911	--	0.407	0.368	0.244	0.614

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	3653	4	93	70211	2667	2667	(12+13)-II-3	11
1	Z	3653	3	155	70211	2667	2667	(12+13)-II-3	9.0

Asta : 8028 [66 , 67]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3636	-11	-260	80960	2800	2800	47	47	0.911	0.911	--	0.407	0.366	0.244	0.609

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3636	4	95	70211	2667	2667	(12+13)-IV-1	11
1	Z	3636	3	158	70211	2667	2667	(12+13)-IV-1	8.9

Asta : 8028 [67 , 68]

Sez. G: Tubo100x100x8 L=177.5 cm Ln1=177.5 cm Ln2=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.248

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
2908	-9	-371	80960	2800	2800	47	47	0.911	0.911	--	0.406	0.245	0.243	0.408

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2908	4	91	70211	2667	2667	(12+13)-VI-1	13
1	Z	2908	2	152	70211	2667	2667	(12+13)-VI-1	10

Asta : 8028 [68 , 69]

Sez. G: Tubo100x100x8 L=115.0 cm Ln1=115.0 cm Ln2=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.557

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1696	47	-242	80960	2800	2800	31	31	0.965	0.965	--	0.401	0.303	0.241	0.505

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1696	19	73	74419	2667	2667	(12+13)-II-4	17
1	Z	1696	11	122	74419	2667	2667	(12+13)-II-4	14

Asta : 8029 [63 , 163]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3765	-600	134	80960	2800	2800	41	41	0.932	0.932	--	0.482	0.244	0.289	0.407

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3765	289	33	71883	2667	2667	1	5.8
1	Z	3765	174	55	71883	2667	2667	1	7.3

Asta : 8031 [64 , 164]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
2074	-570	-33	80960	2800	2800	41	41	0.932	0.932	--	0.564	0.242	0.338	0.404

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2074	321	8	71883	2667	2667	(12+13)-VIII-2	6.6
1	Z	2074	193	13	71883	2667	2667	(12+13)-VIII-2	9.4

Asta : 8031 [65 , 165]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
1222	-342	-18	80960	2800	2800	41	41	0.932	0.932	--	0.629	0.241	0.377	0.402

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1222	215	4	71883	2667	2667	(12+13)-VIII-2	10
1	Z	1222	129	7	71883	2667	2667	(12+13)-VIII-2	15

Asta : 8032 [66 , 166]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
698	-269	1	80960	2800	2800	41	41	0.932	0.932	--	0.544	0.241	0.326	0.401

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	698	146	0	71883	2667	2667	(12+13)-VI-2	15
1	Z	698	88	0	71883	2667	2667	(12+13)-VI-2	23

Asta : 8033 [67 , 167]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
1225	-342	18	80960	2800	2800	41	41	0.932	0.932	--	0.628	0.241	0.377	0.402

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1225	215	4	71883	2667	2667	(12+13)-VI-4	10
1	Z	1225	129	7	71883	2667	2667	(12+13)-VI-4	15

Asta : 8034 [68 , 168]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
2468	-494	39	80960	2800	2800	41	41	0.932	0.932	--	0.625	0.243	0.375	0.405

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2468	309	10	71883	2667	2667	1	6.5
1	Z	2468	185	16	71883	2667	2667	1	9.1

Asta : 8035 [69 , 169]

Sez. G: Tubo100x100x8 L=155.0 cm Ln1=155.0 cm Ln2=155.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=4.865

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
3774	-617	-135	80960	2800	2800	41	41	0.932	0.932	--	0.465	0.244	0.279	0.407

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3774	287	33	71883	2667	2667	1	5.8
1	Z	3774	172	55	71883	2667	2667	1	7.3

Asta : 8036 [63 , 164]

Sez. G: Tubo100x100x8 L=193.0 cm Ln1=193.0 cm Ln2=193.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.907

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-3363	8	-188	80960	2800	2800	51	51	0.894	0.894	--	0.408	0.370	0.245	0.617

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3363	3	70	68921	2667	2667	1	13
1	Z	3363	2	116	68921	2667	2667	1	11

Asta : 8037 [64 , 165]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2385	-12	-85	80960	2800	2800	63	63	0.838	0.838	--	0.538	0.388	0.647

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2385	6	33	64626	2667	2667	1	19
1	Z	2385	4	55	64626	2667	2667	1	17

Asta : 8038 [65 , 166]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-744	-9	151	80960	2800	2800	63	63	0.838	0.838	--	0.937	0.429	0.715

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	744	9	65	64626	2667	2667	(12+13)-VI-2	26
1	Z	744	5	108	64626	2667	2667	(12+13)-VI-2	19

Asta : 8039 [67 , 166]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-740	-9	-151	80960	2800	2800	63	63	0.838	0.838	--	0.936	0.426	0.710

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	740	9	64	64626	2667	2667	(12+13)-VIII-4	26
1	Z	740	5	107	64626	2667	2667	(12+13)-VIII-4	19

Asta : 8040 [68 , 167]

Sez. G: Tubo100x100x8 L=235.7 cm Ln1=235.7 cm Ln2=235.7 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.200

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2380	-12	88	80960	2800	2800	63	63	0.838	0.838	--	0.537	0.386	0.643

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2380	6	34	64626	2667	2667	1	19
1	Z	2380	4	57	64626	2667	2667	1	17

Asta : 8041 [69 , 168]

Sez. G: Tubo100x100x8 L=193.0 cm Ln1=193.0 cm Ln2=193.0 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=3.907

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3366	8	193	80960	2800	2800	51	51	0.894	0.894	--	0.408	0.370	0.617

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3366	3	72	68921	2667	2667	1	13
1	Z	3366	2	119	68921	2667	2667	1	11

Asta : 8042 [2 , 11]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
751	825	-274	80960	2800	2800	29	29	0.968	0.968	--	0.549	0.461	0.769

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	751	453	126	74672	2667	2667	(12+13)-IV-1	4.4
1	Z	751	272	210	74672	2667	2667	(12+13)-IV-1	5.2

Asta : 8042 [33 , 41]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
647	1087	-277	80960	2800	2800	29	29	0.968	0.968	--	0.599	0.450	0.360	0.750

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	647	652	125	74672	2667	2667	(12+13)-VIII-1	3.3
1	Z	647	391	208	74672	2667	2667	(12+13)-VIII-1	4.3

Asta : 8042 [11 , 18]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
502	-522	146	80960	2800	2800	29	29	0.968	0.968	--	0.920	0.394	0.552	0.657

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	502	481	58	74672	2667	2667	(12+13)-IV-2	4.8
1	Z	502	288	96	74672	2667	2667	(12+13)-IV-2	6.6

Asta : 8042 [18 , 25]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
827	-628	-6	80960	2800	2800	29	29	0.968	0.968	--	0.705	0.467	0.423	0.778

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	827	443	3	74672	2667	2667	1	5.6
1	Z	827	266	5	74672	2667	2667	1	8.9

Asta : 8042 [25 , 33]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
701	1051	-282	80960	2800	2800	29	29	0.968	0.968	--	0.597	0.451	0.358	0.751

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	701	627	127	74672	2667	2667	(12+13)-IV-2	3.4
1	Z	701	376	211	74672	2667	2667	(12+13)-IV-2	4.4

Asta : 8042 [41 , 48]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
780	-629	-3	80960	2800	2800	29	29	0.968	0.968	--	0.701	0.383	0.420	0.638

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	780	441	1	74672	2667	2667	1	5.7
1	Z	780	264	2	74672	2667	2667	1	9.1

Asta : 8042 [48 , 55]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
414	-525	147	80960	2800	2800	29	29	0.968	0.968	--	0.928	0.396	0.557	0.660

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	414	488	58	74672	2667	2667	(12+13)-VIII-1	4.8
1	Z	414	293	97	74672	2667	2667	(12+13)-VIII-1	6.6

Asta : 8042 [55 , 63]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
765	820	-271	80960	2800	2800	29	29	0.968	0.968	--	0.549	0.461	0.329	0.768

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	765	450	125	74672	2667	2667	(12+13)-VIII-2	4.4
1	Z	765	270	208	74672	2667	2667	(12+13)-VIII-2	5.3

Asta : 8043 [4 , 12]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
372	611	-411	80960	2800	2800	29	29	0.968	0.968	--	0.453	0.466	0.272	0.776

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	372	277	192	74672	2667	2667	(12+13)-IV-1	5.5
1	Z	372	166	319	74672	2667	2667	(12+13)-IV-1	5.3

Asta : 8043 [34 , 42]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
438	1057	-399	80960	2800	2800	29	29	0.968	0.968	--	0.587	0.459	0.352	0.765

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	438	621	183	74672	2667	2667	(12+13)-VIII-1	3.3
1	Z	438	372	305	74672	2667	2667	(12+13)-VIII-1	3.8

Asta : 8043 [12 , 19]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
195	-538	199	80960	2800	2800	29	29	0.968	0.968	--	0.976	0.392	0.586	0.653

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	195	525	78	74672	2667	2667	(12+13)-IV-2	4.4
1	Z	195	315	130	74672	2667	2667	(12+13)-IV-2	5.9

Asta : 8043 [19 , 26]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
144	-556	183	80960	2800	2800	29	29	0.968	0.968	--	0.736	0.423	0.442	0.705

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	144	409	77	74672	2667	2667	(12+13)-VIII-1	5.4
1	Z	144	246	129	74672	2667	2667	(12+13)-VIII-1	7.0

Asta : 8043 [26 , 34]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
441	1039	-400	80960	2800	2800	29	29	0.968	0.968	--	0.584	0.459	0.350	0.766

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	441	606	184	74672	2667	2667	(12+13)-IV-2	3.3
1	Z	441	364	306	74672	2667	2667	(12+13)-IV-2	3.9

Asta : 8043 [42 , 49]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
178	-554	183	80960	2800	2800	29	29	0.968	0.968	--	0.730	0.429	0.438	0.715

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	178	404	79	74672	2667	2667	(12+13)-VIII-2	5.5
1	Z	178	243	131	74672	2667	2667	(12+13)-VIII-2	7.0

Asta : 8043 [49 , 56]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
206	-546	198	80960	2800	2800	29	29	0.968	0.968	--	0.984	0.392	0.591	0.654

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	206	538	77	74672	2667	2667	(12+13)-VIII-1	4.3
1	Z	206	323	129	74672	2667	2667	(12+13)-VIII-1	5.8

Asta : 8043 [56 , 64]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
402	610	-415	80960	2800	2800	29	29	0.968	0.968	--	0.455	0.466	0.273	0.776

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	402	278	193	74672	2667	2667	(12+13)-VIII-2	5.5
1	Z	402	167	322	74672	2667	2667	(12+13)-VIII-2	5.3

Asta : 8044 [5 , 13]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-200	-529	322	80960	2800	2800	29	29	0.968	0.968	--	0.500	0.459	0.300	0.766

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	200	264	148	74672	2667	2667	(12+13)-II-4	6.4
1	Z	200	159	247	74672	2667	2667	(12+13)-II-4	6.5

Asta : 8044 [35 , 43]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
201	1044	-311	80960	2800	2800	29	29	0.968	0.968	--	0.575	0.452	0.345	0.753

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	201	601	140	74672	2667	2667	(12+13)-II-1	3.6
1	Z	201	360	234	74672	2667	2667	(12+13)-II-1	4.4

Asta : 8044 [13 , 20]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
50	-732	-2	80960	2800	2800	29	29	0.968	0.968	--	0.915	0.529	0.549	0.882

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	50	670	1	74672	2667	2667	1	4.0
1	Z	50	402	2	74672	2667	2667	1	6.6

Asta : 8044 [20 , 27]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
50	-732	-3	80960	2800	2800	29	29	0.968	0.968	--	0.673	0.545	0.404	0.909

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	50	492	2	74672	2667	2667	1	5.4
1	Z	50	295	3	74672	2667	2667	1	8.9

Asta : 8044 [27 , 35]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
200	1036	-316	80960	2800	2800	29	29	0.968	0.968	--	0.573	0.452	0.344	0.753

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	200	593	143	74672	2667	2667	(12+13)-VI-2	3.6
1	Z	200	356	238	74672	2667	2667	(12+13)-VI-2	4.4

Asta : 8044 [43 , 50]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
53	-728	-2	80960	2800	2800	29	29	0.968	0.968	--	0.670	0.375	0.402	0.625

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	53	488	1	74672	2667	2667	1	5.4
1	Z	53	293	2	74672	2667	2667	1	9.0

Asta : 8044 [50 , 57]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
53	-728	-5	80960	2800	2800	29	29	0.968	0.968	--	0.916	0.484	0.549	0.806

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	53	667	2	74672	2667	2667	1	4.0
1	Z	53	400	4	74672	2667	2667	1	6.6

Asta : 8044 [57 , 65]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-198	-530	317	80960	2800	2800	29	29	0.968	0.968	--	0.504	0.459	0.302	0.765

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	198	267	146	74672	2667	2667	(12+13)-VI-3	6.4
1	Z	198	160	243	74672	2667	2667	(12+13)-VI-3	6.5

Asta : 8045 [6 , 14]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-222	-554	-87	80960	2800	2800	29	29	0.968	0.968	--	0.531	0.389	0.319	0.648

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	222	294	34	74672	2667	2667	(12+13)-IV-2	7.9
1	Z	222	177	56	74672	2667	2667	(12+13)-IV-2	11

Asta : 8045 [36 , 44]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
82	1257	3	80960	2800	2800	29	29	0.968	0.968	--	0.561	0.476	0.336	0.793

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	82	705	1	74672	2667	2667	1	3.8
1	Z	82	423	2	74672	2667	2667	1	6.2

Asta : 8045 [14 , 21]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
81	-750	2	80960	2800	2800	29	29	0.968	0.968	--	0.929	0.380	0.558	0.633

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	81	697	1	74672	2667	2667	1	3.8
1	Z	81	418	1	74672	2667	2667	1	6.3

Asta : 8045 [21 , 28]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
81	-750	-1	80960	2800	2800	29	29	0.968	0.968	--	0.668	0.336	0.401	0.560

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	81	501	0	74672	2667	2667	1	5.3
1	Z	81	300	1	74672	2667	2667	1	8.8

Asta : 8045 [28 , 36]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
81	1253	-3	80960	2800	2800	29	29	0.968	0.968	--	0.560	0.474	0.336	0.791

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	81	701	1	74672	2667	2667	1	3.8
1	Z	81	421	2	74672	2667	2667	1	6.3

Asta : 8045 [44 , 51]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
82	-748	1	80960	2800	2800	29	29	0.968	0.968	--	0.666	0.343	0.400	0.572

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		

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Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	82	498	1	74672	2667	2667	1	5.3
1	Z	82	299	1	74672	2667	2667	1	8.8

Asta : 8045 [51 , 58]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
82	-748	-2	80960	2800	2800	29	29	0.968	0.968	--	0.930	0.375	0.558	0.625

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	82	695	1	74672	2667	2667	1	3.8
1	Z	82	417	1	74672	2667	2667	1	6.3

Asta : 8045 [58 , 66]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-223	-554	-91	80960	2800	2800	29	29	0.968	0.968	--	0.532	0.394	0.319	0.657

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	223	295	36	74672	2667	2667	(12+13)-VIII-1	7.9
1	Z	223	177	60	74672	2667	2667	(12+13)-VIII-1	11

Asta : 8046 [7 , 15]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-190	-525	-325	80960	2800	2800	29	29	0.968	0.968	--	0.497	0.460	0.298	0.767

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	190	261	149	74672	2667	2667	(12+13)-IV-2	6.4
1	Z	190	156	249	74672	2667	2667	(12+13)-IV-2	6.5

Asta : 8046 [37 , 45]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
200	1039	323	80960	2800	2800	29	29	0.968	0.968	--	0.574	0.453	0.344	0.755

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	200	596	146	74672	2667	2667	(12+13)-IV-3	3.6
1	Z	200	358	244	74672	2667	2667	(12+13)-IV-3	4.4

Asta : 8046 [15 , 22]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
55	-730	5	80960	2800	2800	29	29	0.968	0.968	--	0.914	0.480	0.548	0.801

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	55	667	2	74672	2667	2667	1	4.0
1	Z	55	400	4	74672	2667	2667	1	6.6

Asta : 8046 [22 , 29]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
55	-730	3	80960	2800	2800	29	29	0.968	0.968	--	0.672	0.361	0.403	0.602

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	55	490	1	74672	2667	2667	1	5.4
1	Z	55	294	2	74672	2667	2667	1	9.0

Asta : 8046 [29 , 37]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
199	1034	319	80960	2800	2800	29	29	0.968	0.968	--	0.573	0.453	0.344	0.754

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	199	593	144	74672	2667	2667	(12+13)-VIII-4	3.6
1	Z	199	356	241	74672	2667	2667	(12+13)-VIII-4	4.4

Asta : 8046 [45 , 52]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
55	-729	3	80960	2800	2800	29	29	0.968	0.968	--	0.671	0.550	0.403	0.916

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	55	489	2	74672	2667	2667	1	5.4
1	Z	55	293	3	74672	2667	2667	1	9.0

Asta : 8046 [52 , 59]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
55	-729	2	80960	2800	2800	29	29	0.968	0.968	--	0.914	0.536	0.549	0.894

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	55	666	1	74672	2667	2667	1	4.0
1	Z	55	400	2	74672	2667	2667	1	6.6

Asta : 8046 [59 , 67]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-191	-526	-331	80960	2800	2800	29	29	0.968	0.968	--	0.496	0.460	0.298	0.767

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	191	261	152	74672	2667	2667	(12+13)-VIII-1	6.3
1	Z	191	157	253	74672	2667	2667	(12+13)-VIII-1	6.4

Asta : 8047 [8 , 16]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
402	604	423	80960	2800	2800	29	29	0.968	0.968	--	0.452	0.466	0.271	0.776

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	402	273	197	74672	2667	2667	(12+13)-II-3	5.5
1	Z	402	164	328	74672	2667	2667	(12+13)-II-3	5.3

Asta : 8047 [38 , 46]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cm² ft=4300

kg/cmq: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
459	1039	407	80960	2800	2800	29	29	0.968	0.968	--	0.585	0.460	0.351	0.766

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	459	607	187	74672	2667	2667	(12+13)-VI-3	3.3
1	Z	459	364	312	74672	2667	2667	(12+13)-VI-3	3.9

Asta : 8047 [16 , 23]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
220	-542	-196	80960	2800	2800	29	29	0.968	0.968	--	0.972	0.387	0.583	0.645

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	220	527	76	74672	2667	2667	(12+13)-VI-4	4.4
1	Z	220	316	127	74672	2667	2667	(12+13)-VI-4	5.9

Asta : 8047 [23 , 30]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
180	-551	-187	80960	2800	2800	29	29	0.968	0.968	--	0.733	0.421	0.440	0.702

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	180	404	79	74672	2667	2667	(12+13)-VI-3	5.4
1	Z	180	242	131	74672	2667	2667	(12+13)-VI-3	7.0

Asta : 8047 [30 , 38]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
458	1039	400	80960	2800	2800	29	29	0.968	0.968	--	0.584	0.460	0.351	0.767

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	458	607	184	74672	2667	2667	(12+13)-VI-4	3.3
1	Z	458	364	307	74672	2667	2667	(12+13)-VI-4	3.9

Asta : 8047 [46 , 53]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
180	-551	-185	80960	2800	2800	29	29	0.968	0.968	--	0.733	0.428	0.440	0.713

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	180	404	79	74672	2667	2667	(12+13)-VI-4	5.4
1	Z	180	242	132	74672	2667	2667	(12+13)-VI-4	7.0

Asta : 8047 [53 , 60]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento γM=1.05 fyk/γM=2619 kg/cmq ft=4300

kg/cmq: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
220	-524	-202	80960	2800	2800	29	29	0.968	0.968	--	0.973	0.392	0.584	0.653

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	220	510	79	74672	2667	2667	(12+13)-VI-3	4.5
1	Z	220	306	132	74672	2667	2667	(12+13)-VI-3	6.0

Asta : 8047 [60 , 68]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
404	610	418	80960	2800	2800	29	29	0.968	0.968	--	0.453	0.466	0.272	0.776

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	404	276	195	74672	2667	2667	(12+13)-VI-4	5.5
1	Z	404	166	325	74672	2667	2667	(12+13)-VI-4	5.3

Asta : 8048 [9 , 17]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
760	817	271	80960	2800	2800	29	29	0.968	0.968	--	0.546	0.463	0.328	0.772

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	760	446	125	74672	2667	2667	(12+13)-VI-3	4.5
1	Z	760	268	209	74672	2667	2667	(12+13)-VI-3	5.3

Asta : 8048 [39 , 47]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
680	1067	283	80960	2800	2800	29	29	0.968	0.968	--	0.597	0.448	0.358	0.747

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	680	637	127	74672	2667	2667	(12+13)-II-3	3.4
1	Z	680	382	211	74672	2667	2667	(12+13)-II-3	4.3

Asta : 8048 [17 , 24]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
480	-523	-145	80960	2800	2800	29	29	0.968	0.968	--	0.915	0.397	0.549	0.661

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	480	478	57	74672	2667	2667	(12+13)-VI-4	4.8
1	Z	480	287	96	74672	2667	2667	(12+13)-VI-4	6.7

Asta : 8048 [24 , 31]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
818	-626	5	80960	2800	2800	29	29	0.968	0.968	--	0.704	0.408	0.423	0.679

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	818	441	2	74672	2667	2667	1	5.6
1	Z	818	265	3	74672	2667	2667	1	9.0

Asta : 8048 [31 , 39]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
684	1067	281	80960	2800	2800	29	29	0.968	0.968	--	0.596	0.448	0.358	0.747

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	684	636	126	74672	2667	2667	(12+13)-VI-4	3.4
1	Z	684	382	210	74672	2667	2667	(12+13)-VI-4	4.3

Asta : 8048 [47 , 54]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
816	-626	6	80960	2800	2800	29	29	0.968	0.968	--	0.704	0.393	0.422	0.655

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	816	441	2	74672	2667	2667	1	5.6
1	Z	816	265	4	74672	2667	2667	1	9.0

Asta : 8048 [54 , 61]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
476	-523	-146	80960	2800	2800	29	29	0.968	0.968	--	0.915	0.398	0.549	0.663

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	476	479	58	74672	2667	2667	(12+13)-II-3	4.8
1	Z	476	287	97	74672	2667	2667	(12+13)-II-3	6.7

Asta : 8048 [61 , 69]

Sez. G: Tubo100x100x8 L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300

kg/cm²: **Verificato**

SF_λ=6.816

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
759	816	269	80960	2800	2800	29	29	0.968	0.968	--	0.546	0.463	0.327	0.771

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	759	445	125	74672	2667	2667	(12+13)-II-4	4.5
1	Z	759	267	208	74672	2667	2667	(12+13)-II-4	5.3

Verifica Resistenza aste Metalliche

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Asta : 701 [102 , 104]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1868	840	47	4	-66	784	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22206	22206	2667	2667	1854	26	2.9	>100	2.9

Asta : 701 [104 , 105]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	162	277	-4	-117	-18	-331	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	20851	20851	2667	2667	1854	75	7.5	16	7.5

Asta : 701 [105 , 106]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
---	-----	---	----	----	----	----	----	-----	-----	-------

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	-1500	68	11	-65	-10	-322	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	21472	21472	2667	2667	1854	>100	7.0	28	7.0

Asta : 701 [106 , 107]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1497	-75	-12	67	-9	-327	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21455	21455	2667	2667	1854	>100	6.9	28	6.9

Asta : 701 [107 , 108]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	165	-291	5	113	-18	-329	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	20902	20902	2667	2667	1854	72	7.5	16	7.5

Asta : 701 [108 , 109]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	1872	-869	-57	-31	-74	852	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	77105	21890	21890	2667	2667	1854	25	2.7	60	2.7

Asta : 701 [101 , 102]

Sez. G: Tubo100x100x8 L=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2000	1640	-3193	500	620	1168	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	16257	16257	2667	2667	1854	5.1	1.4	3.7	1.4

Asta : 701 [109 , 110]

Sez. G: Tubo100x100x8 L=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
25	1	2069	-474	3311	-356	644	767	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
25	1	77105	17988	17988	2667	2667	1854	5.4	1.8	5.2	1.8

Asta : 702 [133 , 134]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4333	530	123	52	-152	542	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21632	21632	2667	2667	1854	41	3.2	36	3.2

Asta : 702 [134 , 135]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	415	185	-35	-43	-47	-208	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	21745	21745	2667	2667	1854	>100	9.9	43	9.9

Asta : 702 [135 , 136]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	-3519	40	-1	-33	-31	-229	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	21866	21866	2667	2667	1854	>100	7.0	57	7.0

Asta : 702 [136 , 137]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3511	41	1	-30	-31	227	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21896	21896	2667	2667	1854	>100	7.0	61	7.0

Asta : 702 [137 , 138]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	433	179	34	-36	-47	197	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21827	21827	2667	2667	1854	>100	10	52	10

Asta : 702 [138 , 139]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	4316	-507	-107	-78	-138	542	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	77105	21320	21320	2667	2667	1854	42	3.2	24	3.2

Asta : 702 [132 , 133]

Sez. G: Tubo100x100x8 L=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4447	-1734	-7066	-276	1380	-766	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	18944	18944	2667	2667	1854	2.7	1.2	6.7	1.2

Asta : 702 [139 , 140]

Sez. G: Tubo100x100x8 L=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
25	1	4528	943	7115	267	1383	-521	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
25	1	77105	19059	19059	2667	2667	1854	2.7	1.3	7.0	1.3

Asta : 703 [163 , 164]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1865	-864	57	-31	-74	-837	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21885	21885	2667	2667	1854	25	2.7	60	2.7

Asta : 703 [164 , 165]Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	161	-287	-5	112	-18	330	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	20910	20910	2667	2667	1854	73	7.5	17	7.5

Asta : 703 [165 , 166]Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	-1498	-72	12	66	-9	324	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	21464	21464	2667	2667	1854	>100	6.9	28	6.9

Asta : 703 [166 , 167]Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1503	73	-11	-66	-9	325	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21464	21464	2667	2667	1854	>100	6.9	28	6.9

Asta : 703 [167 , 168]Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	161	289	5	-113	-18	329	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	20906	20906	2667	2667	1854	72	7.6	16	7.6

Asta : 703 [168 , 169]Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	1870	866	-56	31	-74	-846	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	77105	21892	21892	2667	2667	1854	25	2.7	61	2.7

Asta : 703 [162 , 163]Sez. G: Tubo100x100x8 L=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2097	-1082	-3318	-364	645	-878	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	17882	17882	2667	2667	1854	5.4	1.7	5.1	1.7

Asta : 703 [169 , 170]Sez. G: Tubo100x100x8 L=25.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
25	1	2088	471	3321	354	646	-758	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
25	1	77105	18007	18007	2667	2667	1854	5.4	1.8	5.2	1.8

Asta : 704 [103 , 133]Sez. G: Tubo100x100x8 L=442.8 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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COMUNE DI ANDRIA
 RIUSO E RIDESTINAZIONE FUNZIONALE AD USO CULTURALE DELL'EX MATTATOIO

2° LOTTO FUNZIONALE

PROGETTO ESECUTIVO

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
443	1	-0	20	119	-0	299	-88	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
443	1	77105	22258	22258	2667	2667	1854	>100	6.9	>100	6.9

Asta : 704 [133 , 163]

Sez. G: Tubo100x100x8 L=442.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
443	1	-612	99	135	-9	232	-229	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
443	1	77105	22150	22150	2667	2667	1854	>100	5.5	>100	5.5

Asta : 705 [109 , 139]

Sez. G: Tubo100x100x8 L=442.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1239	85	-133	-9	226	206	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22153	22153	2667	2667	1854	>100	5.6	>100	5.6

Asta : 705 [139 , 169]

Sez. G: Tubo100x100x8 L=442.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
443	1	-1232	-85	132	9	226	205	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
443	1	77105	22153	22153	2667	2667	1854	>100	5.6	>100	5.6

Asta : 8000 [2 , 4]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1573	-408	-62	-58	37	-304	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21557	21557	2667	2667	1854	53	6.8	32	6.8

Asta : 8000 [4 , 5]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	2907	-364	16	-49	-4	366	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	21674	21674	2667	2667	1854	59	5.7	38	5.7

Asta : 8000 [5 , 6]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	3645	-170	13	-12	-7	257	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	22112	22112	2667	2667	1854	>100	6.8	>100	6.8

Asta : 8000 [6 , 7]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3647	175	-14	13	-6	259	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22098	22098	2667	2667	1854	>100	6.8	>100	6.8

Asta : 8000 [7 , 8]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3132	370	-16	51	-4	369	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21648	21648	2667	2667	1854	58	5.5	36	5.5

Asta : 8000 [8 , 9]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	1587	395	63	60	37	-294	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	77105	21534	21534	2667	2667	1854	55	6.9	31	6.9

Asta : 8001 [2 , 102]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3191	-110	-802	18	747	-59	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22041	22041	2667	2667	1854	27	2.9	>100	2.9

Asta : 8002 [4 , 104]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2085	-36	-391	118	568	-33	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	20838	20838	2667	2667	1854	53	4.0	16	4.0

Asta : 8003 [5 , 105]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1223	-23	-198	96	337	-18	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21112	21112	2667	2667	1854	>100	6.7	19	6.7

Asta : 8004 [6 , 106]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	695	-1	-195	5	267	-1	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22195	22195	2667	2667	1854	>100	9.1	>100	9.1

Asta : 8005 [7 , 107]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1224	23	-204	-97	343	18	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21095	21095	2667	2667	1854	>100	6.6	19	6.6

Asta : 8006 [8 , 108]Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2072	35	-405	-112	571	33	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	20911	20911	2667	2667	1854	52	4.0	17	4.0

Asta : 8007 [9 , 109]Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3205	116	-830	5	733	61	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22195	22195	2667	2667	1854	27	2.9	>100	2.9

Asta : 8008 [2 , 104]Sez. G: Tubo100x100x8 L=193.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
193	1	-3321	-182	12	112	1	192	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
193	1	77105	20920	20920	2667	2667	1854	>100	8.7	17	8.7

Asta : 8009 [4 , 105]Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-1797	-58	24	13	8	112	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22100	22100	2667	2667	1854	>100	15	>100	15

Asta : 8010 [5 , 106]Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-706	48	20	-14	2	-153	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22090	22090	2667	2667	1854	>100	15	>100	15

Asta : 8011 [7 , 106]Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-707	-48	20	13	2	150	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22103	22103	2667	2667	1854	>100	15	>100	15

Asta : 8012 [8 , 107]Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-1803	57	24	-17	8	-117	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22054	22054	2667	2667	1854	>100	14	>100	14

Asta : 8013 [9 , 108]Sez. G: Tubo100x100x8 L=193.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
193	1	-3329	187	11	-113	-0	-195	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
193	1	77105	20907	20907	2667	2667	1854	>100	8.6	16	8.6

Asta : 8014 [33 , 34]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4023	643	-175	-33	113	453	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21859	21859	2667	2667	1854	34	3.8	56	3.8

Asta : 8014 [34 , 35]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	7566	-449	-7	17	-33	448	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	22052	22052	2667	2667	1854	49	3.6	>100	3.6

Asta : 8014 [35 , 36]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	8855	-229	-4	4	-32	296	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	22207	22207	2667	2667	1854	97	4.2	>100	4.2

Asta : 8014 [36 , 37]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	8854	-240	4	5	-32	-306	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22203	22203	2667	2667	1854	92	4.1	>100	4.1

Asta : 8014 [37 , 38]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	7559	-459	8	17	-33	-454	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22050	22050	2667	2667	1854	48	3.6	>100	3.6

Asta : 8014 [38 , 39]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	3978	-645	172	37	110	457	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	77105	21814	21814	2667	2667	1854	34	3.8	50	3.8

Asta : 8015 [33 , 133]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
155	1	7108	-236	637	11	518	240	--	--	(12+13)-IV-2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
155	1	77105	22122	22122	2667	2667	1854	35	2.7	>100	2.7

Asta : 8016 [34 , 134]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4912	-79	-263	62	337	-70	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21517	21517	2667	2667	1854	82	4.6	30	4.6

Asta : 8017 [35 , 135]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3098	-56	-168	65	215	-41	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21478	21478	2667	2667	1854	>100	7.3	29	7.3

Asta : 8018 [36 , 136]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1930	2	-144	-6	149	1	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22185	22185	2667	2667	1854	>100	12	>100	12

Asta : 8019 [37 , 137]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3080	56	-170	-63	211	41	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21498	21498	2667	2667	1854	>100	7.4	29	7.4

Asta : 8020 [38 , 138]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4883	80	-270	-57	323	70	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21578	21578	2667	2667	1854	80	4.7	33	4.7

Asta : 8021 [39 , 139]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
155	1	7132	234	599	-18	500	-238	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
155	1	77105	22043	22043	2667	2667	1854	37	2.7	>100	2.7

Asta : 8022 [33 , 134]

Sez. G: Tubo100x100x8 L=193.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-8225	-11	-34	6	25	-19	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22186	22186	2667	2667	1854	>100	8.1	>100	8.1

Asta : 8023 [34 , 135]Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-4847	-60	-12	-27	-11	-83	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21930	21930	2667	2667	1854	>100	10	68	10

Asta : 8024 [35 , 136]Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-1675	-57	16	19	-10	129	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22033	22033	2667	2667	1854	>100	14	99	14

Asta : 8025 [37 , 136]Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-1686	-60	16	17	-10	131	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22053	22053	2667	2667	1854	>100	13	>100	13

Asta : 8026 [38 , 137]Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-4854	-58	-12	-29	-11	-83	--	--	(12+13)-VIII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21907	21907	2667	2667	1854	>100	10	63	10

Asta : 8027 [39 , 138]Sez. G: Tubo100x100x8 L=193.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
193	1	-6424	-68	1	77	-4	89	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
193	1	77105	21340	21340	2667	2667	1854	>100	8.5	24	8.5

Asta : 8028 [63 , 64]Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1583	397	-62	51	37	293	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21649	21649	2667	2667	1854	55	6.9	37	6.9

Asta : 8028 [64 , 65]Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	3123	361	16	47	-4	-364	--	--	(12+13)-VIII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	21688	21688	2667	2667	1854	60	5.6	39	5.6

Asta : 8028 [65 , 66]Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
177	1	3651	167	14	12	-6	-254	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
177	1	77105	22115	22115	2667	2667	1854	>100	6.9	>100	6.9

Asta : 8028 [66 , 67]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3633	-177	-14	-13	-7	-261	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22098	22098	2667	2667	1854	>100	6.8	>100	6.8

Asta : 8028 [67 , 68]

Sez. G: Tubo100x100x8 L=177.5 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2908	-374	-16	-50	-5	-371	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21659	21659	2667	2667	1854	58	5.6	37	5.6

Asta : 8028 [68 , 69]

Sez. G: Tubo100x100x8 L=115.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	1576	-398	63	-60	37	298	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	77105	21543	21543	2667	2667	1854	54	6.9	31	6.9

Asta : 8029 [63 , 163]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3190	-115	843	1	-741	-61	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22242	22242	2667	2667	1854	26	2.9	>100	2.9

Asta : 8030 [64 , 164]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2074	-35	404	-113	-570	-33	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	20903	20903	2667	2667	1854	52	4.0	16	4.0

Asta : 8031 [65 , 165]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1222	-23	203	-96	-342	-18	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21103	21103	2667	2667	1854	>100	6.6	19	6.6

Asta : 8032 [66 , 166]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	698	-1	196	-6	-269	-1	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22188	22188	2667	2667	1854	>100	9.1	>100	9.1

Asta : 8033 [67 , 167]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1225	23	204	96	-342	18	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	21107	21107	2667	2667	1854	>100	6.6	19	6.6

Asta : 8034 [68 , 168]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2083	36	405	112	-571	33	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	20911	20911	2667	2667	1854	52	3.9	17	3.9

Asta : 8035 [69 , 169]

Sez. G: Tubo100x100x8 L=155.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3197	115	828	-5	-732	61	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22199	22199	2667	2667	1854	27	3.0	>100	3.0

Asta : 8036 [63 , 164]

Sez. G: Tubo100x100x8 L=193.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
193	1	-3321	184	11	-111	-0	-188	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
193	1	77105	20928	20928	2667	2667	1854	>100	8.8	17	8.8

Asta : 8037 [64 , 165]

Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-1795	59	24	-14	8	-112	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22094	22094	2667	2667	1854	>100	15	>100	15

Asta : 8038 [65 , 166]

Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-709	-47	20	14	2	151	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22092	22092	2667	2667	1854	>100	15	>100	15

Asta : 8039 [67 , 166]

Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-704	48	20	-13	2	-151	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22103	22103	2667	2667	1854	>100	15	>100	15

Asta : 8040 [68 , 167]

Sez. G: Tubo100x100x8 L=235.7 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
236	1	-1793	-58	24	17	8	117	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	77105	22059	22059	2667	2667	1854	>100	14	>100	14

Asta : 8041 [69 , 168]

Sez. G: Tubo100x100x8 L=193.0 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
193	1	-3324	-187	11	112	-0	193	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
193	1	77105	20917	20917	2667	2667	1854	>100	8.6	17	8.6

Asta : 8042 [2 , 11]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	751	-144	-859	3	825	-274	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22226	22226	2667	2667	1854	26	2.4	>100	2.4

Asta : 8042 [33 , 41]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	647	-155	-1001	-3	1087	-277	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22227	22227	2667	2667	1854	22	1.9	>100	1.9

Asta : 8042 [11 , 18]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	796	116	-172	3	-522	-134	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22221	22221	2667	2667	1854	>100	3.9	>100	3.9

Asta : 8042 [18 , 25]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	834	-50	367	3	-522	-134	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22221	22221	2667	2667	1854	60	3.9	>100	3.9

Asta : 8042 [25 , 33]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	704	162	969	3	1049	-284	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22226	22226	2667	2667	1854	23	2.0	>100	2.0

Asta : 8042 [41 , 48]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	765	49	-375	-3	-525	-130	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22221	22221	2667	2667	1854	59	3.9	>100	3.9

Asta : 8042 [48 , 55]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	746	-115	167	-3	-525	-130	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22221	22221	2667	2667	1854	>100	3.9	>100	3.9

Asta : 8042 [55 , 63]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	765	143	854	-3	820	-271	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22224	22224	2667	2667	1854	26	2.4	>100	2.4

Asta : 8043 [4 , 12]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	372	-209	-772	4	611	-411	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22208	22208	2667	2667	1854	29	2.6	>100	2.6

Asta : 8043 [34 , 42]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	438	-212	-1003	-4	1057	-399	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22207	22207	2667	2667	1854	22	1.8	>100	1.8

Asta : 8043 [12 , 19]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	334	-140	-178	4	-540	143	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22209	22209	2667	2667	1854	>100	3.8	>100	3.8

Asta : 8043 [19 , 26]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	348	150	384	4	-539	142	--	--	(12+13)-I-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22208	22208	2667	2667	1854	58	3.8	>100	3.8

Asta : 8043 [26 , 34]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	441	212	995	4	1039	-400	--	--	(12+13)-IV-2

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22207	22207	2667	2667	1854	22	1.8	>100	1.8

Asta : 8043 [42 , 49]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	309	-52	-338	-4	-538	145	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22209	22209	2667	2667	1854	66	3.8	>100	3.8

Asta : 8043 [49 , 56]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	346	144	174	-4	-538	145	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22209	22209	2667	2667	1854	>100	3.8	>100	3.8

Asta : 8043 [56 , 64]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	402	211	768	-4	610	-415	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22209	22209	2667	2667	1854	29	2.6	>100	2.6

Asta : 8044 [5 , 13]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	277	-170	-602	2	385	-324	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22232	22232	2667	2667	1854	37	3.7	>100	3.7

Asta : 8044 [35 , 43]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201	-172	-1019	-2	1044	-311	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22232	22232	2667	2667	1854	22	2.0	>100	2.0

Asta : 8044 [13 , 20]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	50	1	-125	3	-732	-2	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22223	22223	2667	2667	1854	>100	3.6	>100	3.6

Asta : 8044 [20 , 27]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	50	1	525	3	-732	-2	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22223	22223	2667	2667	1854	42	3.6	>100	3.6

Asta : 8044 [27 , 35]Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	200	175	1015	2	1036	-316	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22231	22231	2667	2667	1854	22	2.0	>100	2.0

Asta : 8044 [43 , 50]Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	53	2	-527	-3	-728	-2	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22223	22223	2667	2667	1854	42	3.6	>100	3.6

Asta : 8044 [50 , 57]Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	53	2	123	-3	-728	-2	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22223	22223	2667	2667	1854	>100	3.6	>100	3.6

Asta : 8044 [57 , 65]Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	280	172	601	-2	388	-328	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22231	22231	2667	2667	1854	37	3.7	>100	3.7

Asta : 8045 [6 , 14]Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	81	1	-786	-0	-617	2	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22258	22258	2667	2667	1854	28	4.3	>100	4.3

Asta : 8045 [36 , 44]Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	82	1	-1264	0	1257	3	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22258	22258	2667	2667	1854	18	2.1	>100	2.1

Asta : 8045 [14 , 21]Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	81	1	-103	-0	-750	0	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22258	22258	2667	2667	1854	>100	3.5	>100	3.5

Asta : 8045 [21 , 28]Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	81	1	547	-0	-750	0	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22258	22258	2667	2667	1854	41	3.5	>100	3.5

Asta : 8045 [28 , 36]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	81	1	1263	-0	1253	-3	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22258	22258	2667	2667	1854	18	2.1	>100	2.1

Asta : 8045 [44 , 51]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	82	1	-548	0	-748	-0	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22258	22258	2667	2667	1854	41	3.6	>100	3.6

Asta : 8045 [51 , 58]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	82	1	102	0	-748	-0	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22258	22258	2667	2667	1854	>100	3.6	>100	3.6

Asta : 8045 [58 , 66]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	82	1	786	0	-616	-2	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22258	22258	2667	2667	1854	28	4.3	>100	4.3

Asta : 8046 [7 , 15]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	276	175	-688	-2	388	337	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22230	22230	2667	2667	1854	32	3.6	>100	3.6

Asta : 8046 [37 , 45]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	200	178	-1016	2	1039	323	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22230	22230	2667	2667	1854	22	1.9	>100	1.9

Asta : 8046 [15 , 22]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	55	2	-125	-3	-730	3	--	--	1

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22222	22222	2667	2667	1854	>100	3.6	>100	3.6

Asta : 8046 [22 , 29]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	55	2	525	-3	-730	3	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22222	22222	2667	2667	1854	42	3.6	>100	3.6

Asta : 8046 [29 , 37]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	199	-177	1013	-2	1034	319	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22232	22232	2667	2667	1854	22	2.0	>100	2.0

Asta : 8046 [45 , 52]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	55	1	-525	3	-729	2	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22223	22223	2667	2667	1854	42	3.6	>100	3.6

Asta : 8046 [52 , 59]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	55	1	125	3	-729	2	--	--	1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22223	22223	2667	2667	1854	>100	3.6	>100	3.6

Asta : 8046 [59 , 67]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	276	-174	603	2	387	332	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22232	22232	2667	2667	1854	37	3.7	>100	3.7

Asta : 8047 [8 , 16]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	402	215	-763	-4	604	423	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22209	22209	2667	2667	1854	29	2.6	>100	2.6

Asta : 8047 [38 , 46]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	459	215	-993	4	1039	407	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22207	22207	2667	2667	1854	22	1.8	>100	1.8

Asta : 8047 [16 , 23]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	153	-40	-164	-4	-538	147	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22206	22206	2667	2667	1854	>100	3.9	>100	3.9

Asta : 8047 [23 , 30]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	160	61	367	-4	-537	148	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22206	22206	2667	2667	1854	61	3.9	>100	3.9

Asta : 8047 [30 , 38]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	458	-211	993	-4	1039	400	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22207	22207	2667	2667	1854	22	1.8	>100	1.8

Asta : 8047 [46 , 53]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	370	151	-383	4	-535	-144	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22208	22208	2667	2667	1854	58	3.9	>100	3.9

Asta : 8047 [53 , 60]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	360	-143	177	4	-536	-144	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22209	22209	2667	2667	1854	>100	3.9	>100	3.9

Asta : 8047 [60 , 68]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	404	-212	772	4	610	418	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22209	22209	2667	2667	1854	29	2.6	>100	2.6

Asta : 8048 [9 , 17]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	760	140	-856	-3	817	271	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22224	22224	2667	2667	1854	26	2.4	>100	2.4

Asta : 8048 [39 , 47]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	680	162	-992	3	1067	283	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22226	22226	2667	2667	1854	22	1.9	>100	1.9

Asta : 8048 [17 , 24]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	425	46	-180	-3	-519	-126	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22228	22228	2667	2667	1854	>100	4.0	>100	4.0

Asta : 8048 [24 , 31]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	432	-116	361	-3	-519	-126	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22228	22228	2667	2667	1854	62	4.0	>100	4.0

Asta : 8048 [31 , 39]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	684	-161	992	-3	1067	281	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22226	22226	2667	2667	1854	22	1.9	>100	1.9

Asta : 8048 [47 , 54]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	429	117	-361	3	-518	-127	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22228	22228	2667	2667	1854	62	4.0	>100	4.0

Asta : 8048 [54 , 61]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	421	-47	180	3	-518	-127	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	77105	22228	22228	2667	2667	1854	>100	4.0	>100	4.0

Asta : 8048 [61 , 69]

Sez. G: Tubo100x100x8 L=110.6 cm Crit.: Acciaio_Svergolamento $\gamma M=1.05$ $f_{yk}/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	759	-140	856	3	816	269	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	77105	22224	22224	2667	2667	1854	26	2.4	>100	2.4

VERIFICHE STATO LIMITE DI ESERCIZIO

Verifica spostamenti verticali delle aste in Acciaio secondo NTC 2008

Scenario di calcolo : **Set_NT_SLV_SLD_A2_STR/GEO**

Travata: 8000 [2 , 9]

$L = 940.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
470.0	21	0.90	37.60	42

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	31.33	>100

Travata: 8014 [33 , 39]

$L = 940.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
470.0	21	2.26	37.60	17

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	31.33	>100

Travata: 8028 [63 , 69]

$L = 940.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
470.0	21	0.89	37.60	42

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	31.33	>100

Travata: 8042 [2 , 63]

$L = 885.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
674.8	21	7.11	35.40	5.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	29.50	>100

Travata: 8043 [4 , 64]

$L = 885.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
210.2	21	8.43	35.40	4.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	29.50	>100

Travata: 8044 [5 , 65]

L = 885.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
199.1	21	9.93	35.40	3.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	29.50	>100

Travata: 8045 [6 , 66]

L = 885.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
199.1	21	10.46	35.40	3.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	29.50	>100

Travata: 8046 [7 , 67]

L = 885.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
199.1	21	9.88	35.40	3.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	29.50	>100

Travata: 8047 [8 , 68]

L = 885.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
210.2	21	8.33	35.40	4.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	29.50	>100

Travata: 8048 [9 , 69]

L = 885.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
674.8	21	7.05	35.40	5.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	29.50	>100

Travata: 8001 [2 , 102]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.17	>100

Travata: 8002 [4 , 104]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.17	>100

Travata: 8003 [5 , 105]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.17	>100

Travata: 8004 [6 , 106]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.17	>100

Travata: 8005 [7 , 107]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.17	>100

Travata: 8006 [8 , 108]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{\max} mm	L/250.00 mm	Cs
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x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8007 [9 , 109]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8008 [2 , 104]

L = 193.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
135.1	21	0.00	7.72	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	6.43	>100

Travata: 8009 [4 , 105]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
117.8	21	0.04	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	7.86	>100

Travata: 8010 [5 , 106]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
117.8	21	0.04	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	7.86	>100

Travata: 8011 [7 , 106]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
117.8	21	0.04	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
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x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	7.86	>100

Travata: 8012 [8 , 107]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
117.8	21	0.04	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	7.86	>100

Travata: 8013 [9 , 108]

L = 193.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
135.1	21	0.00	7.72	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	6.43	>100

Travata: 8015 [33 , 133]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8016 [34 , 134]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8017 [35 , 135]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8018 [36 , 136]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8019 [37 , 137]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8020 [38 , 138]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8021 [39 , 139]

$L = 155.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8022 [33 , 134]

$L = 193.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
57.9	21	-0.01	7.72	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	6.43	>100

Travata: 8023 [34 , 135]

$L = 235.7\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	

x	Comb.	δ_{max}	L/250.00	Cs
94.3	21	0.07	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	7.86	>100

Travata: 8024 [35 , 136]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
117.8	21	0.09	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	7.86	>100

Travata: 8025 [37 , 136]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
117.8	21	0.09	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	7.86	>100

Travata: 8026 [38 , 137]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
94.3	21	0.07	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	7.86	>100

Travata: 8027 [39 , 138]

L = 193.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
57.9	21	-0.01	7.72	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	6.43	>100

Travata: 8029 [63 , 163]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	$\delta 2$	L/300.00	Cs
0.0	21	-0.00	5.17	>100

Travata: 8030 [64 , 164]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8031 [65 , 165]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8032 [66 , 166]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8033 [67 , 167]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8034 [68 , 168]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	$\delta 2$	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	5.17	>100

Travata: 8035 [69 , 169]

L = 155.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
62.0	21	0.00	6.20	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	5.17	>100

Travata: 8036 [63 , 164]

L = 193.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
135.1	21	0.00	7.72	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	6.43	>100

Travata: 8037 [64 , 165]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
117.8	21	0.04	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	7.86	>100

Travata: 8038 [65 , 166]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
117.8	21	0.04	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	7.86	>100

Travata: 8039 [67 , 166]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
117.8	21	0.04	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_2 mm	L/300.00 mm	Cs
0.0	21	-0.00	7.86	>100

Travata: 8040 [68 , 167]

L = 235.7cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x cm	Comb.	δ_{max} mm	L/250.00 mm	Cs
117.8	21	0.04	9.43	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	7.86	>100

Travata: 8041 [69 , 168]

L = 193.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
135.1	21	0.00	7.72	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	6.43	>100

Travata: 701 [101 , 110]

L = 990.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
495.0	21	1.14	39.60	35

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	33.00	>100

Travata: 702 [132 , 140]

L = 990.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
495.0	21	2.83	39.60	14

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	33.00	>100

Travata: 703 [162 , 170]

L = 990.0cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
495.0	21	1.14	39.60	35

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	33.00	>100

Travata: 704 [103 , 163]

L = 885.3cm

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
398.5	21	-7.66	35.41	4.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	29.51	>100

Travata: 705 [109 , 169]

$L = 885.0\text{cm}$

Crit.Prog: Acciaio_Svergolamento $\delta c = 0.0\text{cm}$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{\max}	L/250.00	Cs
cm		mm	mm	
309.8	21	0.31	35.40	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
0.0	21	-0.00	29.50	>100